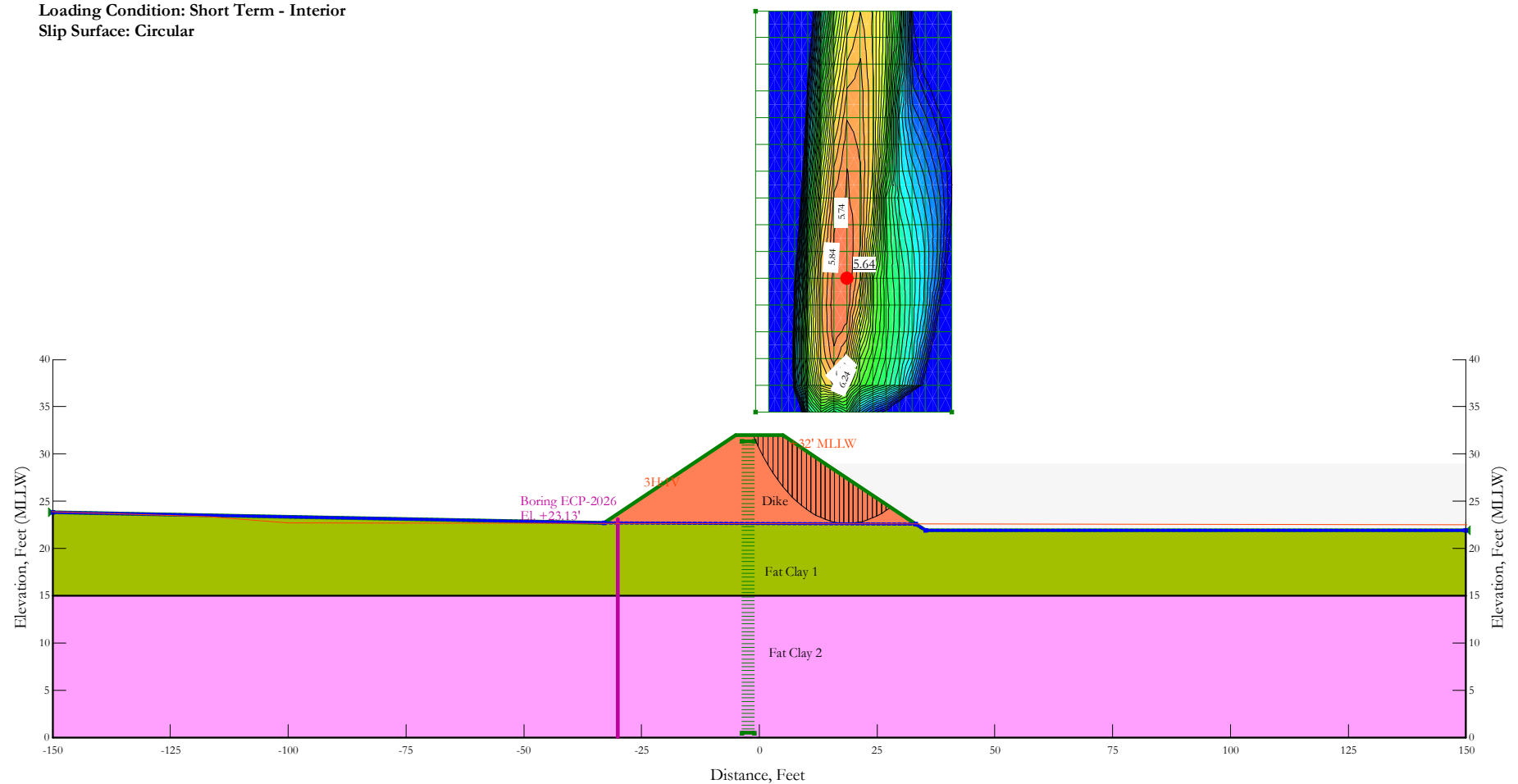


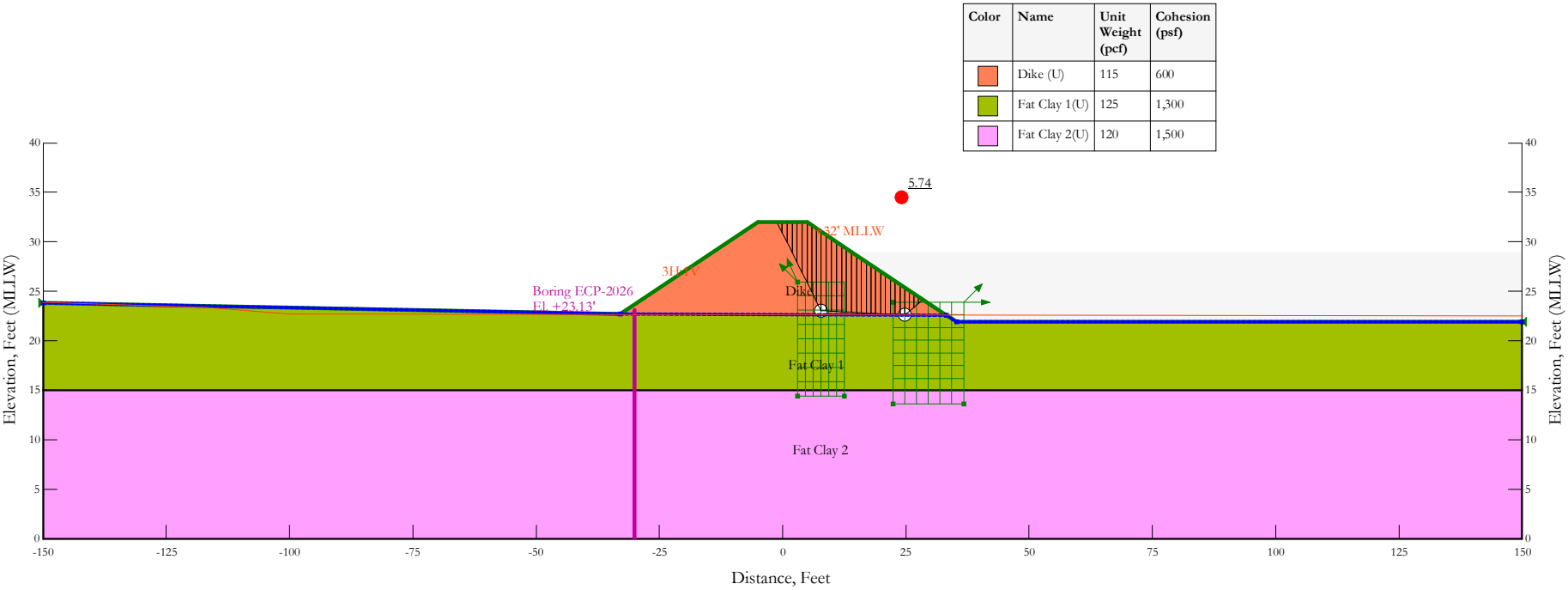
Project Name: Houston Ship Channel Expansion Channel Improvement Project
 Location: Beltway 8 Placement Area
 Station: 10+00
 HVJ Project Number: HG1910092.2.1
 Boring ECP-2026
 Loading Condition: Short Term - Interior
 Slip Surface: Circular

Color	Name	Unit Weight (pcf)	Cohesion (psf)
Orange	Dike (U)	115	600
Green	Fat Clay 1(U)	125	1,300
Pink	Fat Clay 2(U)	120	1,500

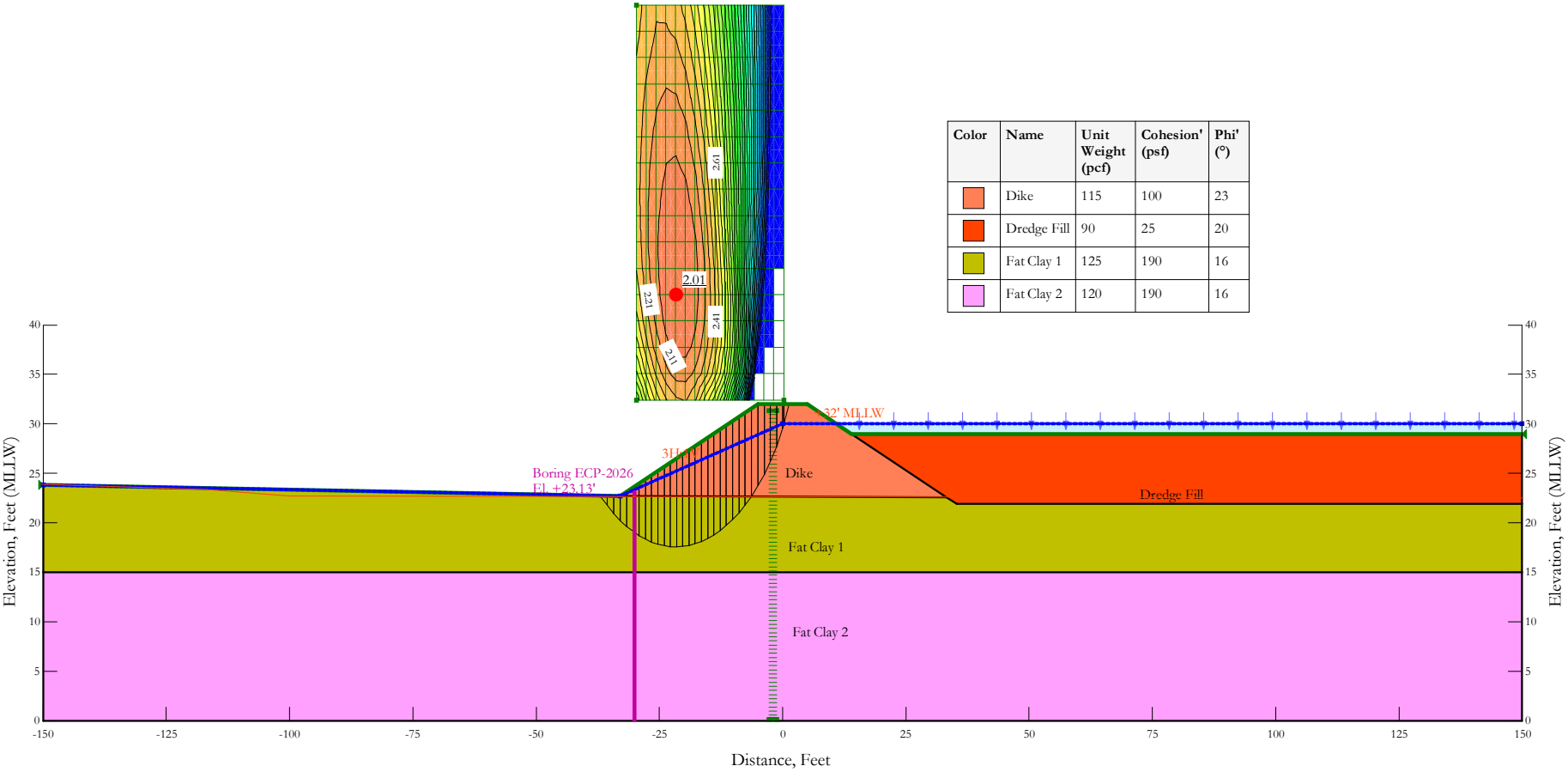


Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 10+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2026

Loading Condition: Short Term - Interior
Slip Surface: Block

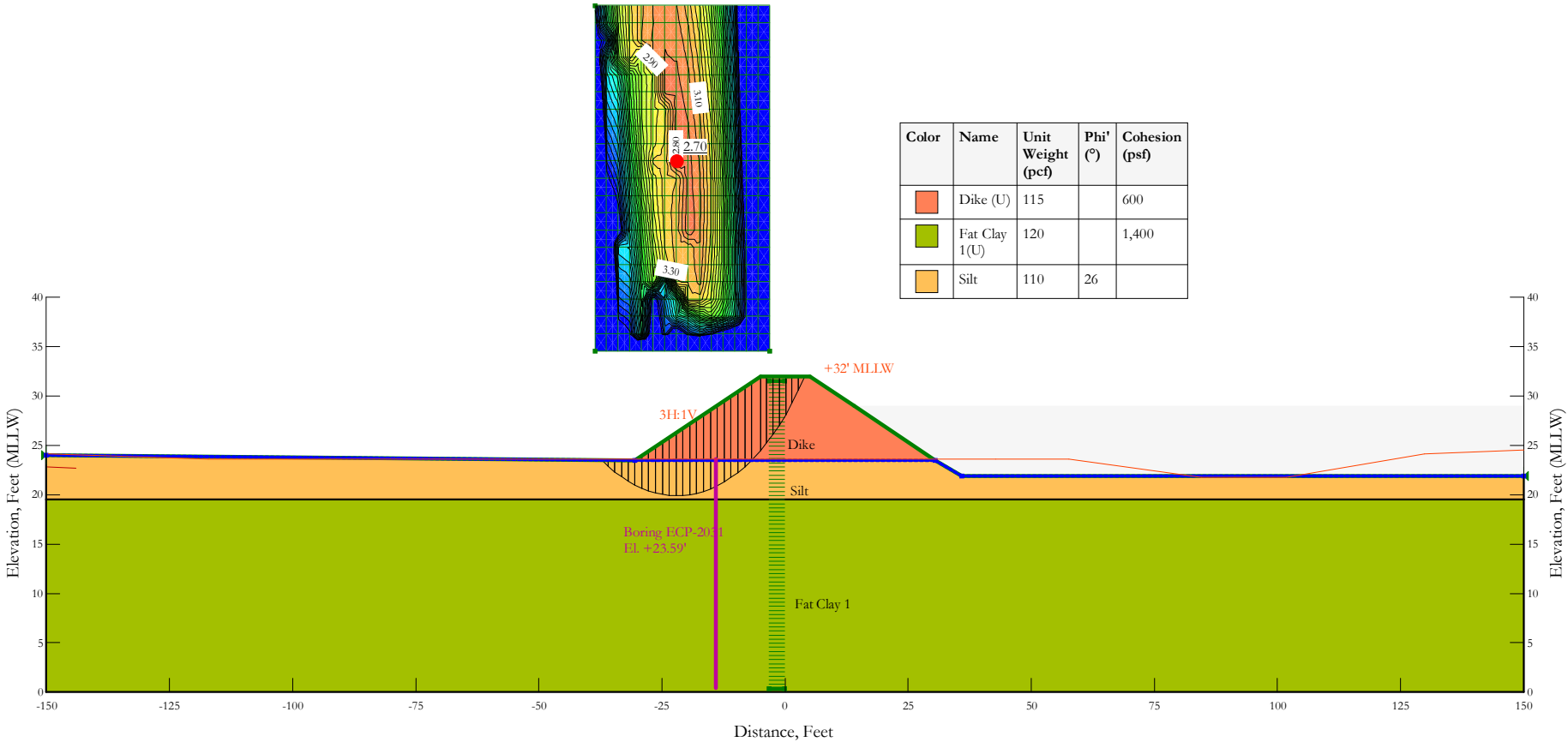


Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 10+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2026
Loading Condition: Long Term - Exterior
Slip Surface: Circular



Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 35+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2031

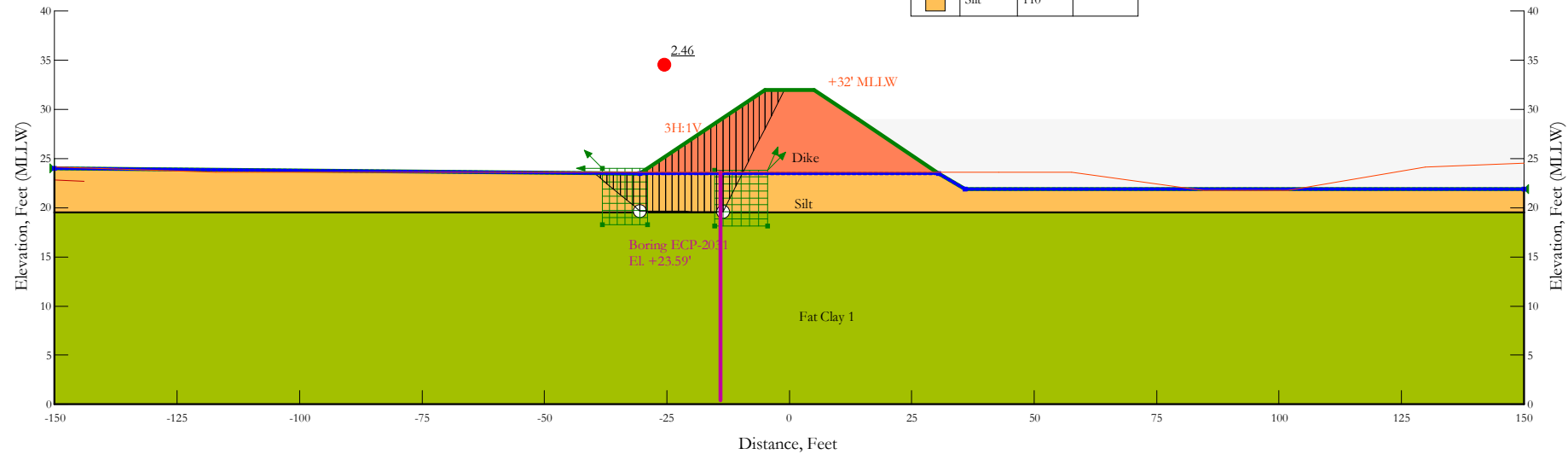
Loading Condition: Short Term - Exterior
Slip Surface: Circular



Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 35+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2031

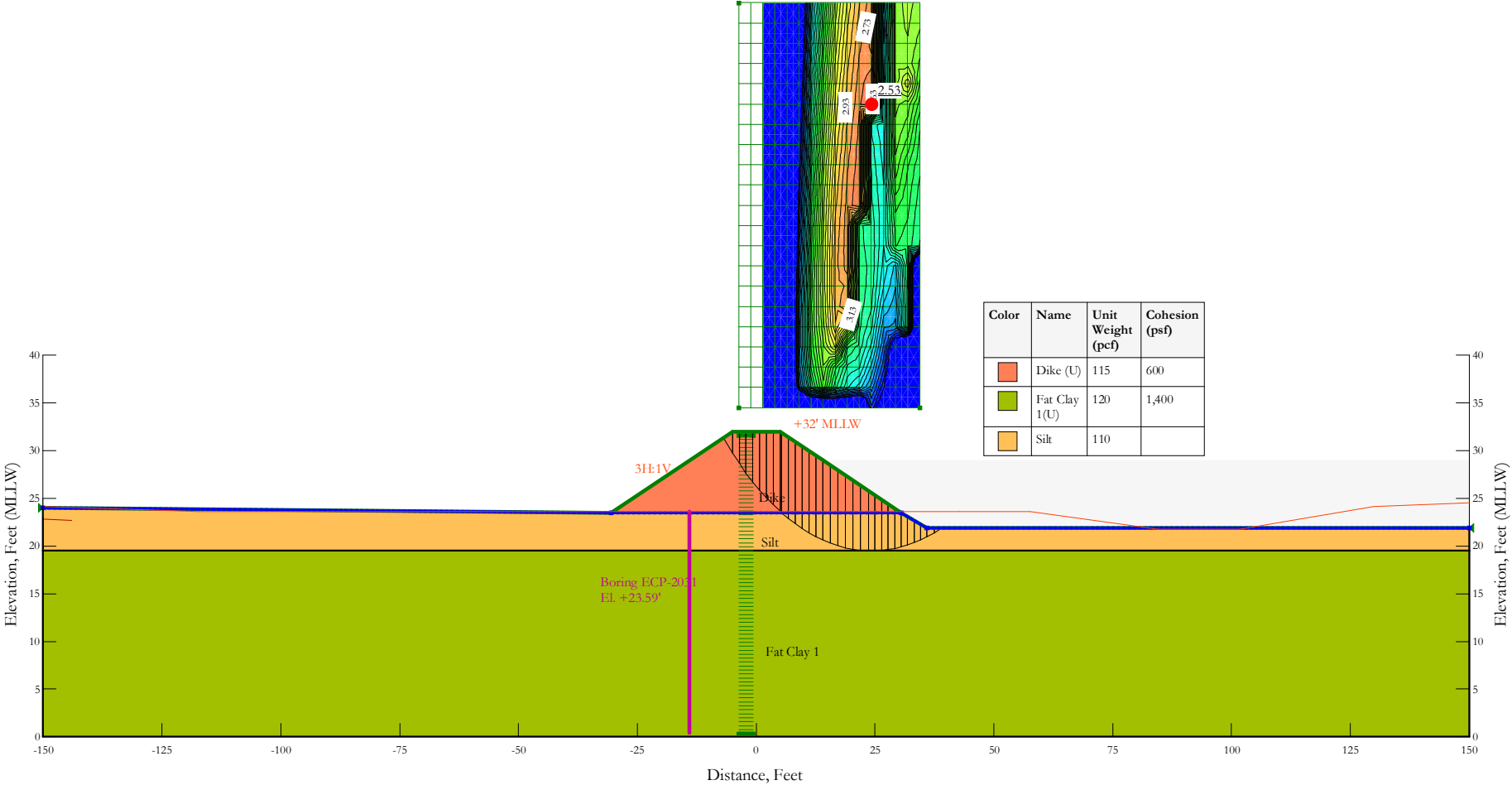
Loading Condition: Short Term - Exterior
Slip Surface: Block

Color	Name	Unit Weight (pcf)	Cohesion (psf)
	Dike (U)	115	600
	Fat Clay 1(U)	120	1,400
	Silt	110	



Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 35+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2031

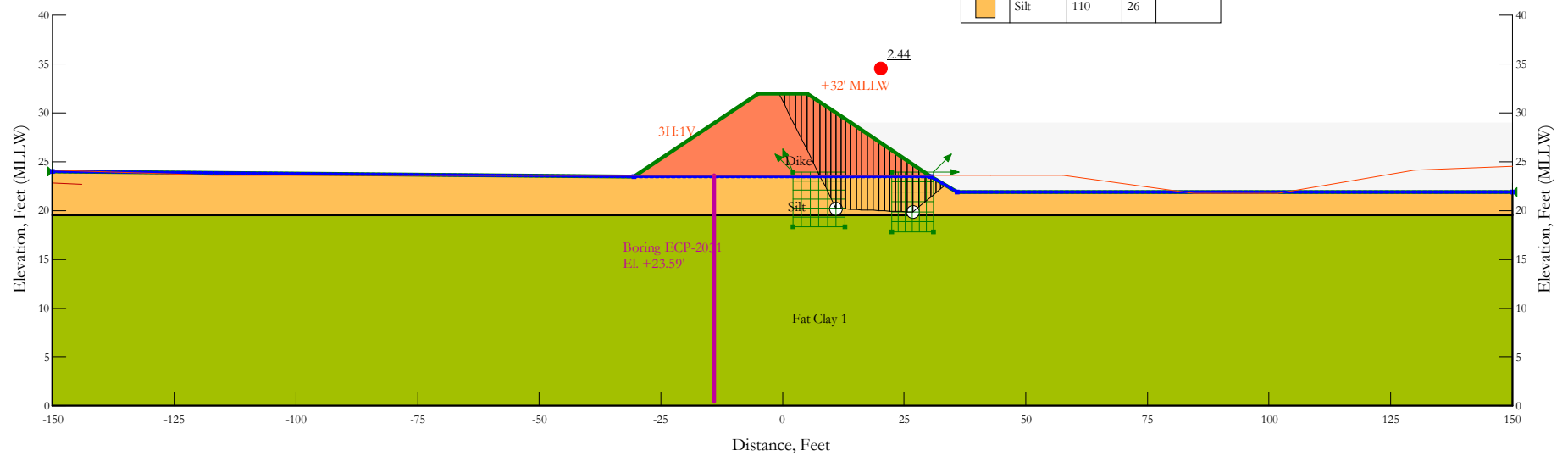
Loading Condition: Short Term - Interior
Slip Surface: Circular



Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 35+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2031

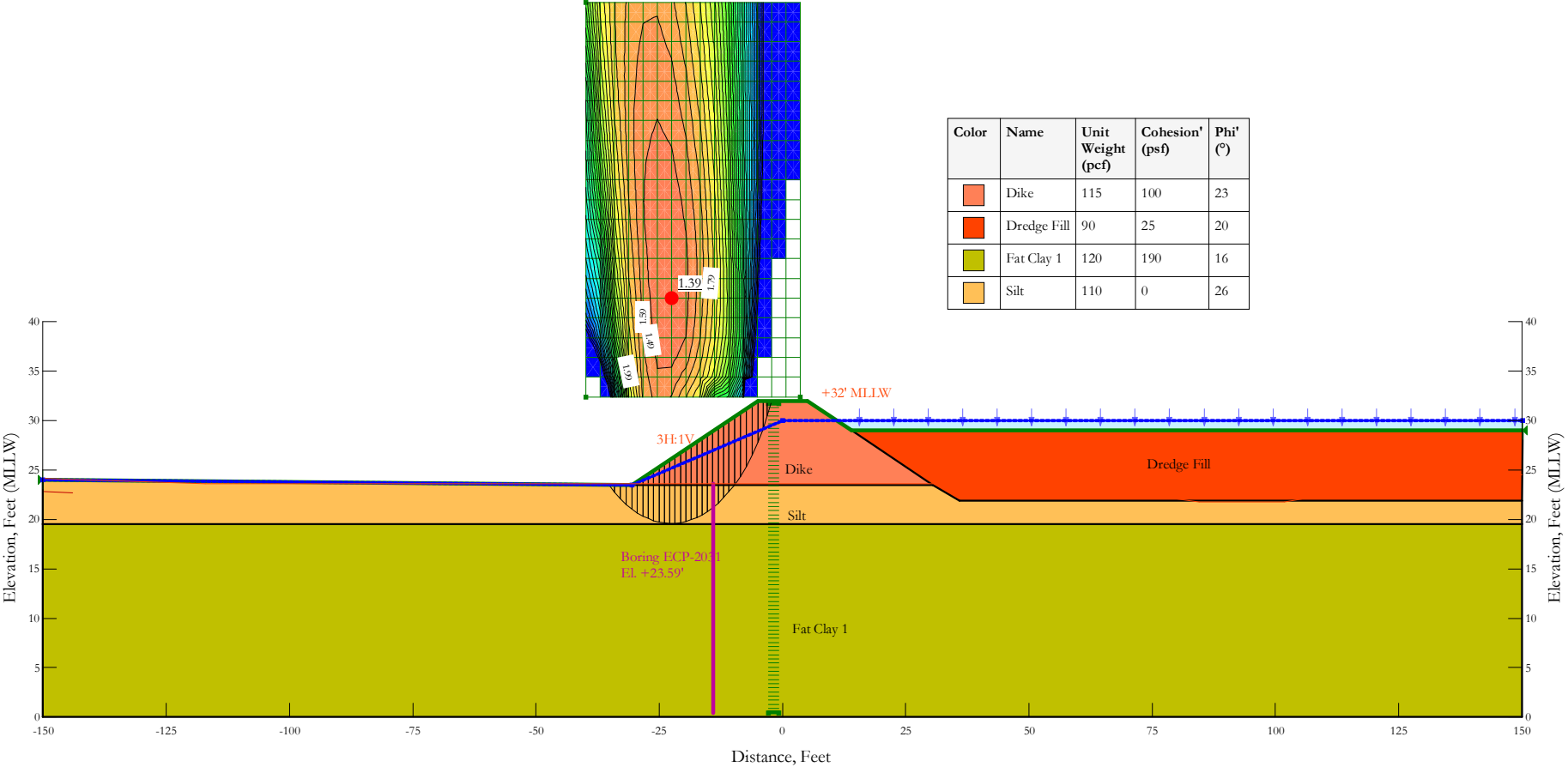
Loading Condition: Short Term - Interior
Slip Surface: Block

Color	Name	Unit Weight (pcf)	Phi' (°)	Cohesion (psf)
	Dike (U)	115		600
	Fat Clay 1(U)	120		1,400
	Silt	110	26	



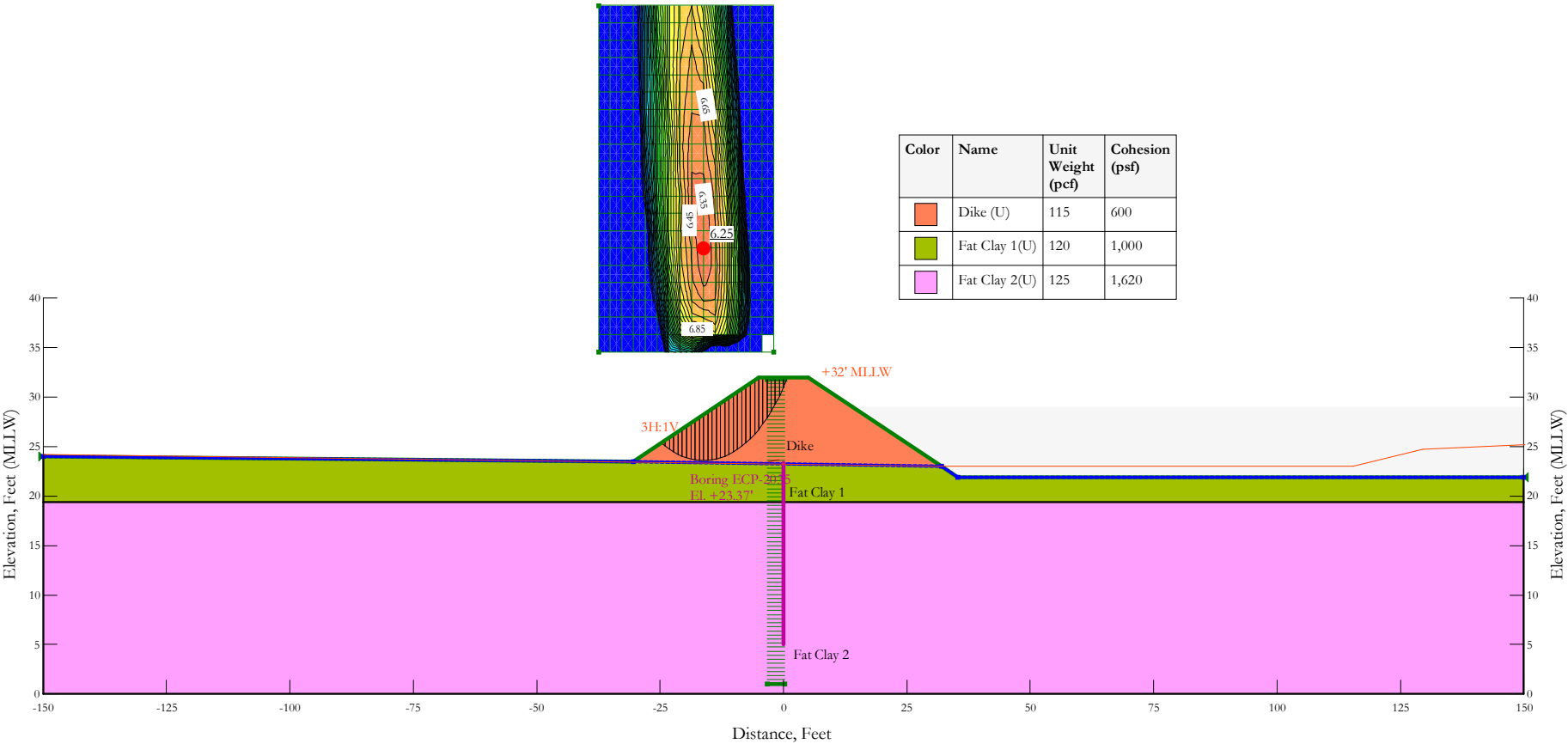
Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 35+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2031

Loading Condition: Long Term - Exterior
Slip Surface: Circular



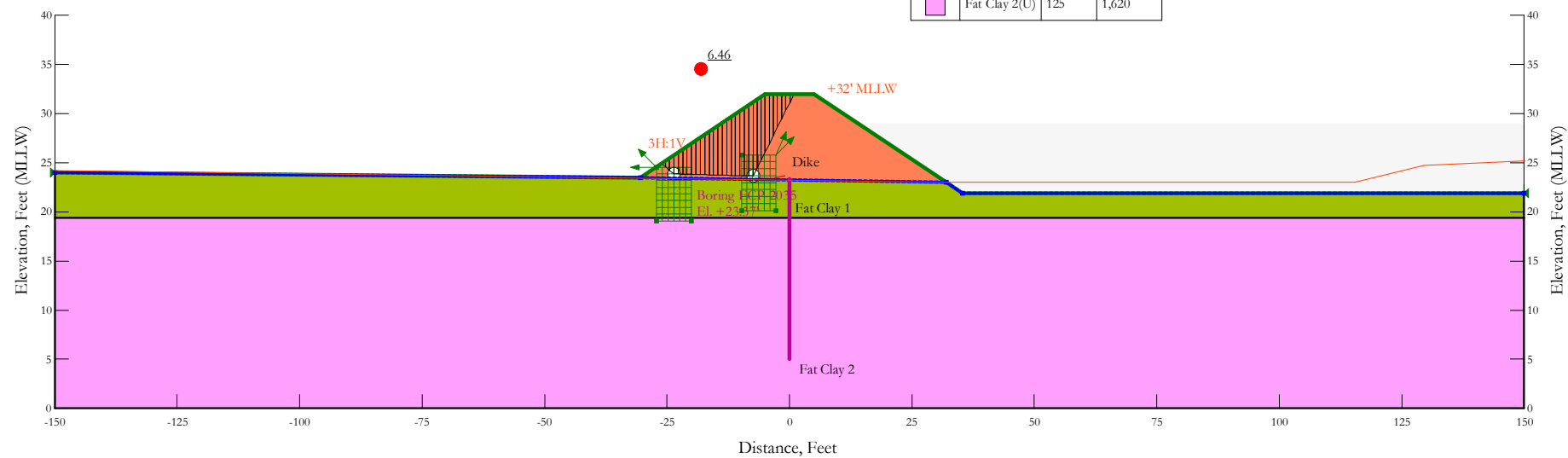
Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 50+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2035

Loading Condition: Short Term - Exterior
Slip Surface: Circular

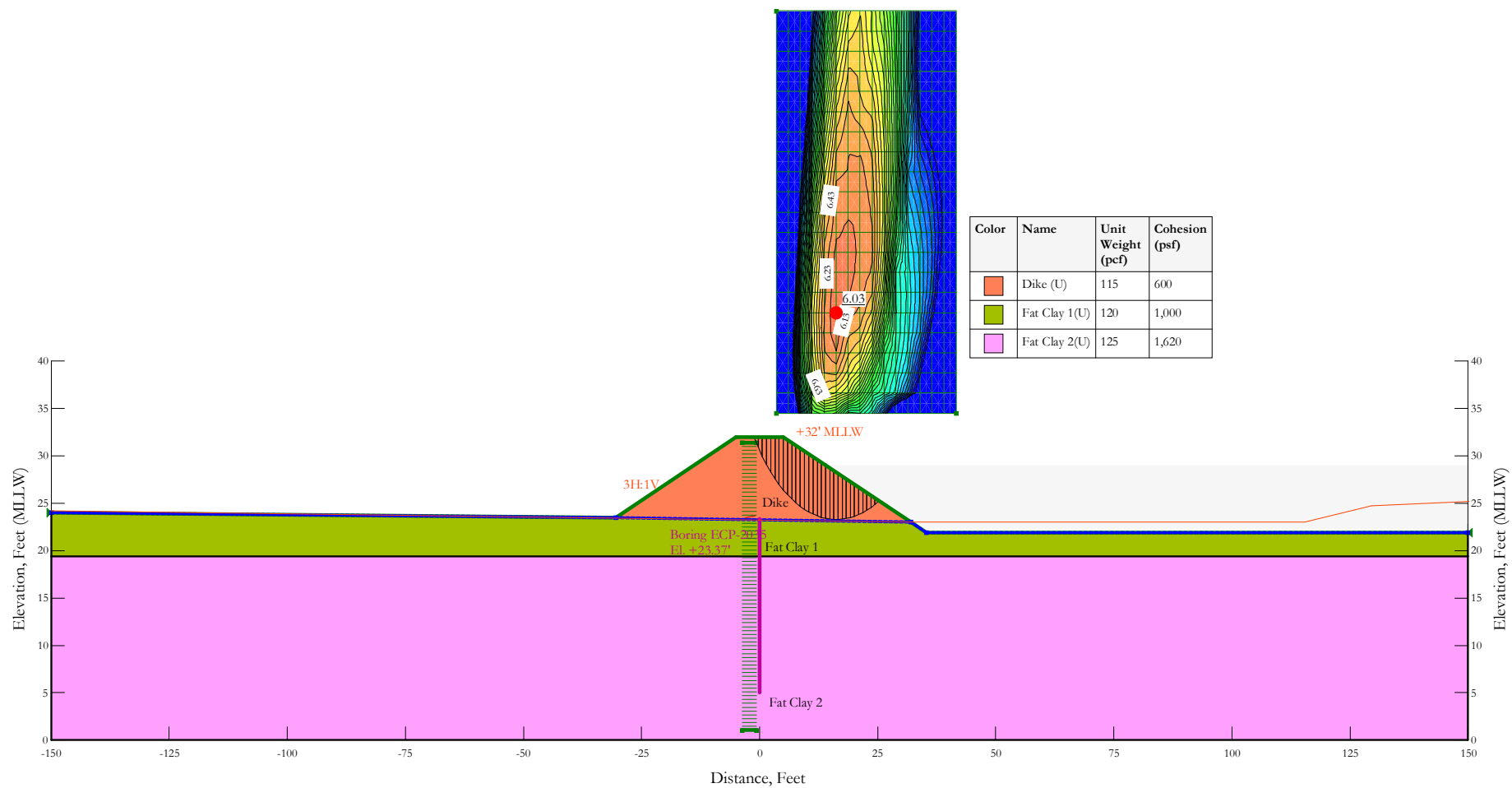


Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 50+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2035
Loading Condition: Short Term - Exterior
Slip Surface: Block

Color	Name	Unit Weight (pcf)	Cohesion (psf)
	Dike (U)	115	600
	Fat Clay 1(U)	120	1,000
	Fat Clay 2(U)	125	1,620

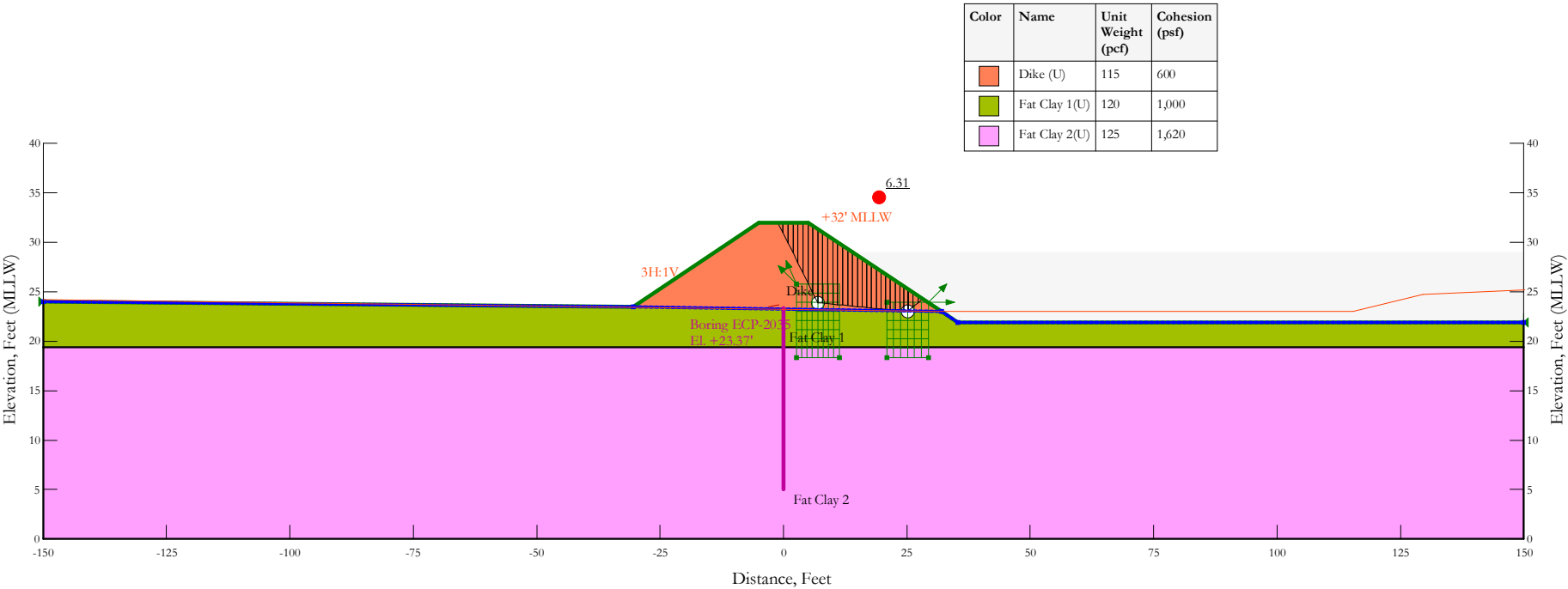


Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 50+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2035
Loading Condition: Short Term - Interior
Slip Surface: Circular



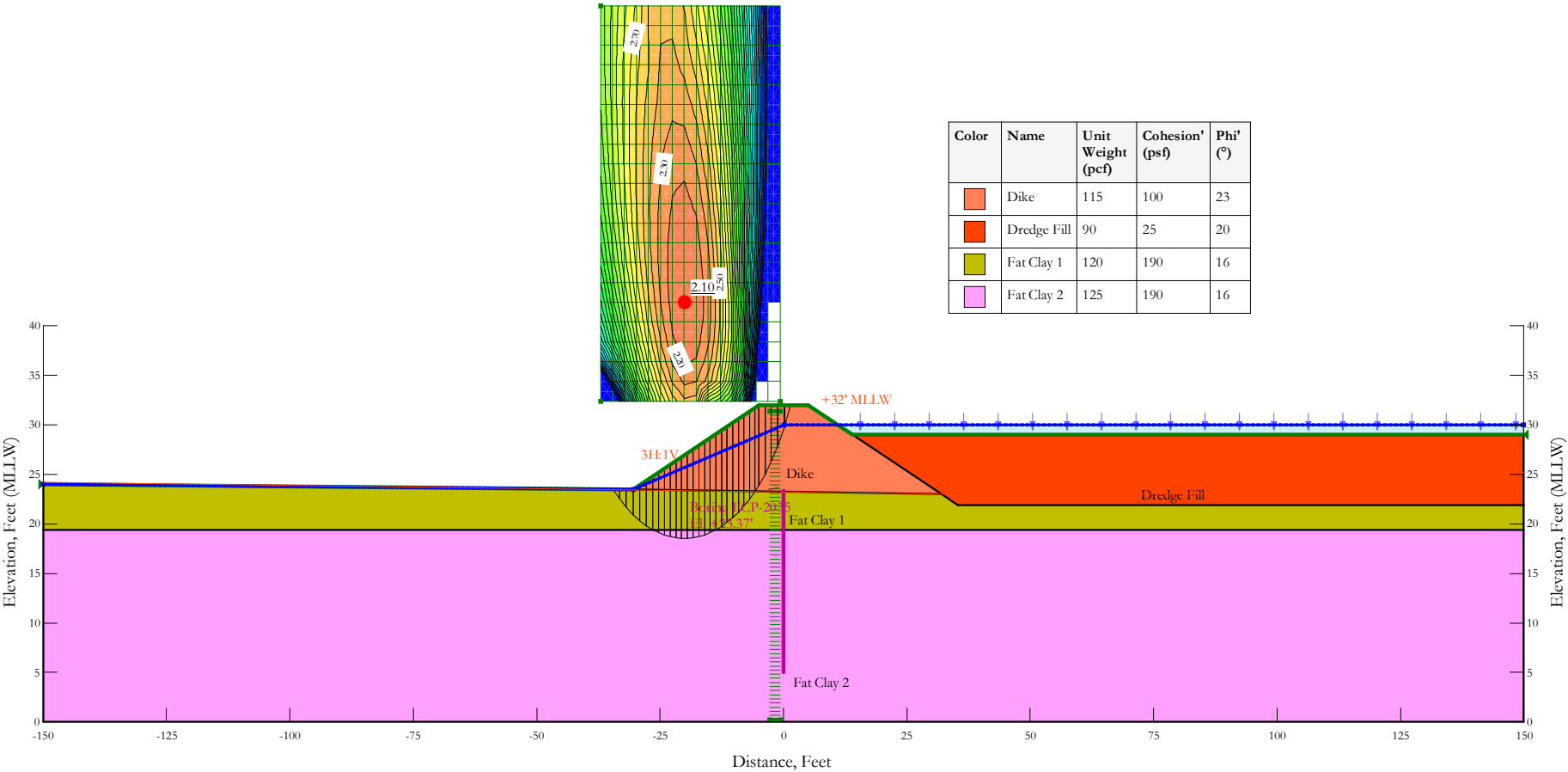
Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 50+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2035

Loading Condition: Short Term - Interior
Slip Surface: Block



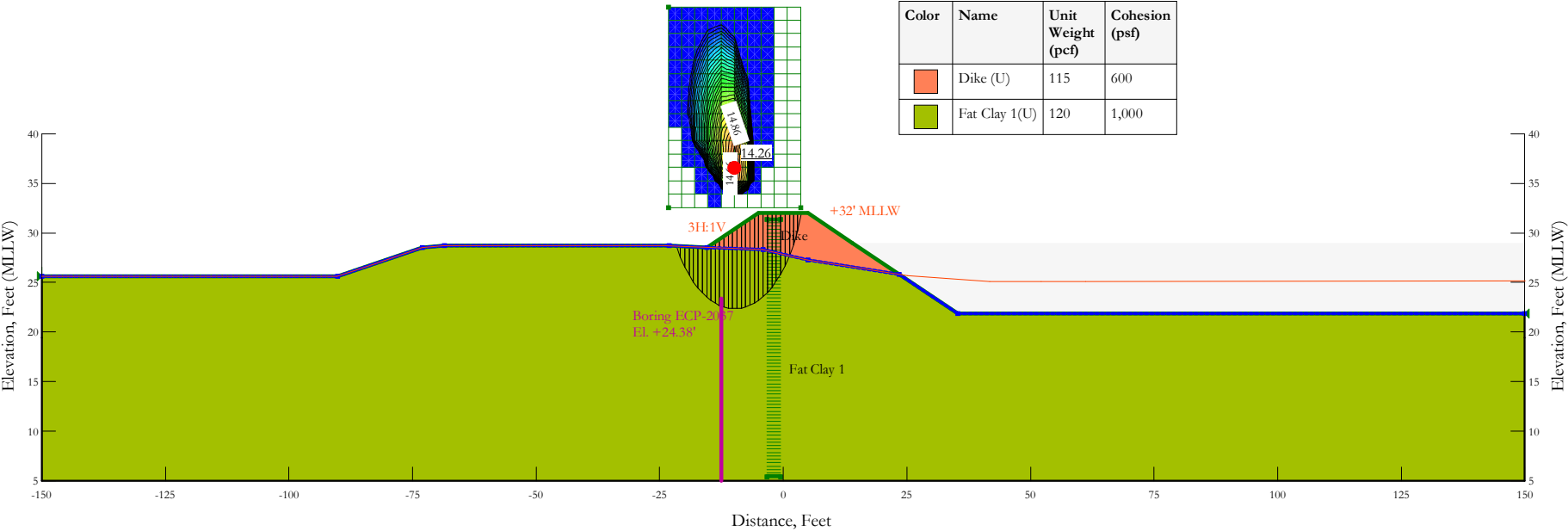
Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 50+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2035

Loading Condition: Long Term - Exterior
Slip Surface: Circular



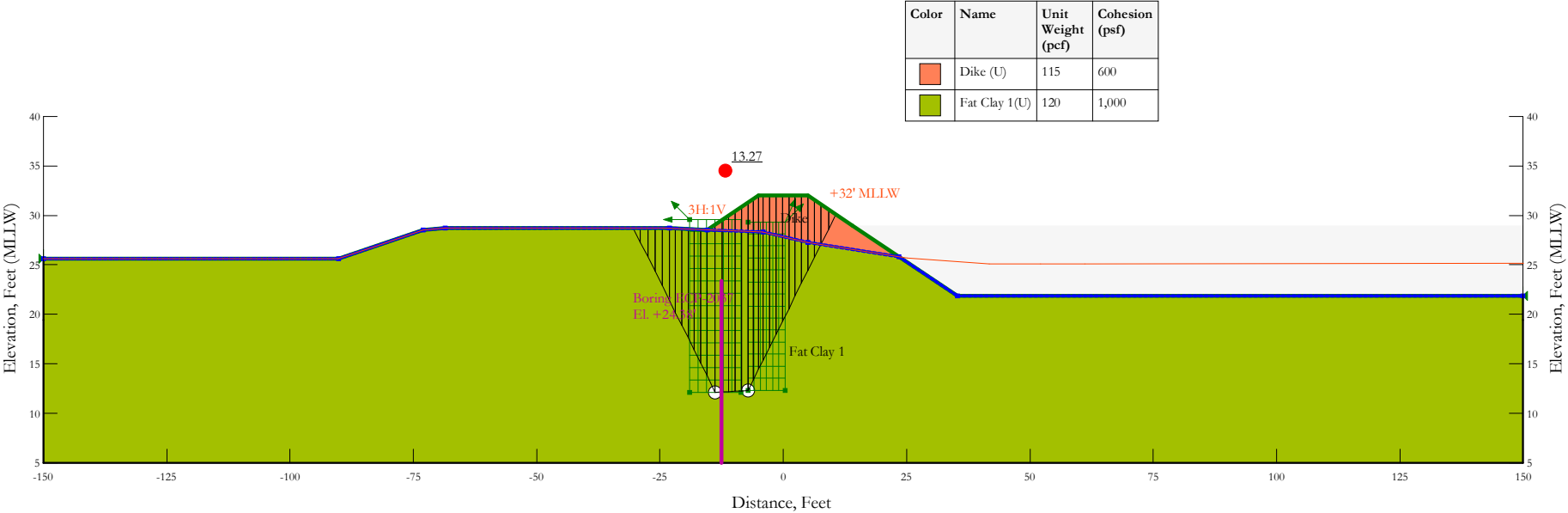
Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 70+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2037

Loading Condition: Short Term - Exterior
Slip Surface: Circular



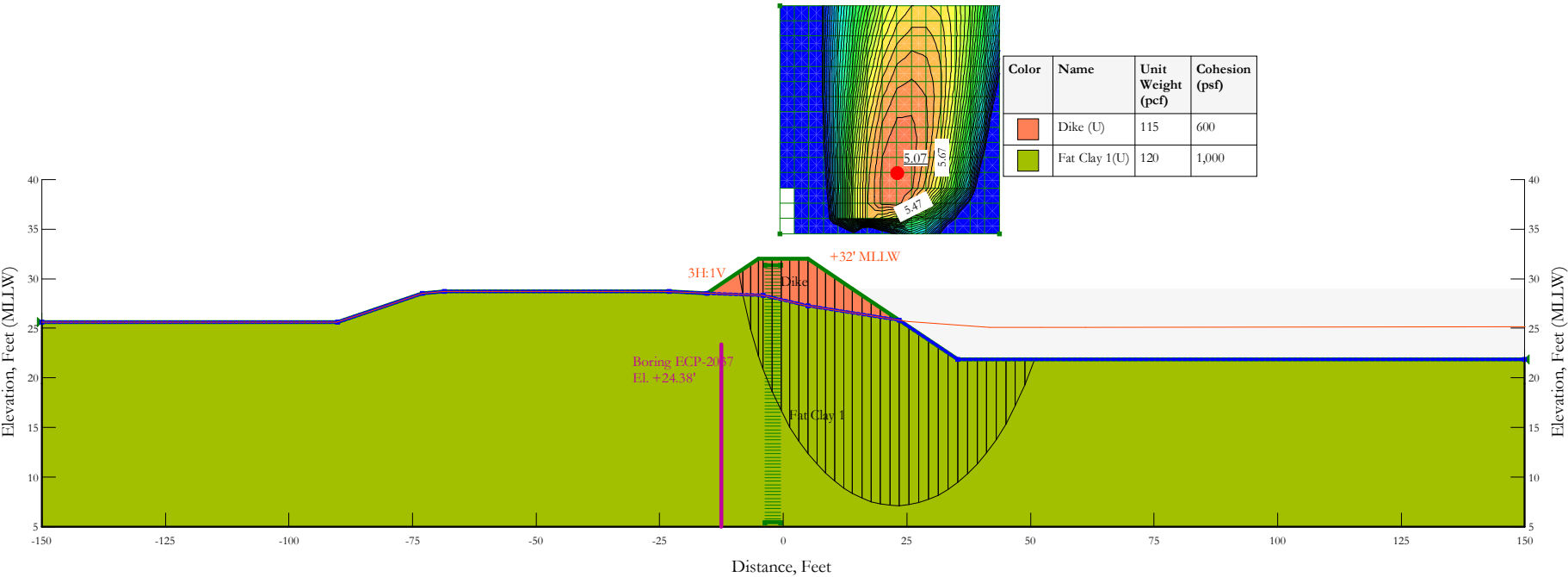
Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 70+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2037

Loading Condition: Short Term - Exterior
Slip Surface: Block



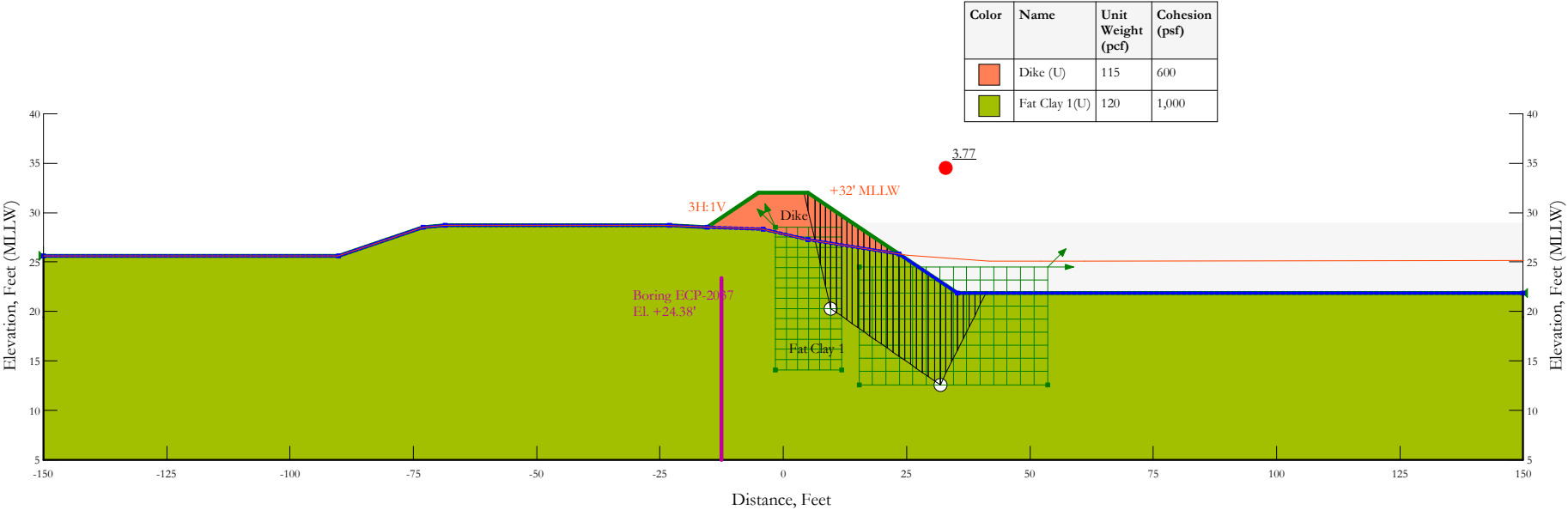
Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 70+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2037

Loading Condition: Short Term - Interior
Slip Surface: Circular



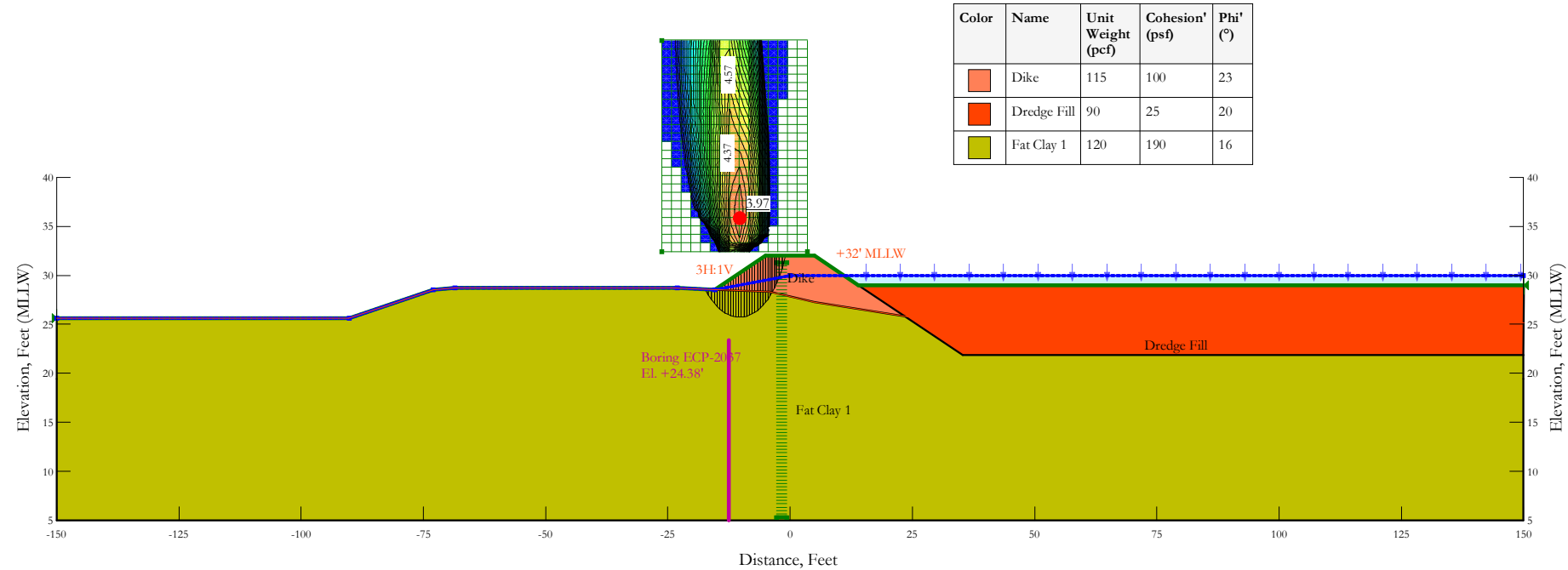
Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 70+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2037

Loading Condition: Short Term - Interior
Slip Surface: Block



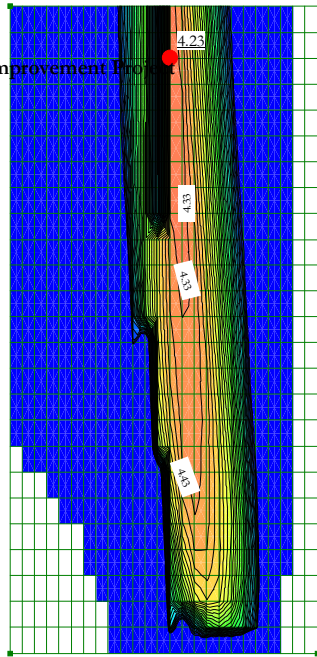
Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 70+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2037

Loading Condition: Long Term - Exterior
Slip Surface: Circular

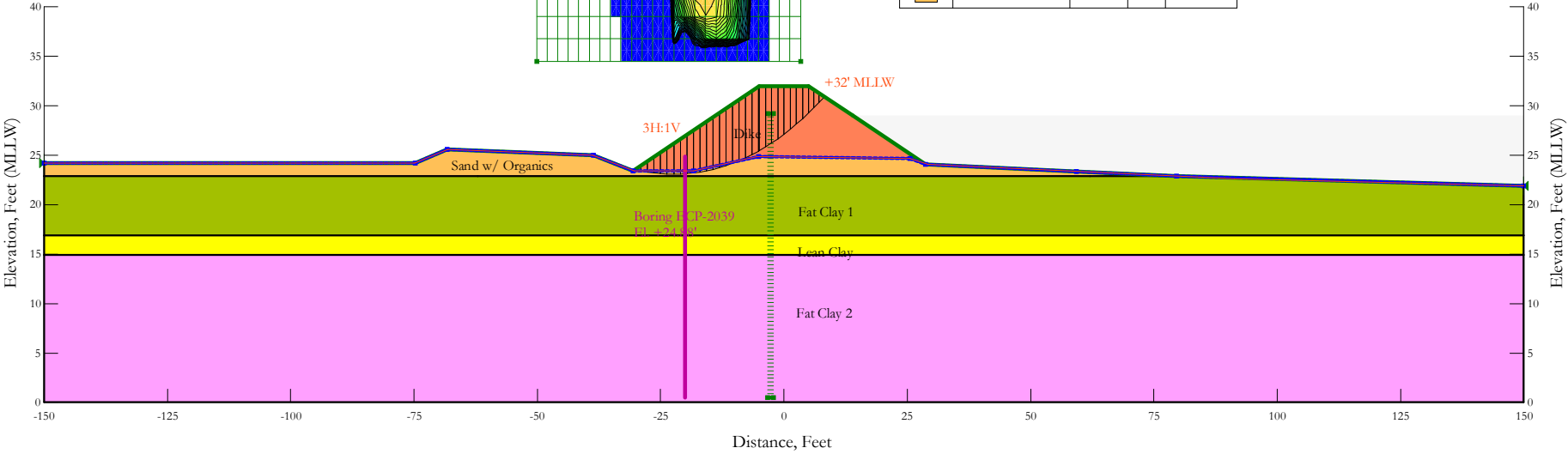


Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 74+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2039

Loading Condition: Short Term - Exterior
Slip Surface: Circular



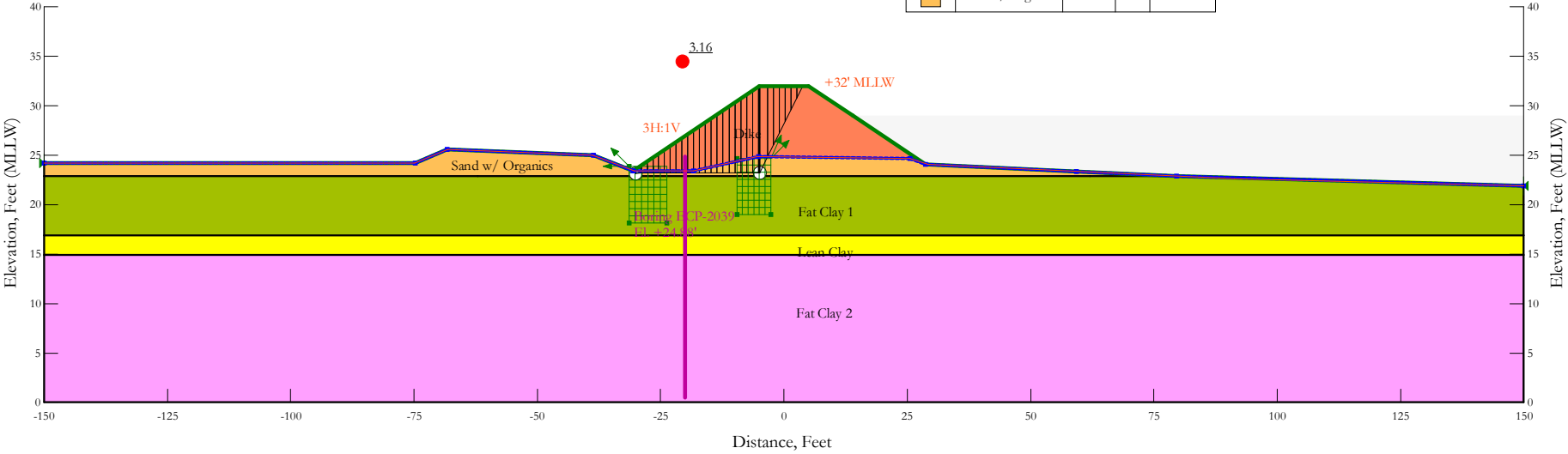
Color	Name	Unit Weight (pcf)	Phi' (°)	Cohesion (psf)
■	Dike (U)	115		600
■	Fat Clay 1 (U)	125		1,600
■	Fat Clay 2 (U)	120		1,540
■	Lean Clay (U)	125		1,340
■	Sand w/ Organics	110	22	



Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 74+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2039

Loading Condition: Short Term - Exterior
Slip Surface: Block

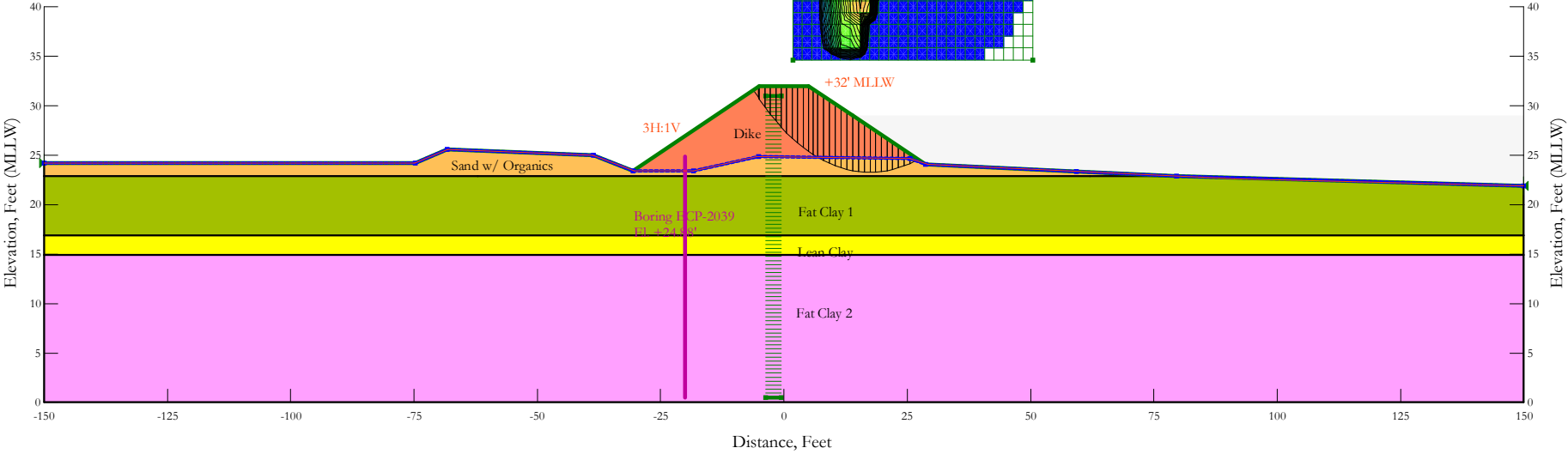
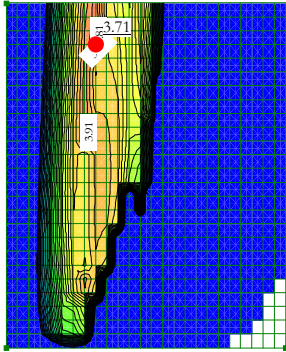
Color	Name	Unit Weight (pcf)	Phi' (°)	Cohesion (psf)
	Dike (U)	115		600
	Fat Clay 1 (U)	125		1,600
	Fat Clay 2 (U)	120		1,540
	Lean Clay (U)	125		1,340
	Sand w/ Organics	110	22	



Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 74+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2039

Loading Condition: Short Term - Interior
Slip Surface: Circular

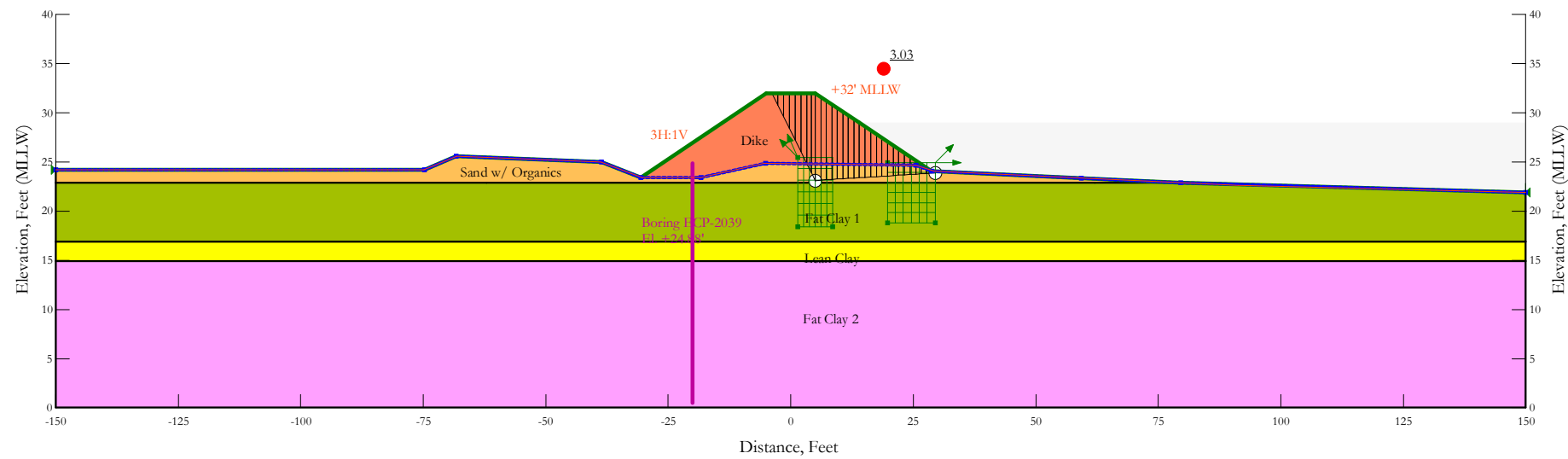
Color	Name	Unit Weight (pcf)	Phi' (°)	Cohesion (psf)
	Dike (U)	115		600
	Fat Clay 1(U)	125		1,600
	Fat Clay 2(U)	120		1,540
	Lean Clay (U)	125		1,340
	Sand w/ Organics	110	22	



Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 74+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2039

Loading Condition: Short Term - Interior
Slip Surface: Block

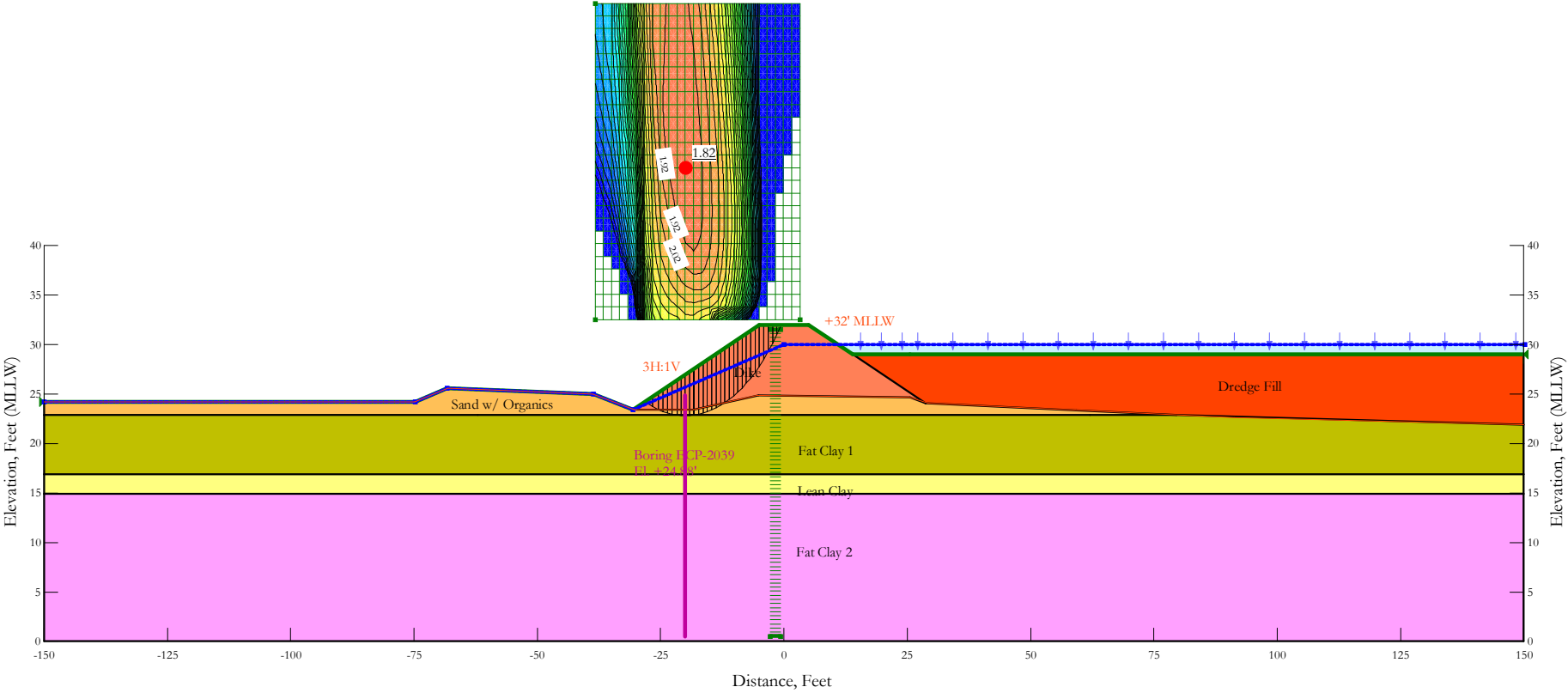
Color	Name	Unit Weight (pcf)	Phi' (°)	Cohesion (psf)
	Dike (U)	115		600
	Fat Clay 1 (U)	125		1,600
	Fat Clay 2 (U)	120		1,540
	Lean Clay (U)	125		1,340
	Sand w/ Organics	110	22	



Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 74+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2039

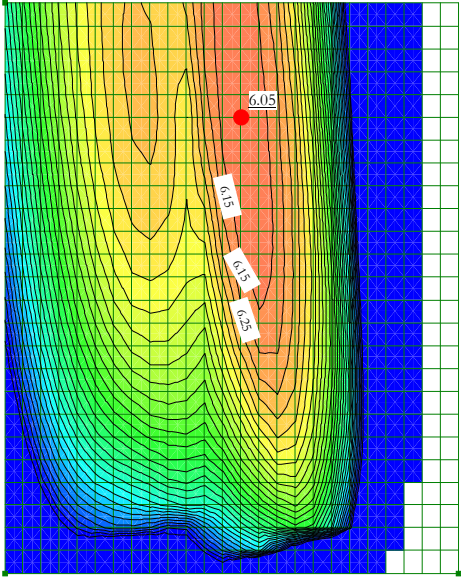
Loading Condition: Long Term - Exterior
Slip Surface: Circular

Color	Name	Unit Weight (pcf)	Cohesion' (psf)	Phi' (°)
	Dike	115	100	23
	Dredge Fill	90	25	20
	Fat Clay 1	125	190	16
	Fat Clay 2	120	190	16
	Lean Clay	125	370	17
	Sand w/ Organics	110	0	22

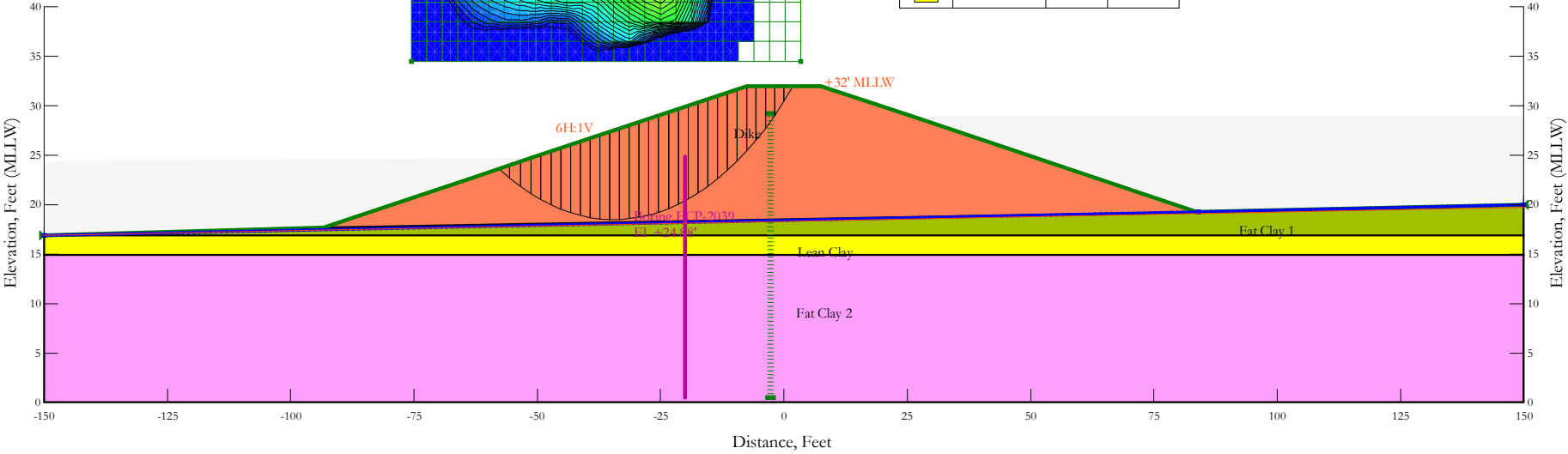


Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 87+18
HVJ Project Number: HG1910092.2.1
Boring ECP-2039

Loading Condition: Short Term - Exterior
Slip Surface: Circular



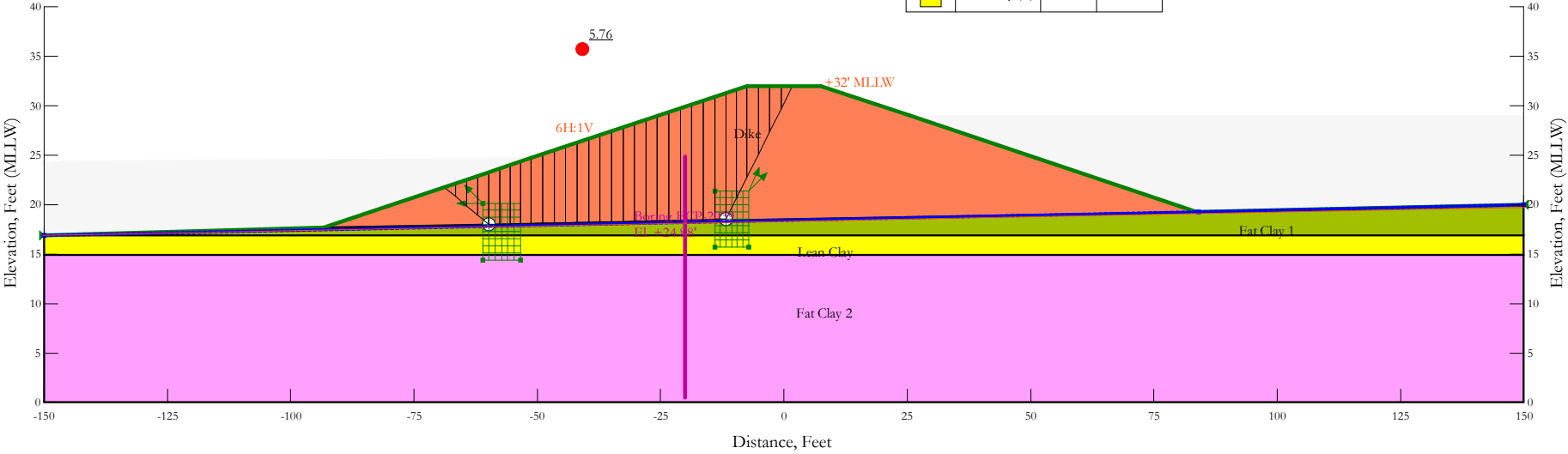
Color	Name	Unit Weight (pcf)	Cohesion (psf)
■	Dike (U)	115	600
■	Fat Clay 1(U)	125	1,600
■	Fat Clay 2(U)	120	1,540
■	Lean Clay (U)	125	1,340



Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 87+18
HVJ Project Number: HG1910092.2.1
Boring ECP-2039

Loading Condition: Short Term - Exterior
Slip Surface: Block

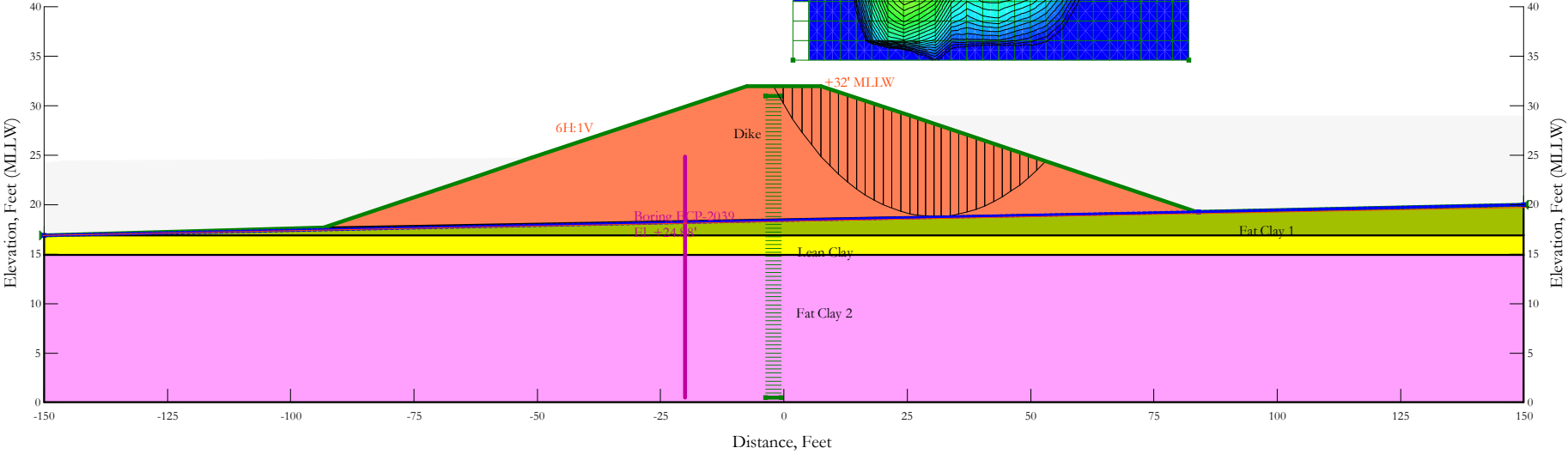
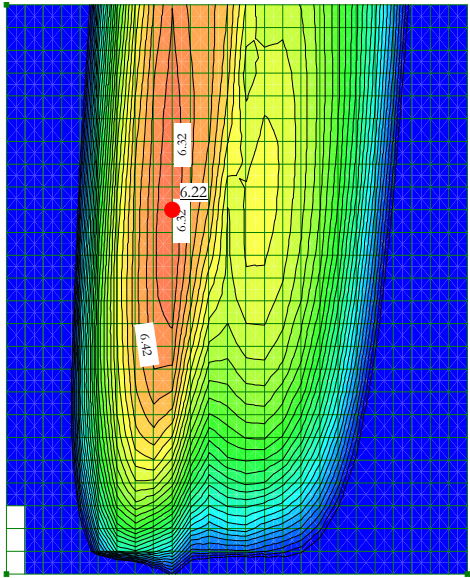
Color	Name	Unit Weight (pcf)	Cohesion (psf)
	Dike (U)	115	600
	Fat Clay 1 (U)	125	1,600
	Fat Clay 2 (U)	120	1,540
	Lean Clay (U)	125	1,340



Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 87+18
HVJ Project Number: HG1910092.2.1
Boring ECP-2039

Loading Condition: Short Term - Interior
Slip Surface: Circular

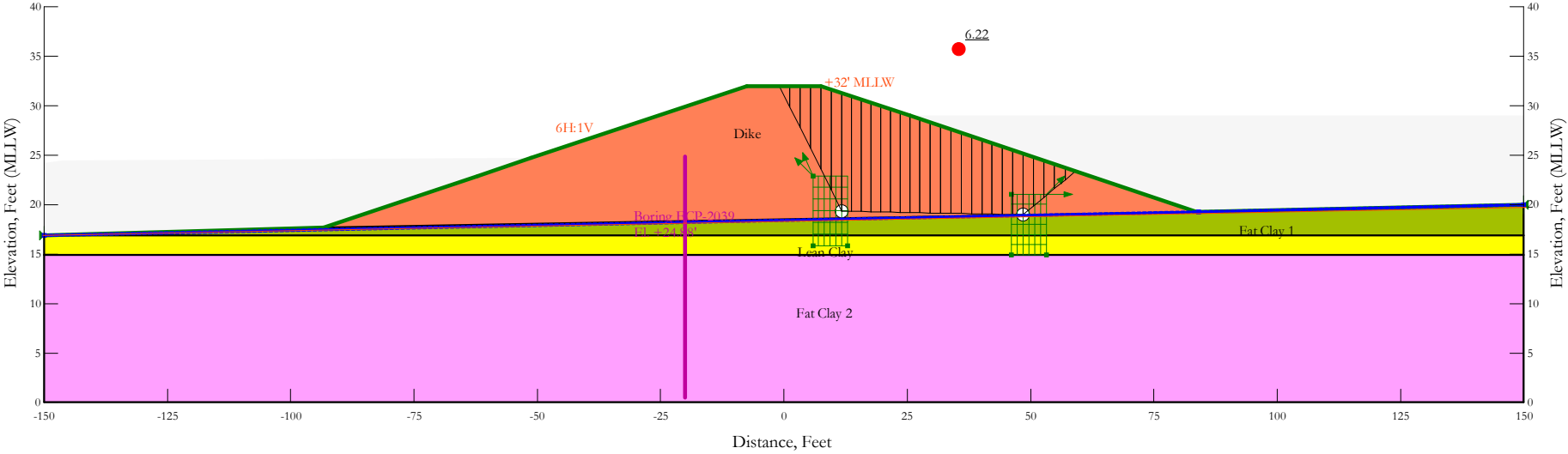
Color	Name	Unit Weight (pcf)	Cohesion (psf)
	Dike (U)	115	600
	Fat Clay 1 (U)	125	1,600
	Fat Clay 2 (U)	120	1,540
	Lean Clay (U)	125	1,340



Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 87+18
HVJ Project Number: HG1910092.2.1
Boring ECP-2039

Loading Condition: Short Term - Interior
Slip Surface: Block

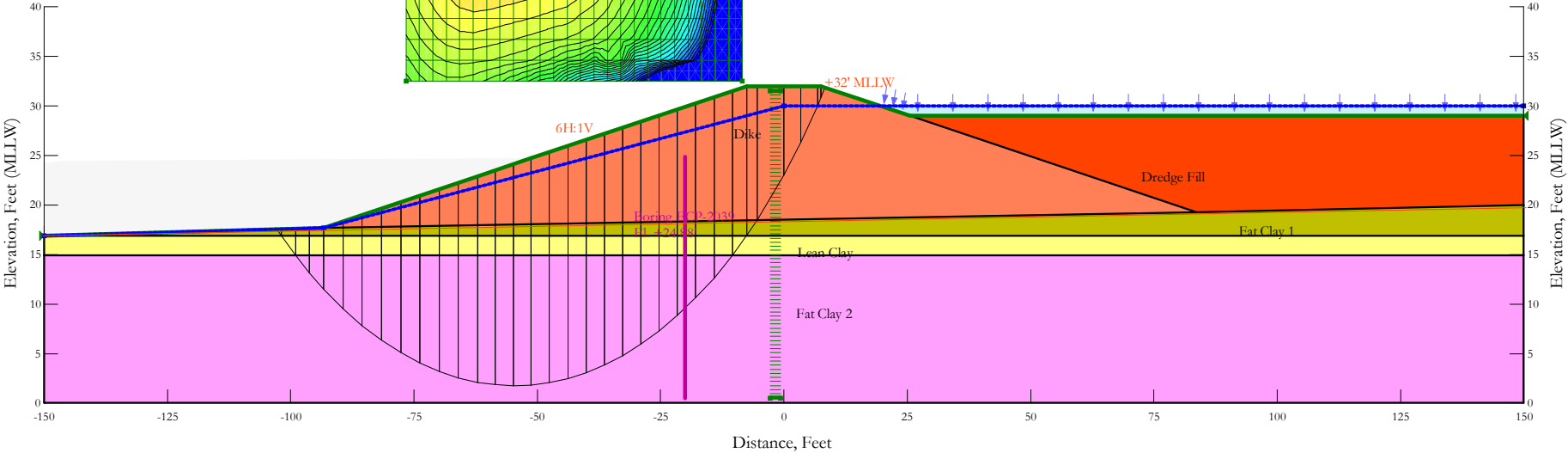
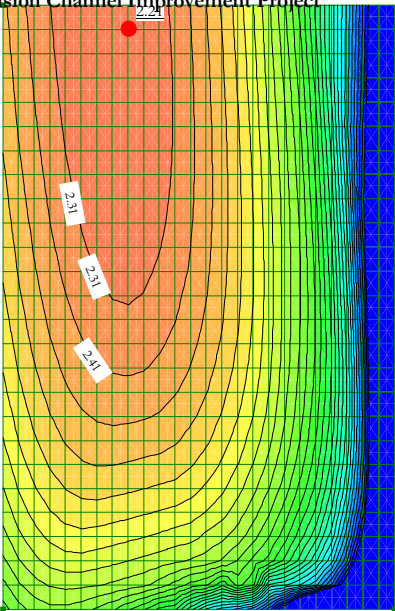
Color	Name	Unit Weight (pcf)	Cohesion (psf)
Orange	Dike (U)	115	600
Green	Fat Clay 1 (U)	125	1,600
Pink	Fat Clay 2 (U)	120	1,540
Yellow	Lean Clay (U)	125	1,340



Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 87+18
HVJ Project Number: HG1910092.2.1
Boring ECP-2039

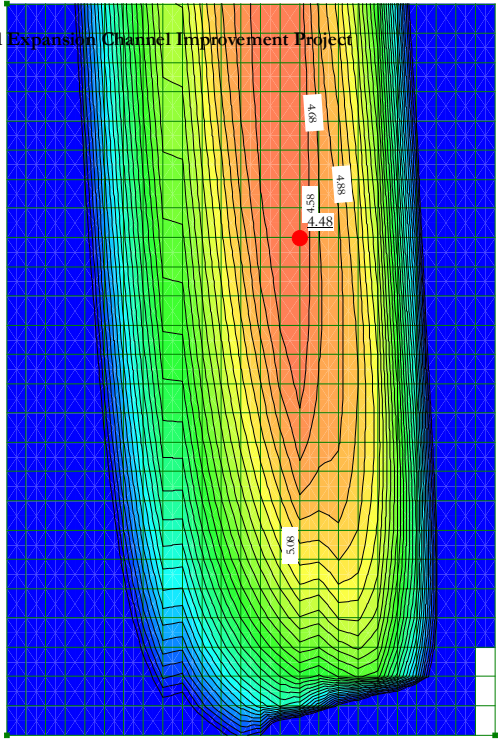
Loading Condition: Long Term - Exterior
Slip Surface: Circular

Color	Name	Unit Weight (pcf)	Cohesion' (psf)	Phi' (°)
	Dike	115	100	23
	Dredge Fill	90	25	20
	Fat Clay 1	125	190	16
	Fat Clay 2	120	190	16
	Lean Clay	125	370	17

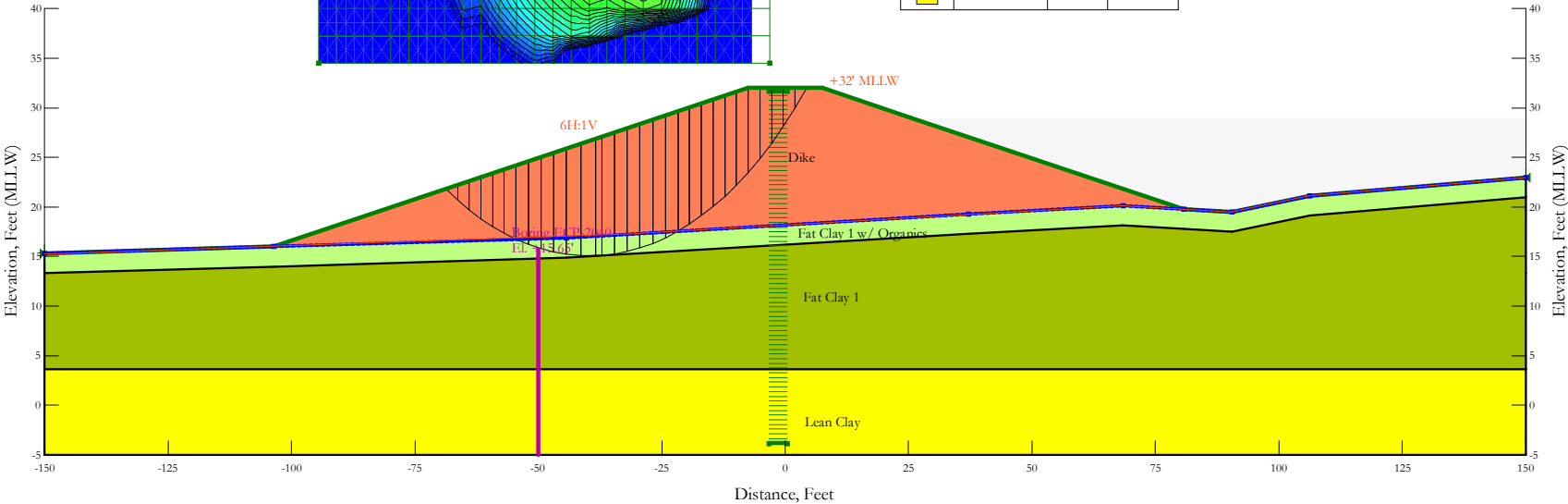


Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 92+00
HVJ Project Number: HG1910092.2.1
Borings: ECP-2040 and ECP-2041

Loading Condition: Short Term - Exterior
Slip Surface: Circular



Color	Name	Unit Weight (pcf)	Cohesion (psf)
Red	Dike (U)	115	600
Light Green	Fat Clay 1 w/ Organics (U)	120	500
Dark Green	Fat Clay 1(U)	120	1,840
Yellow	Lean Clay (U)	125	2,400



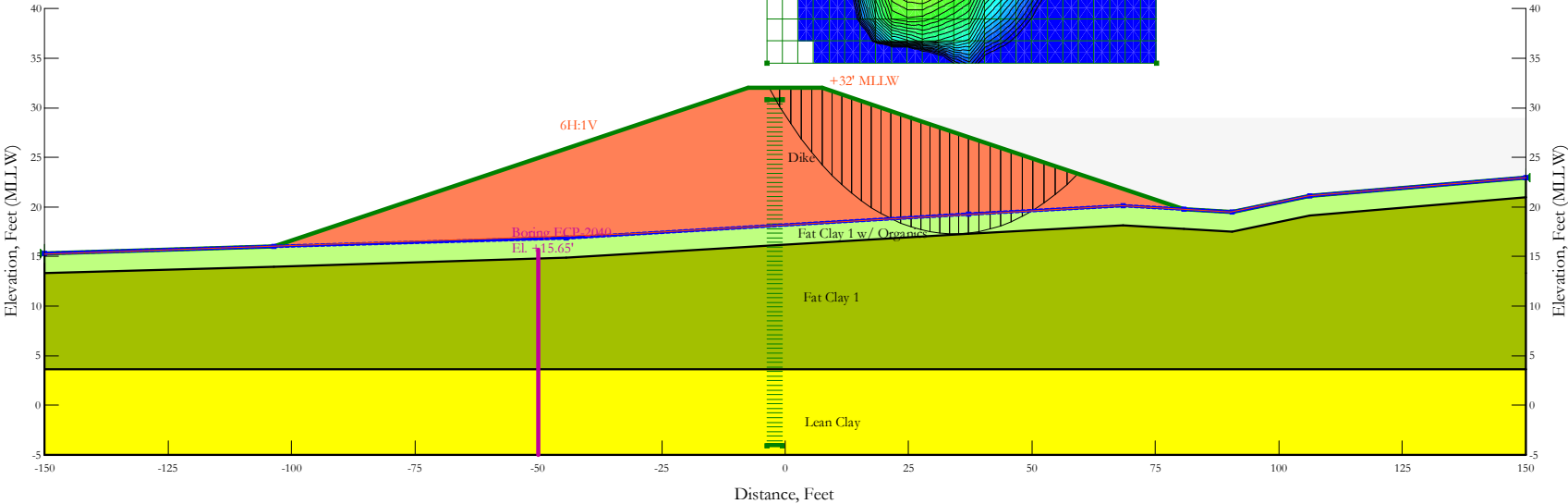
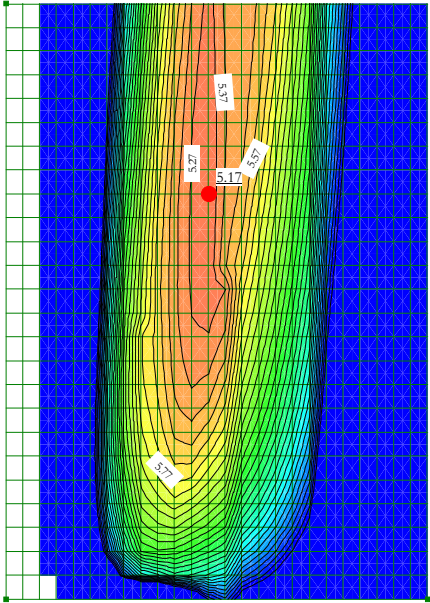
Loading Condition: Short Term - Exterior
 Slip Surface: Block

Figure 1 is a cross-section diagram showing the proposed dike and existing ground conditions. The x-axis represents Distance, Feet, ranging from -150 to 150. The y-axis represents Elevation, Feet (MLLW), ranging from -5 to 40. The diagram includes a legend at the top right identifying soil types: Lean Clay (C) in yellow, Fat Clay 1 in green, and Fat Clay 1 w/ Organics in light green. The proposed dike is shown in orange with a 6H:1V slope. A red dot indicates a water level at 4.19 feet. A purple line indicates the proposed dike crest at +32' MLLW. A vertical pink line is at -50 feet. The existing ground is shown in yellow (Lean Clay), green (Fat Clay 1), and light green (Fat Clay 1 w/ Organics). The diagram also shows a 'Dike' label and a 'Proposed Elevation' label.

Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 92+00
HVJ Project Number: HG1910092.2.1
Borings: ECP-2040 and ECP-2041

Loading Condition: Short Term - Interior
Slip Surface: Circular

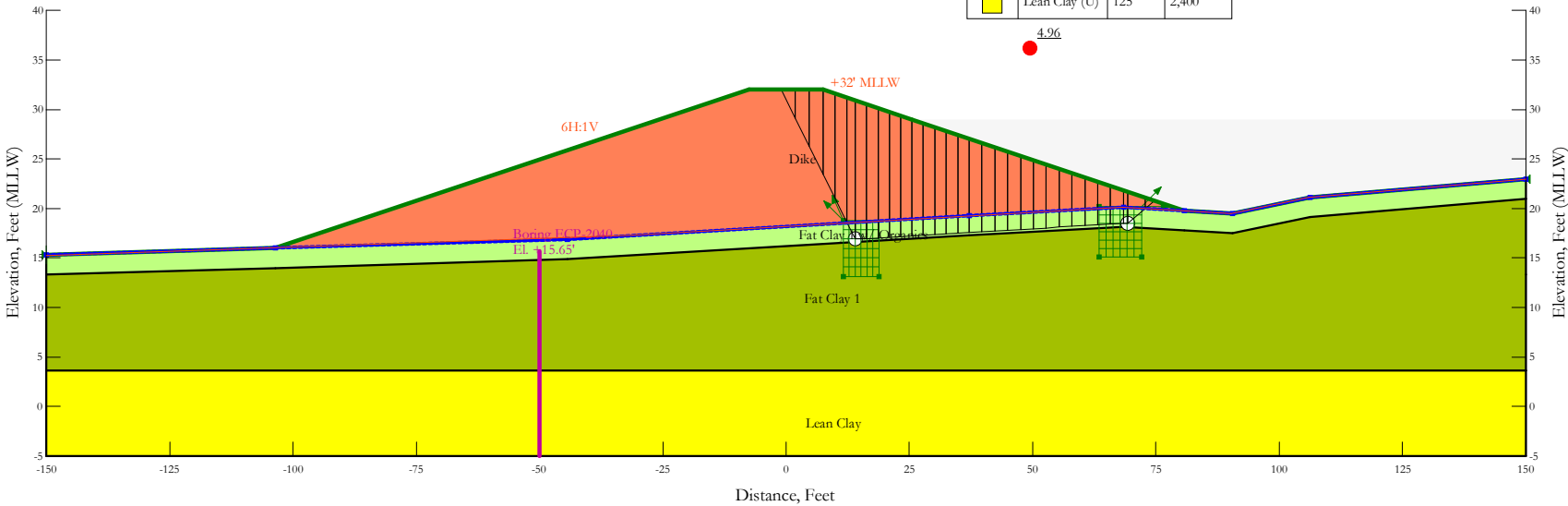
Color	Name	Unit Weight (pcf)	Cohesion (psf)
Orange	Dike (U)	115	600
Light Green	Fat Clay 1 w/ Organics (U)	120	500
Dark Green	Fat Clay 1 (U)	120	1,840
Yellow	Lean Clay (U)	125	2,400



Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 92+00
HVJ Project Number: HG1910092.2.1
Borings: ECP-2040 and ECP-2041

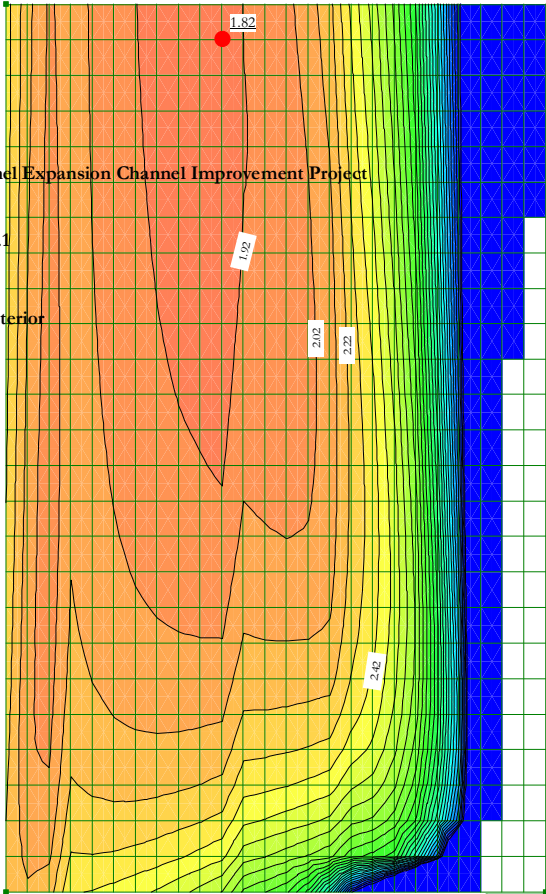
Loading Condition: Short Term - Interior
Slip Surface: Block

Color	Name	Unit Weight (pcf)	Cohesion (psf)
	Dike (U)	115	600
	Fat Clay 1 w/ Organics (U)	120	500
	Fat Clay 1 (U)	120	1,840
	Lean Clay (U)	125	2,400

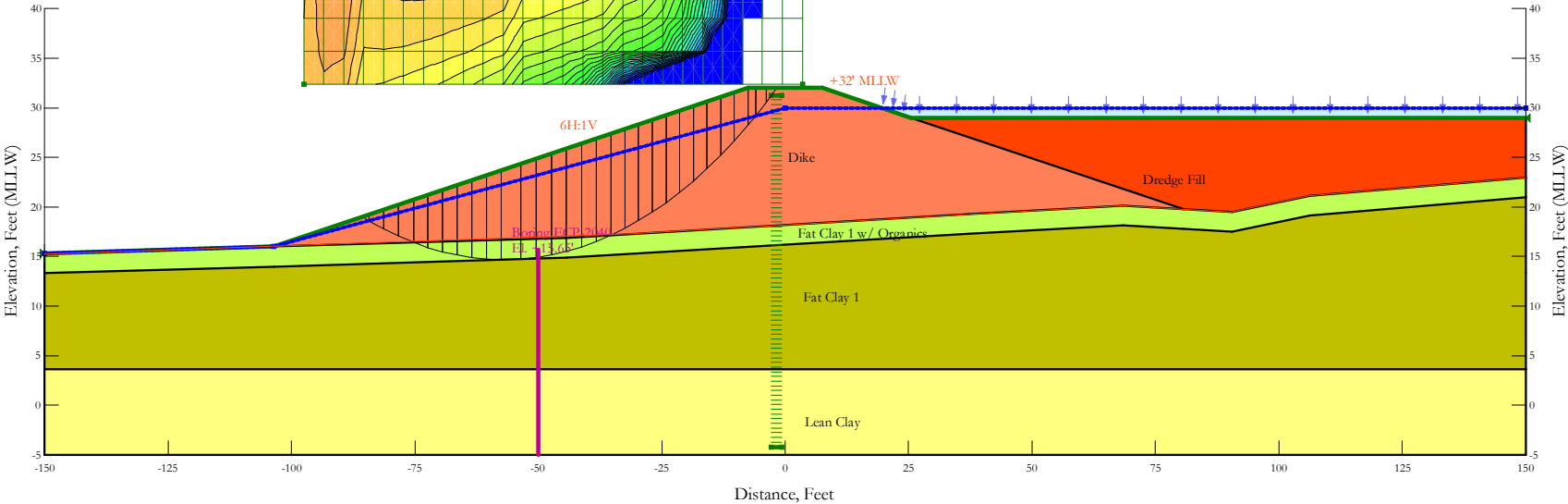


Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 92+00
HVJ Project Number: HG1910092.2.1
Borings: ECP-2040 and ECP-2041

Loading Condition: Long Term - Exterior
Slip Surface: Circular



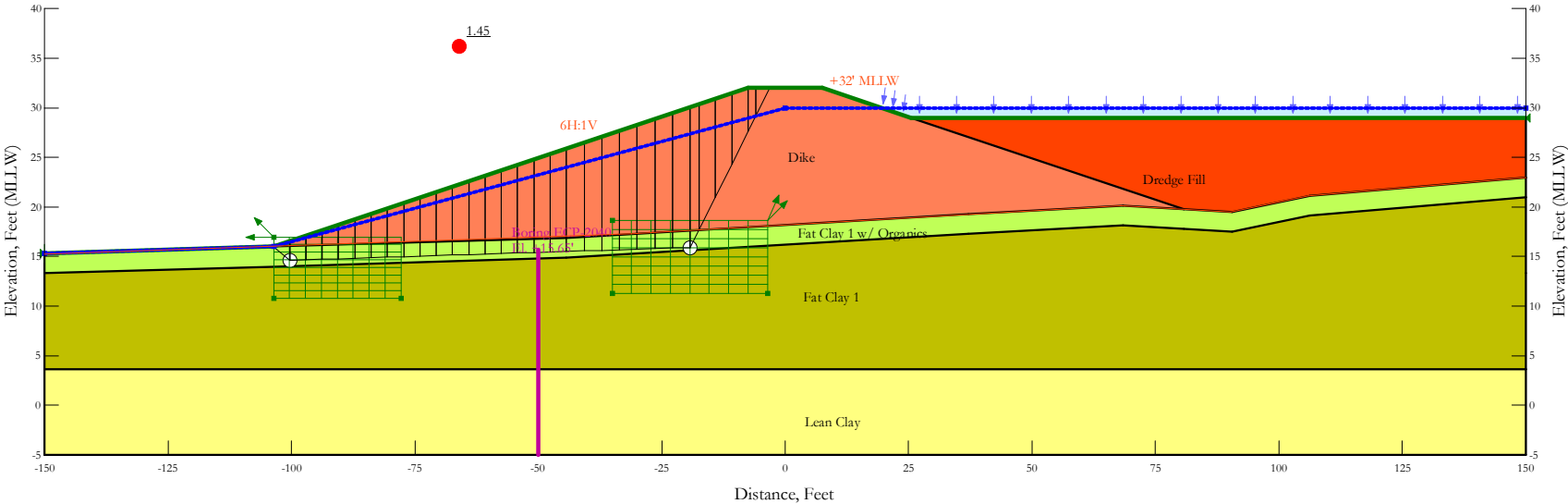
Color	Name	Unit Weight (pcf)	Cohesion' (psf)	Phi' (°)
	Dike	115	100	23
	Dredge Fill	90	25	20
	Fat Clay 1	120	190	16
	Fat Clay 1 w/ Organics	120	20	14
	Lean Clay	125	370	17



Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 92+00
HVJ Project Number: HG1910092.2.1
Borings: ECP-2040 and ECP-2041

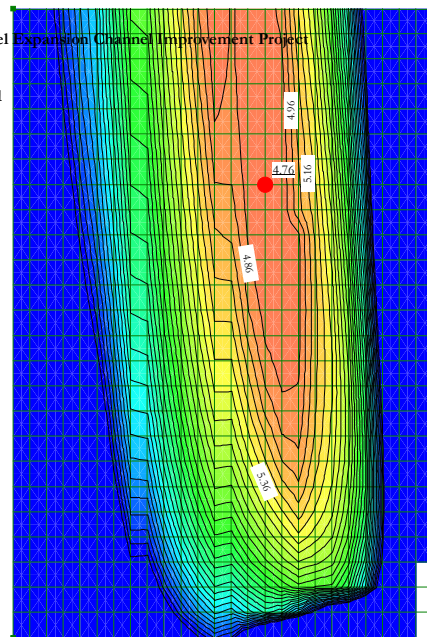
Loading Condition: Long Term - Exterior
Slip Surface: Circular

Color	Name	Unit Weight (pcf)	Cohesion' (psf)	Phi' (°)
	Dike	115	100	23
	Dredge Fill	90	25	20
	Fat Clay 1	120	190	16
	Fat Clay 1 w/ Organics	120	20	14
	Lean Clay	125	370	17

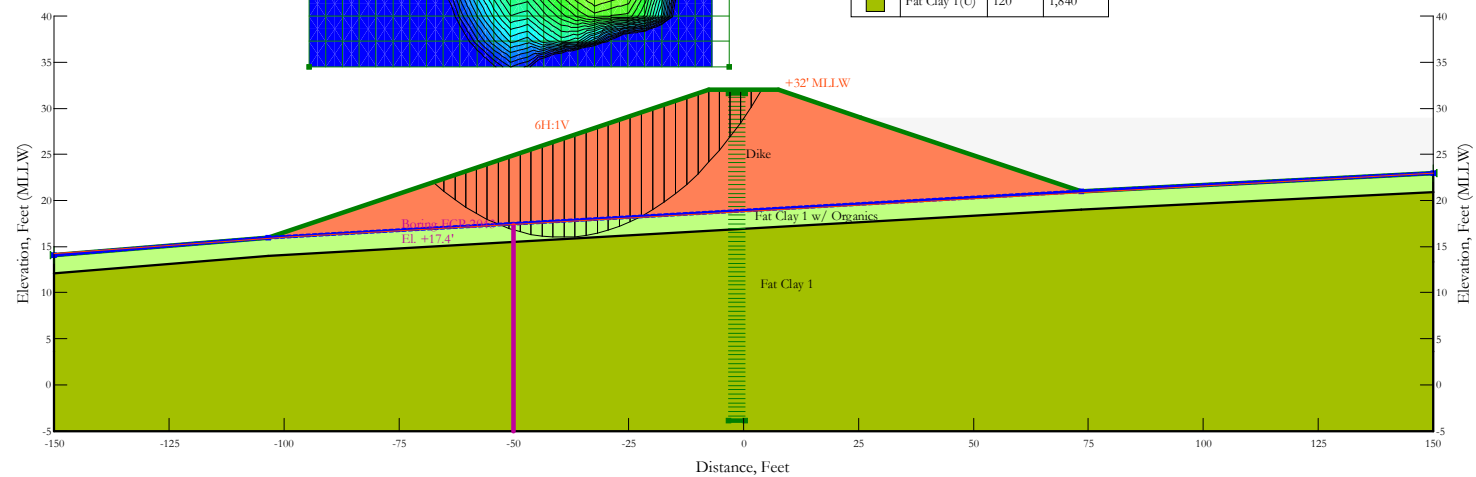


Project Name: Houston Ship Channel Expansion Channel Improvement Project
 Location: Beltway 8 Placement Area
 Station: 100+00
 HVJ Project Number: HG1910092.2.1
 Boring: ECP-2043

Loading Condition: Short Term - Exterior
 Slip Surface: Circular

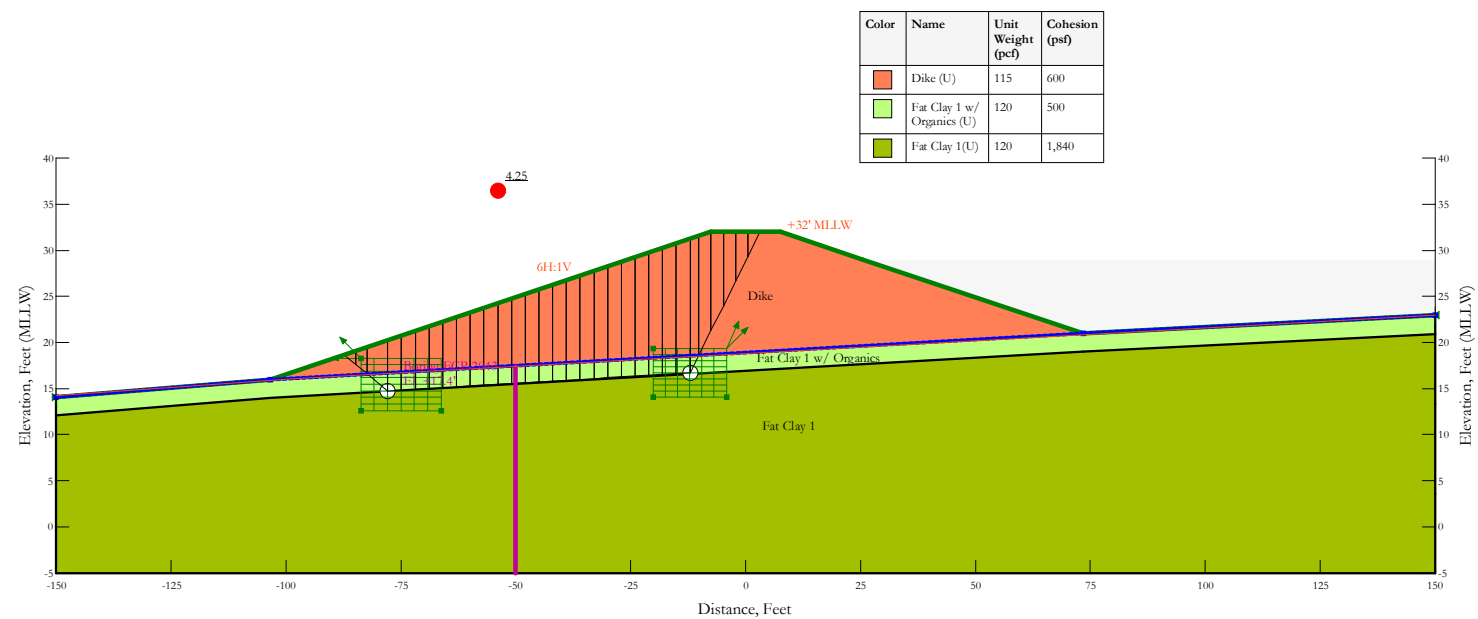


Color	Name	Unit Weight (pcf)	Cohesion (psf)
Orange	Dike (U)	115	600
Light Green	Fat Clay 1 w/ Organics (U)	120	500
Dark Green	Fat Clay 1 (U)	120	1,840



Project Name: Houston Ship Channel Expansion Channel Improvement Project
 Location: Beltway 8 Placement Area
 Station: 100+00
 HVJ Project Number: HG1910092.2.1
 Boring: ECP-2043

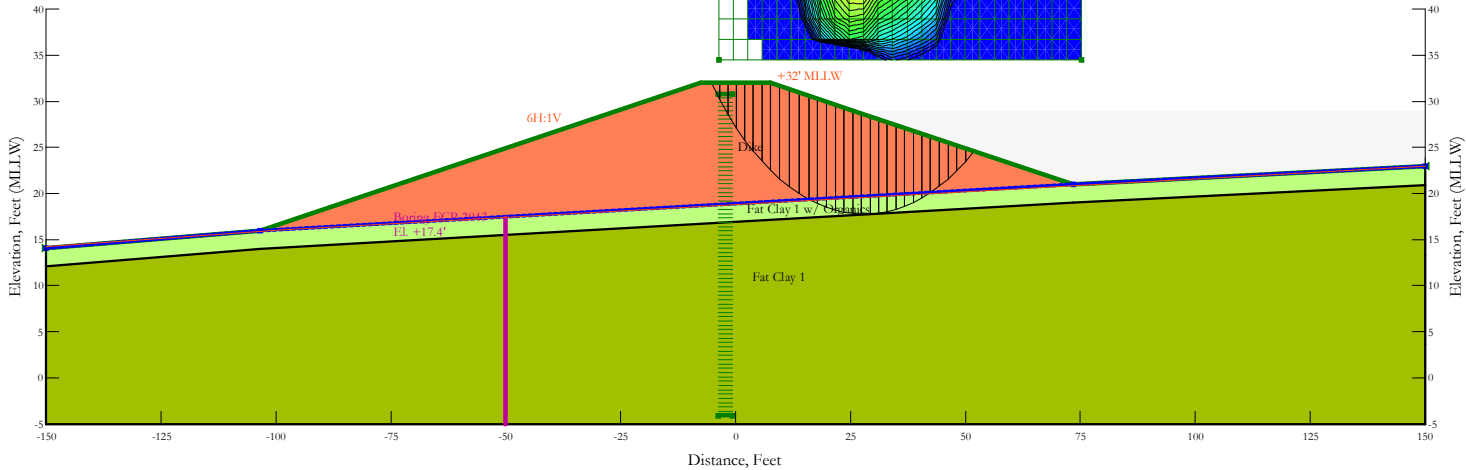
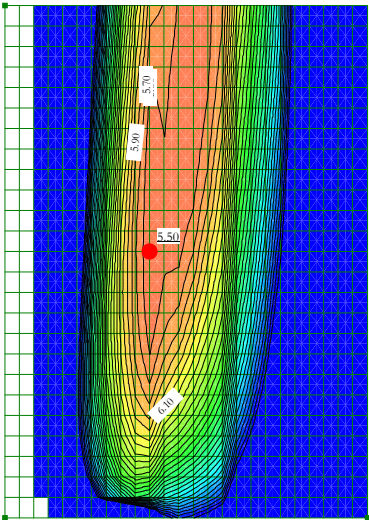
Loading Condition: Short Term - Exterior
 Slip Surface: Block



Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 100+00
HVJ Project Number: HG1910092.2.1
Boring: ECP-2043

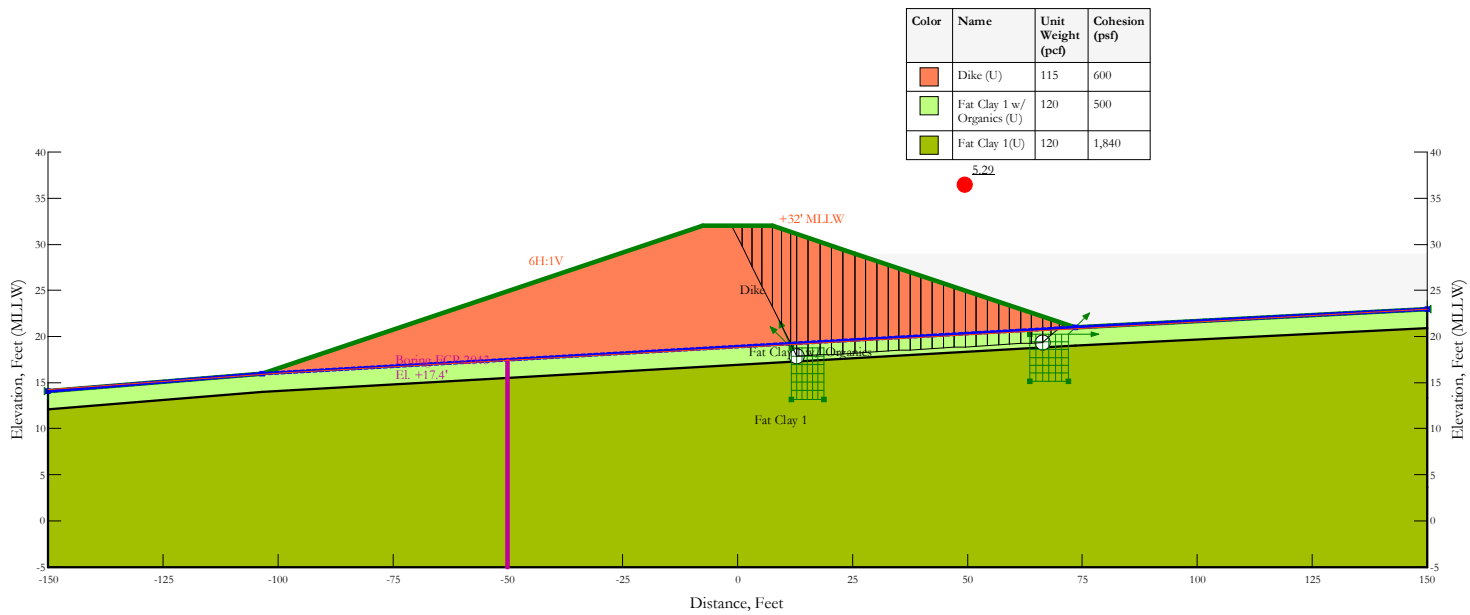
Loading Condition: Short Term - Interior
Slip Surface: Circular

Color	Name	Unit Weight (pcf)	Cohesion (psf)
Orange	Dike (U)	115	600
Light Green	Fat Clay 1 w/ Organics (U)	120	500
Dark Green	Fat Clay 1 (U)	120	1,840



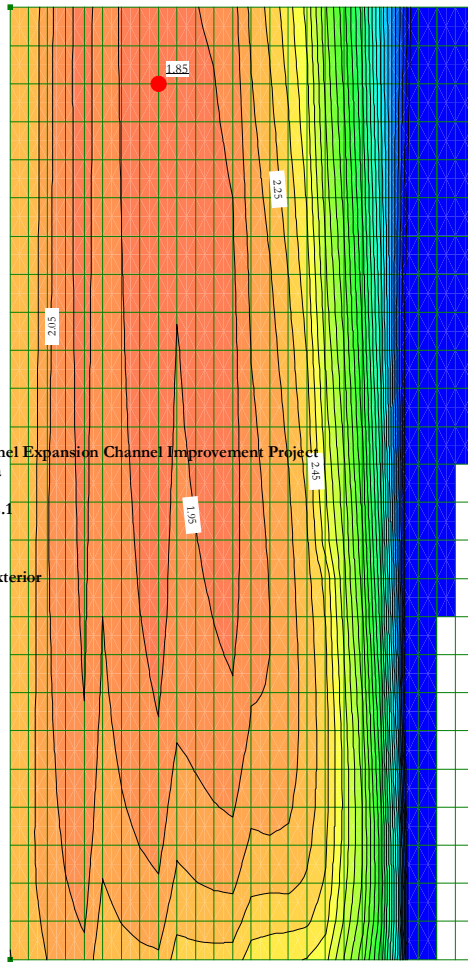
Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 100+00
HVJ Project Number: HG1910092.2.1
Boring: ECP-2043

Loading Condition: Short Term - Interior
Slip Surface: Block

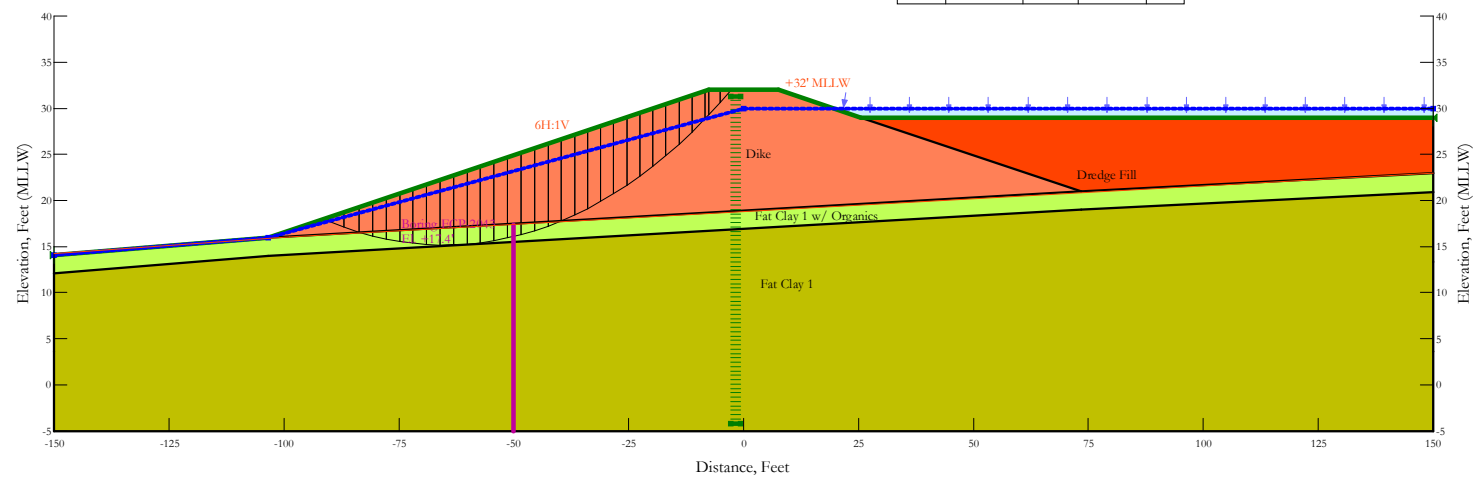


Project Name: Houston Ship Channel Expansion Channel Improvement Project
 Location: Beltway 8 Placement Area
 Station: 100+00
 HVJ Project Number: HG1910092.2.1
 Boring: ECP-2043

Loading Condition: Long Term - Exterior
 Slip Surface: Circular

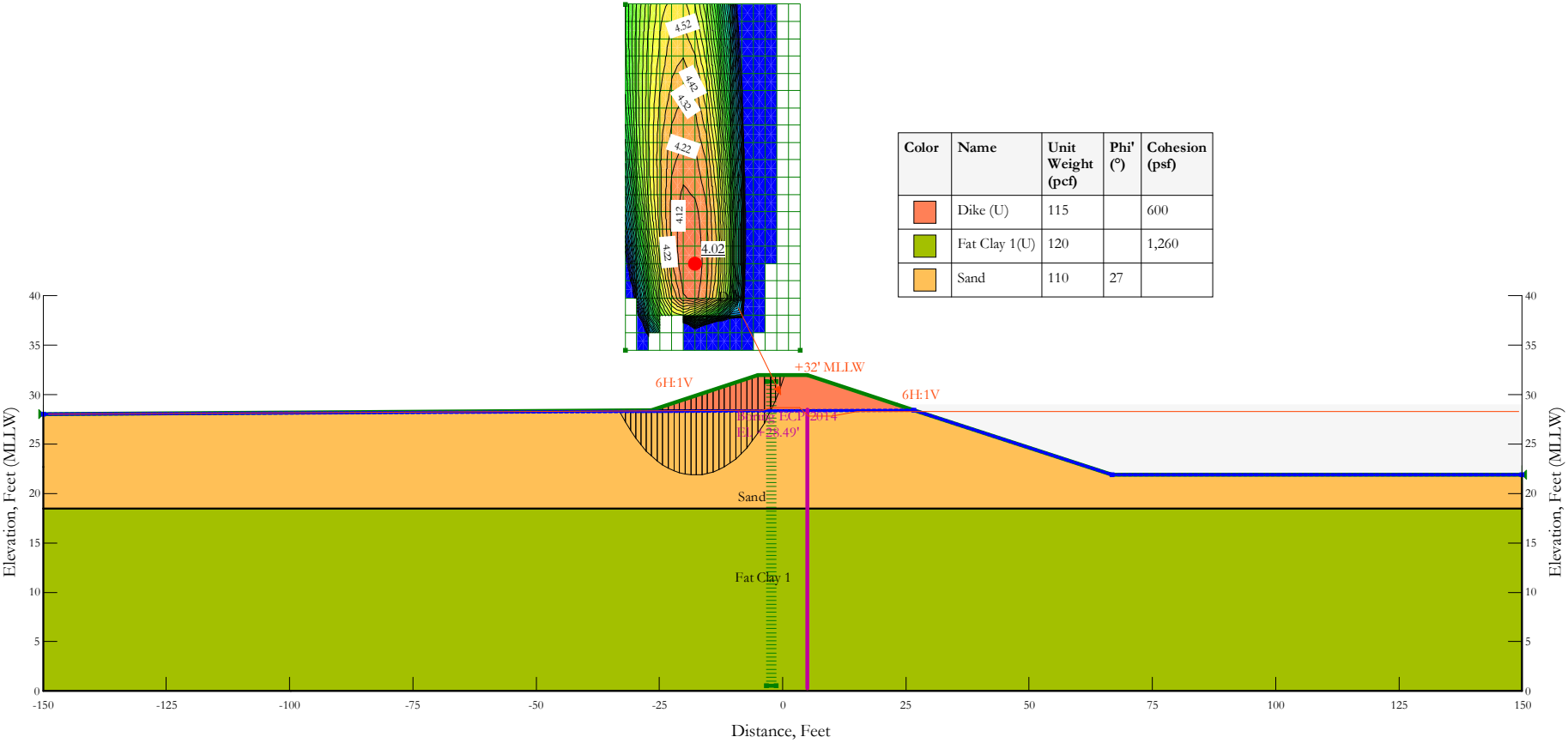


Color	Name	Unit Weight (pcf)	Cohesion' (psf)	Phi' (°)
	Dike	115	100	23
	Dredge Fill	90	25	20
	Fat Clay 1	120	190	16
	Fat Clay 1 w/ Organics	120	20	14



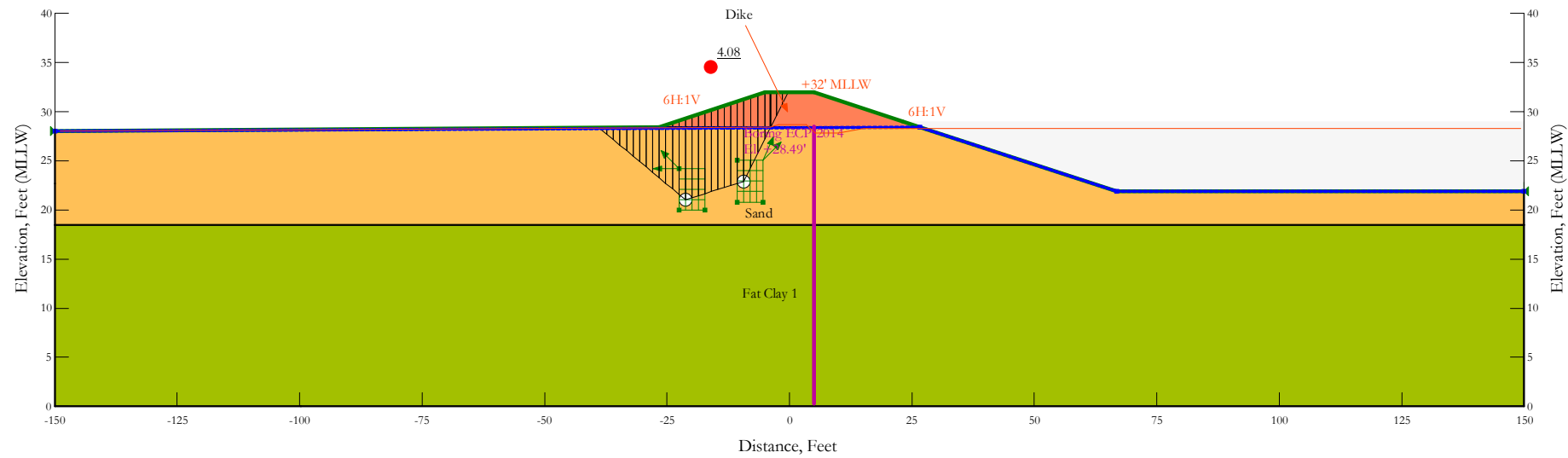
Loading Condition: Long Term - Exterior
 Slip Surface: Circular

Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 120+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2014
Loading Condition: Short Term - Exterior
Slip Surface: Circular



Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 120+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2014
Loading Condition: Short Term - Exterior
Slip Surface: Block

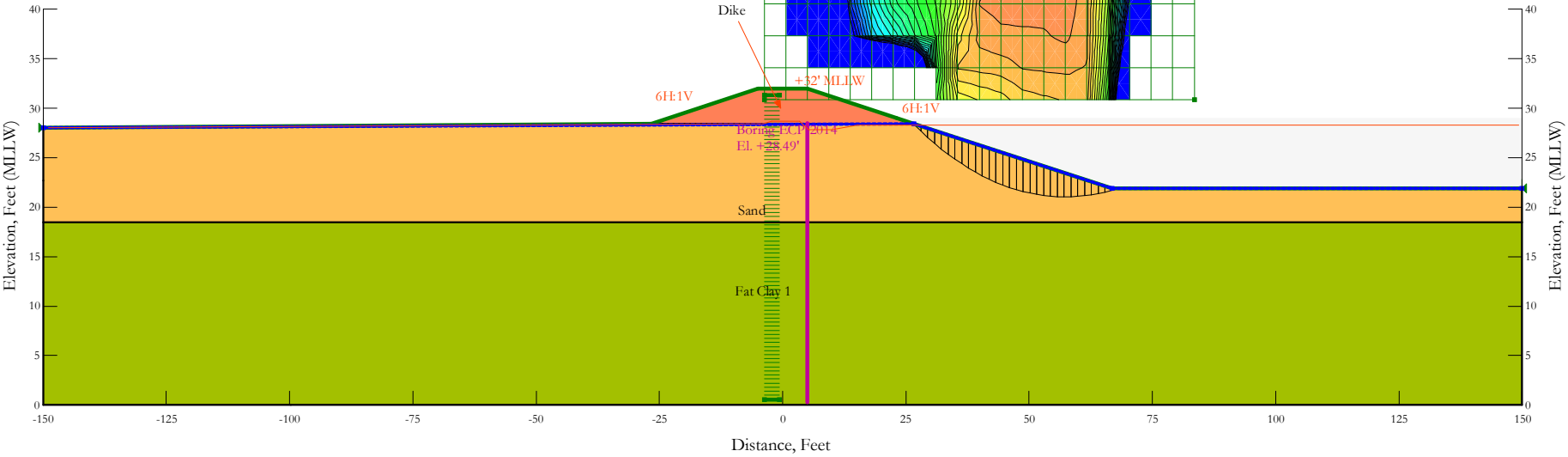
Color	Name	Unit Weight (pcf)	Phi' (°)	Cohesion (psf)
	Dike (U)	115		600
	Fat Clay 1 (U)	120		1,260
	Sand	110	27	



Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 120+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2014

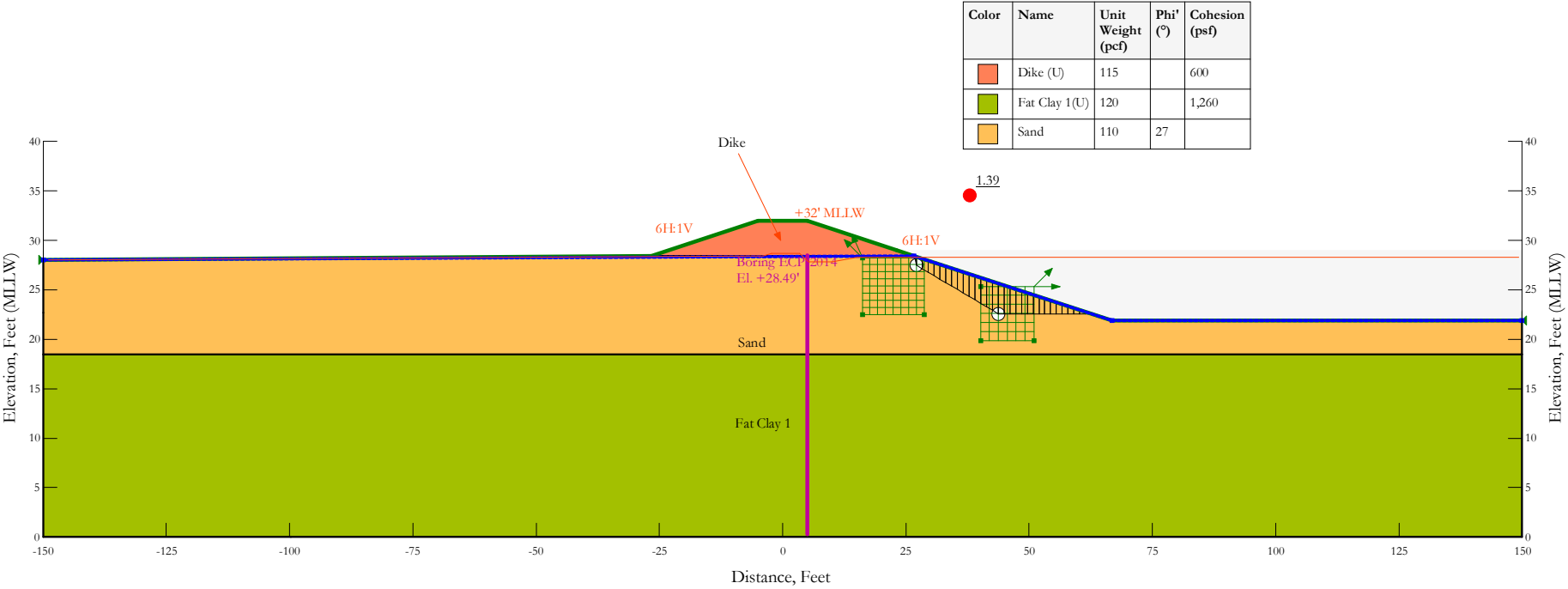
Loading Condition: Short Term - Interior
Slip Surface: Circular

Color	Name	Unit Weight (pcf)	Phi' (°)	Cohesion (psf)
Orange	Dike (U)	115		600
Green	Fat Clay 1 (U)	120		1,260
Yellow	Sand	110	27	



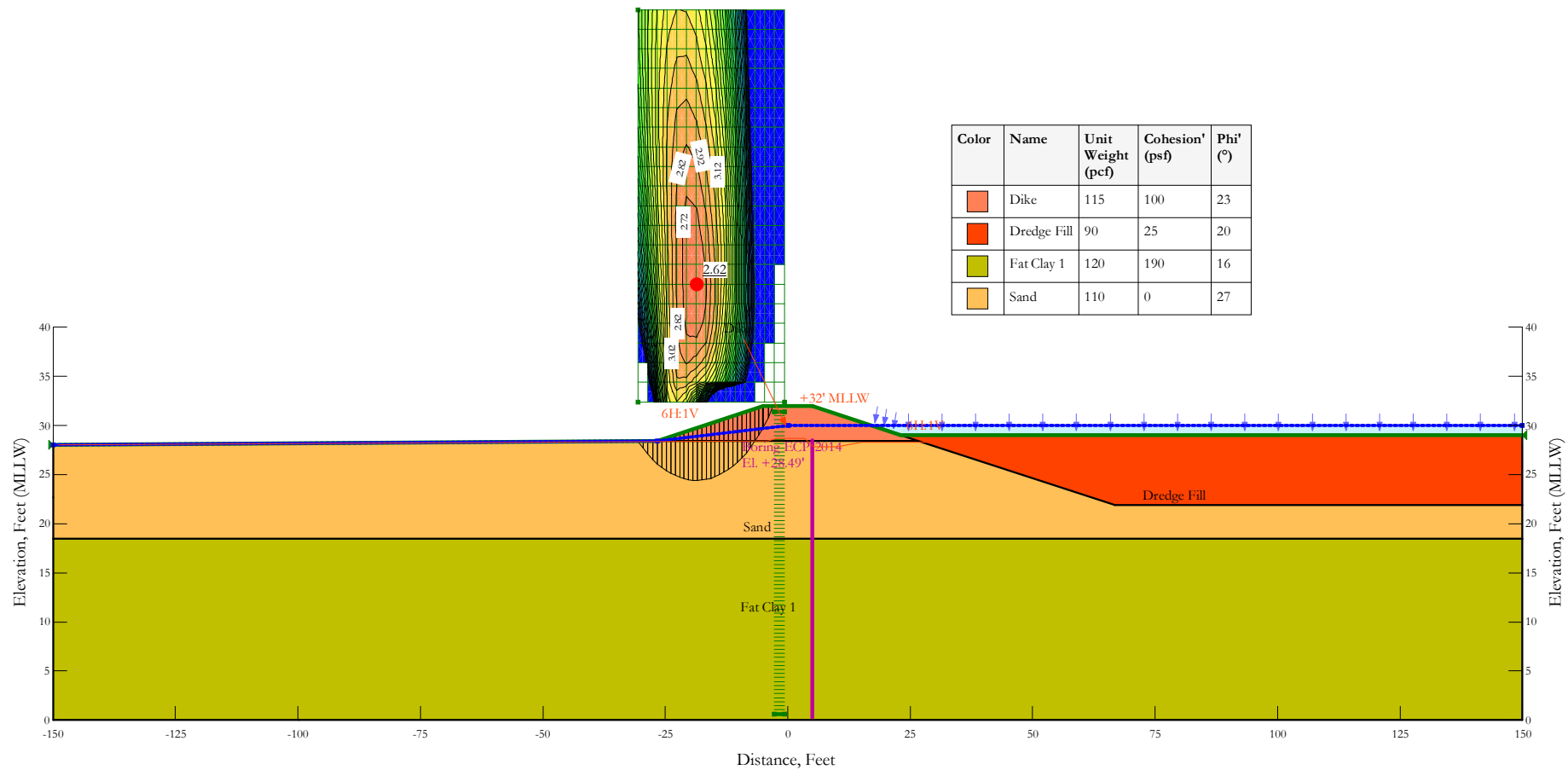
Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 120+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2014

Loading Condition: Short Term - Interior
Slip Surface: Block



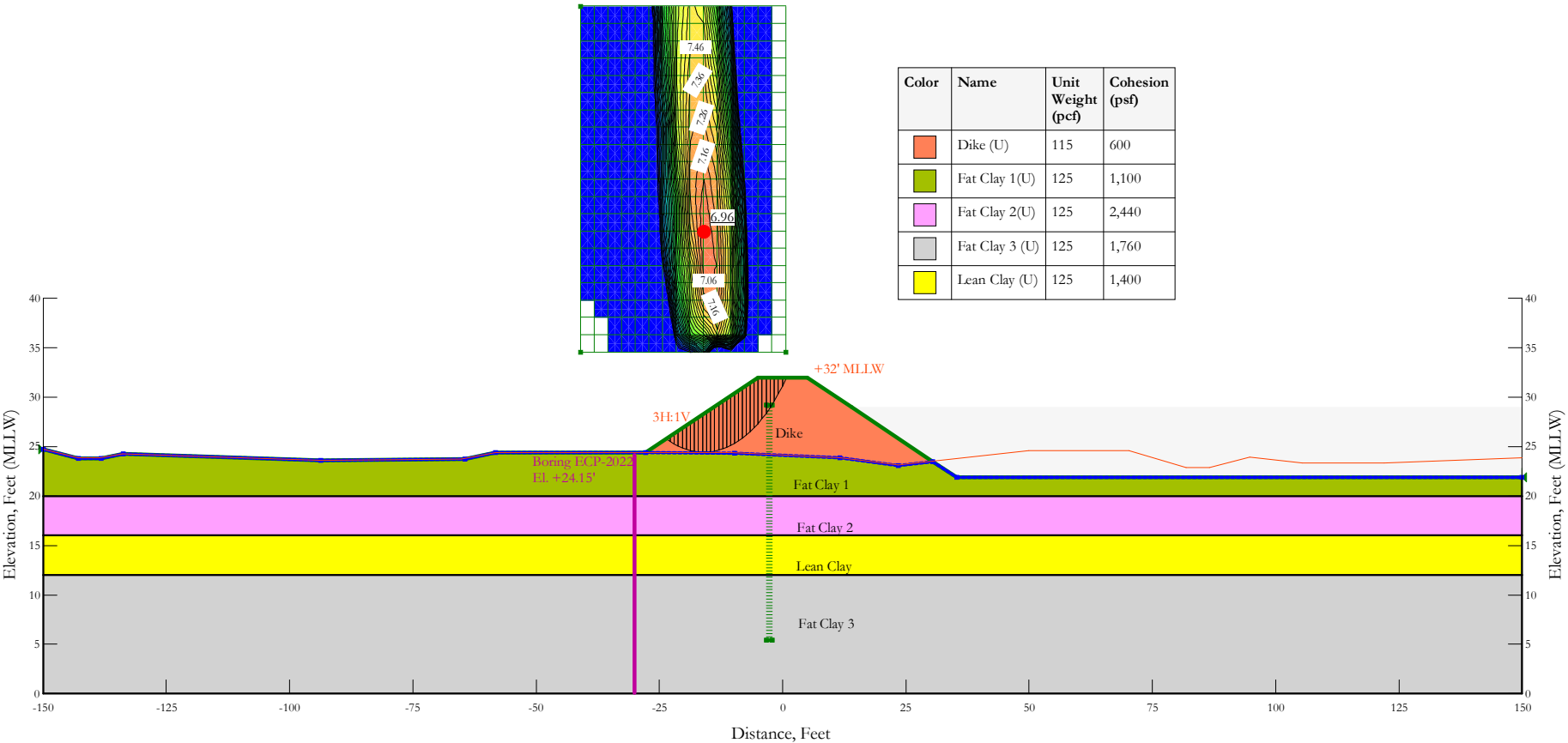
Boring ECP-2014

Slip Surface: Circular



Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 155+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2022

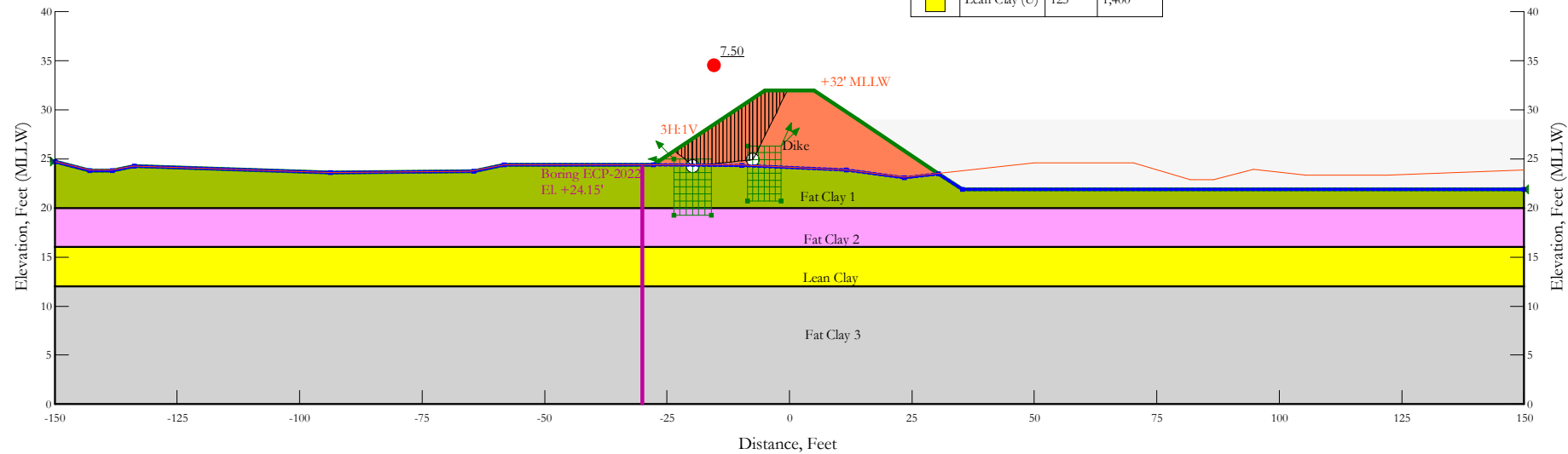
Loading Condition: Short Term - Exterior
Slip Surface: Circular



Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 155+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2022

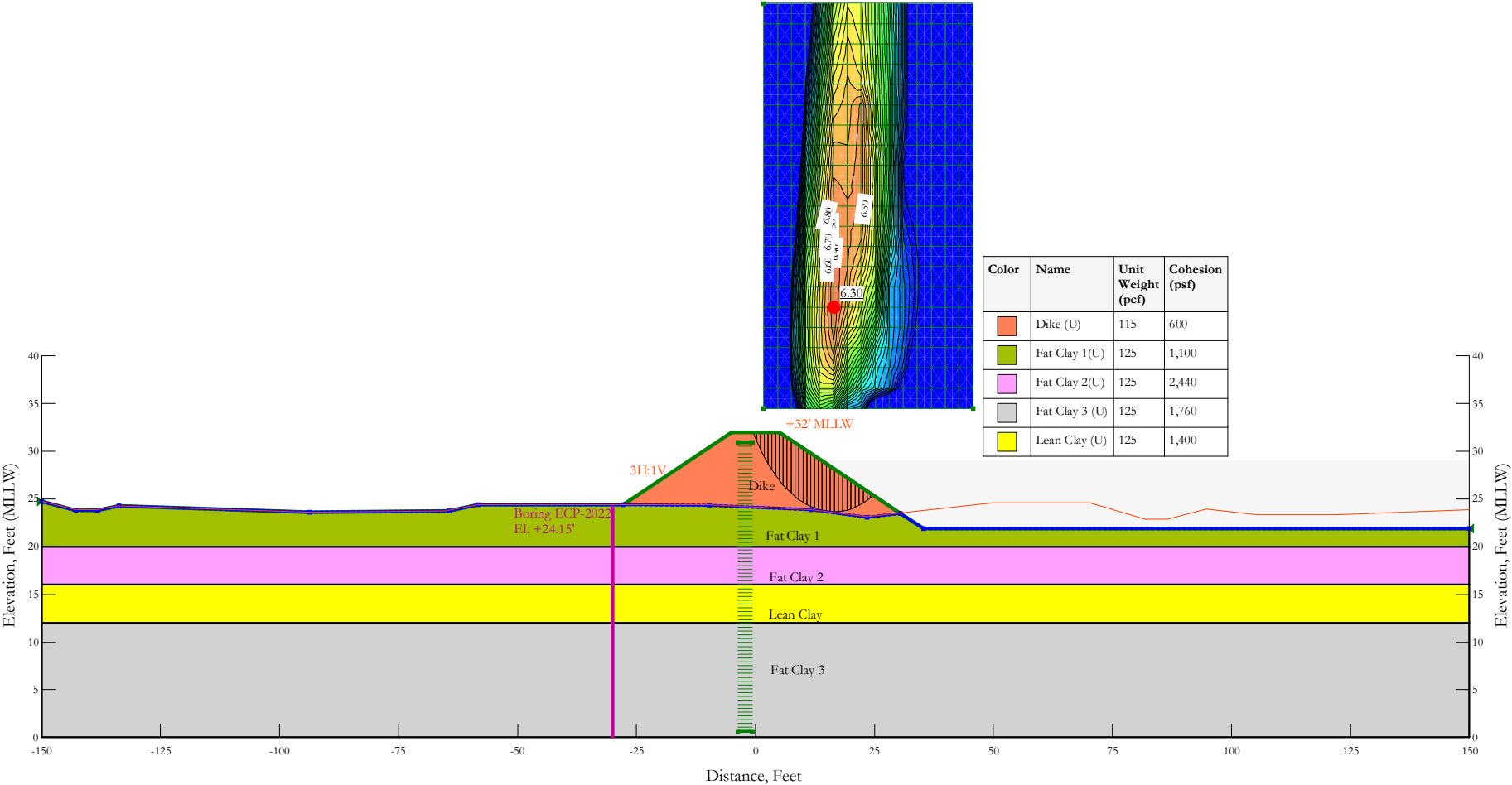
Loading Condition: Short Term - Exterior
Slip Surface: Block

Color	Name	Unit Weight (pcf)	Cohesion (psf)
	Dike (U)	115	600
	Fat Clay 1 (U)	125	1,100
	Fat Clay 2 (U)	125	2,440
	Fat Clay 3 (U)	125	1,760
	Lean Clay (U)	125	1,400



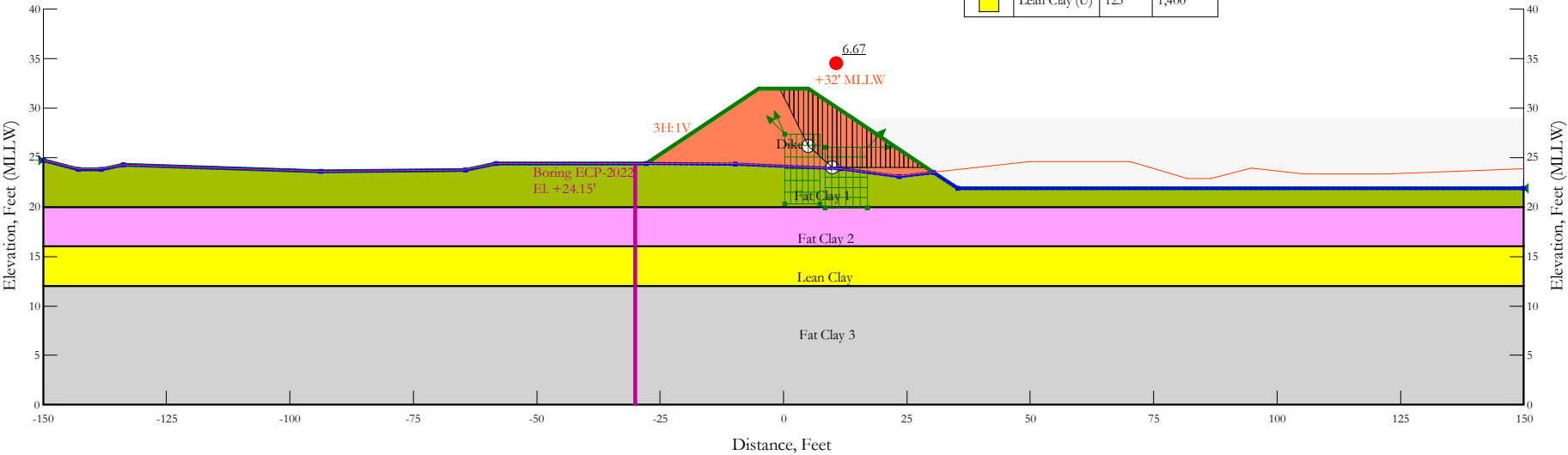
Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 155+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2022

Loading Condition: Short Term - Interior
Slip Surface: Circular

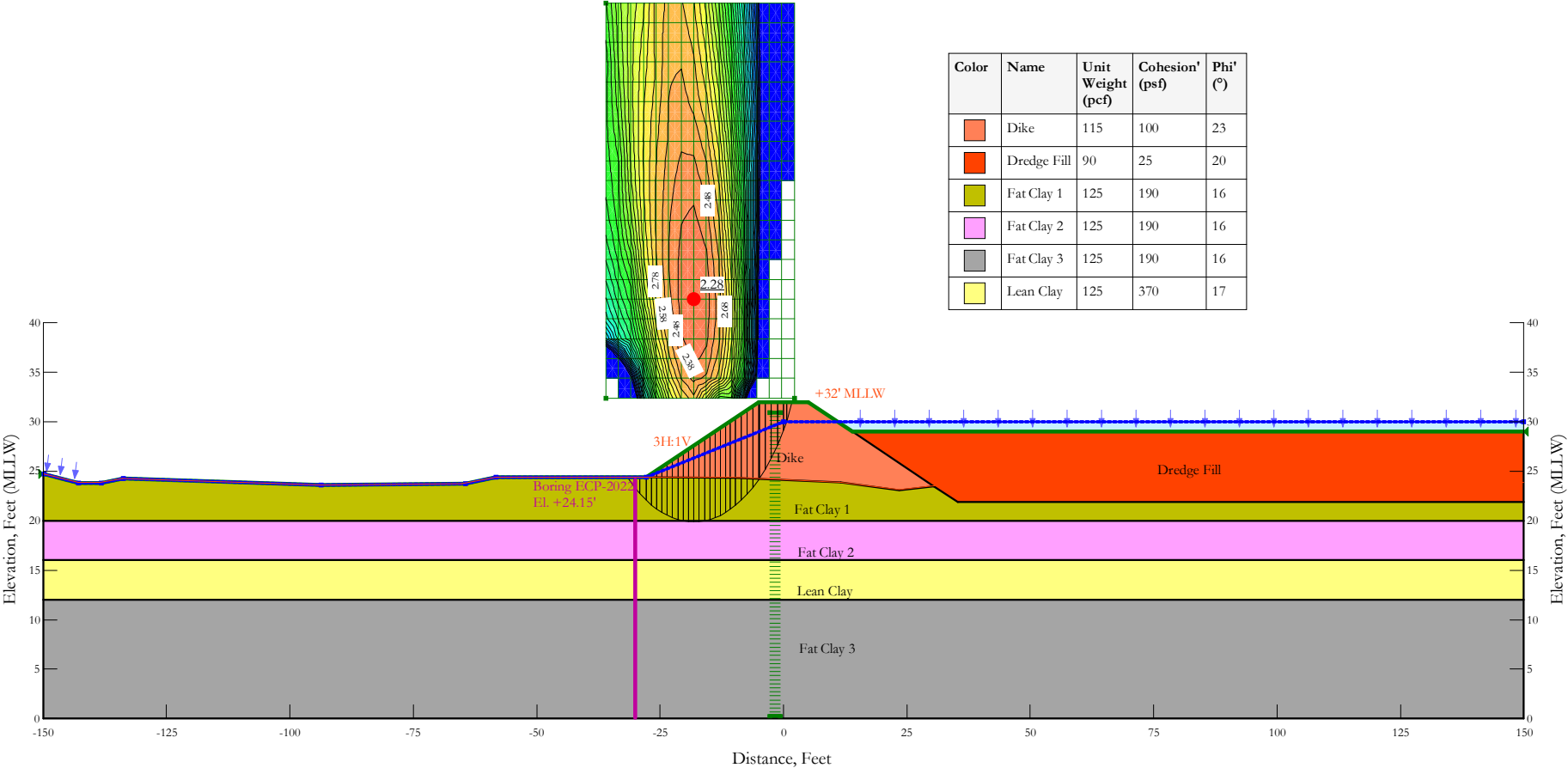


Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 155+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2022
Loading Condition: Short Term - Interior
Slip Surface: Block

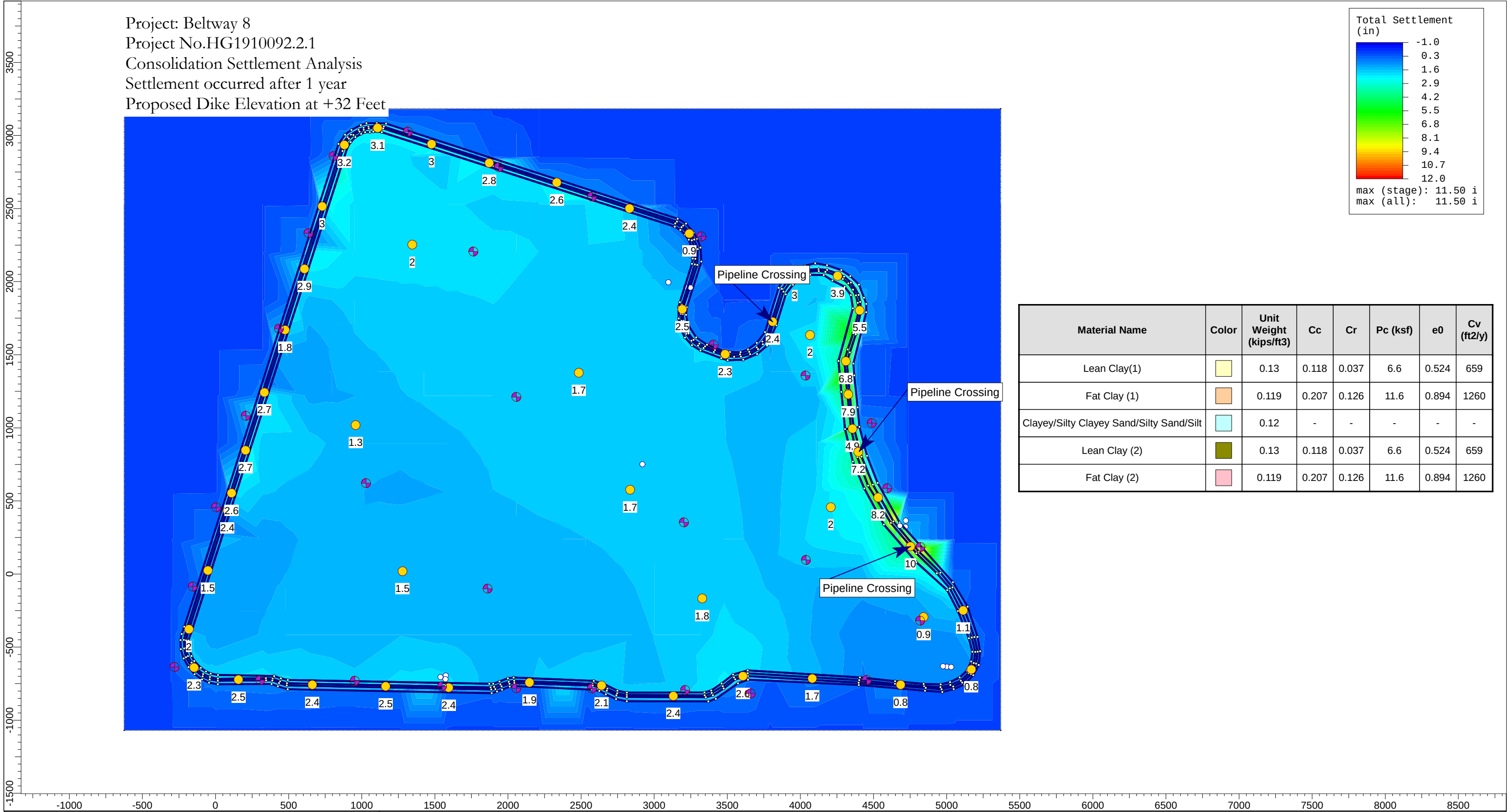
Color	Name	Unit Weight (pcf)	Cohesion (psf)
	Dike (U)	115	600
	Fat Clay 1 (U)	125	1,100
	Fat Clay 2 (U)	125	2,440
	Fat Clay 3 (U)	125	1,760
	Lean Clay (U)	125	1,400



Project Name: Houston Ship Channel Expansion Channel Improvement Project
Location: Beltway 8 Placement Area
Station: 155+00
HVJ Project Number: HG1910092.2.1
Boring ECP-2022
Loading Condition: Long Term - Exterior
Slip Surface: Circular

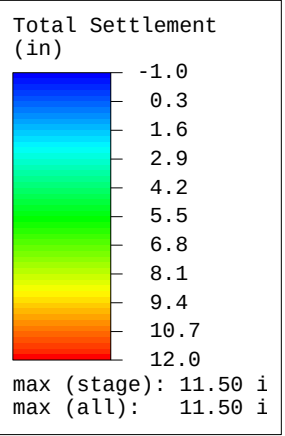
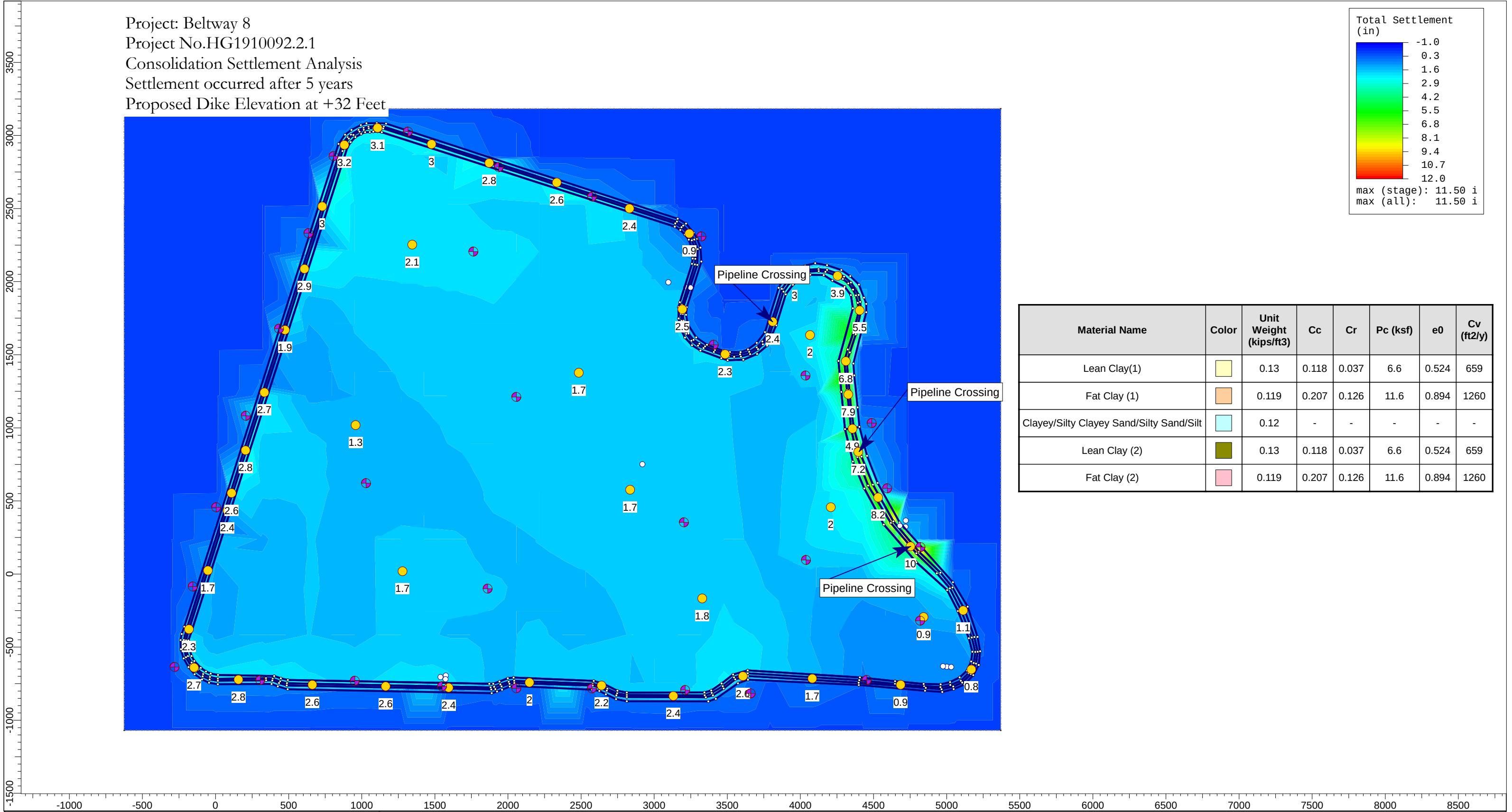


Project: Beltway 8
Project No.HG1910092.2.1
Consolidation Settlement Analysis
Settlement occurred after 1 year
Proposed Dike Elevation at +32 Feet



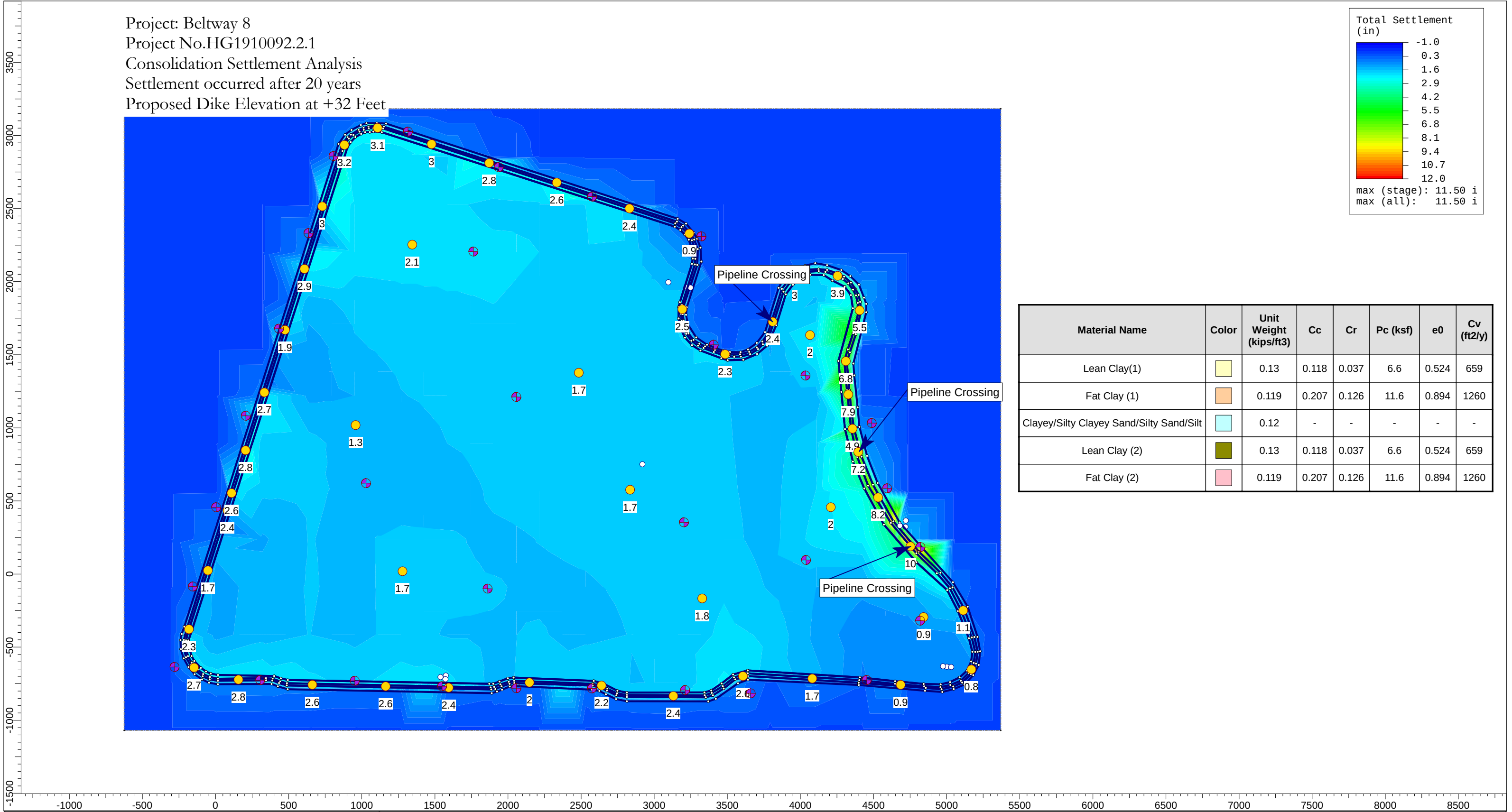
Material Name	Color	Unit Weight (kips/ft3)	Cc	Cr	Pc (ksf)	e0	Cv (ft2/y)
Lean Clay(1)		0.13	0.118	0.037	6.6	0.524	659
Fat Clay (1)		0.119	0.207	0.126	11.6	0.894	1260
Clayey/Silty Clayey Sand/Silty Sand/Silt		0.12	-	-	-	-	-
Lean Clay (2)		0.13	0.118	0.037	6.6	0.524	659
Fat Clay (2)		0.119	0.207	0.126	11.6	0.894	1260

Project: Beltway 8
Project No.HG1910092.2.1
Consolidation Settlement Analysis
Settlement occurred after 5 years
Proposed Dike Elevation at +32 Feet

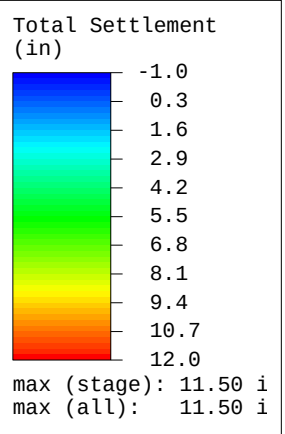
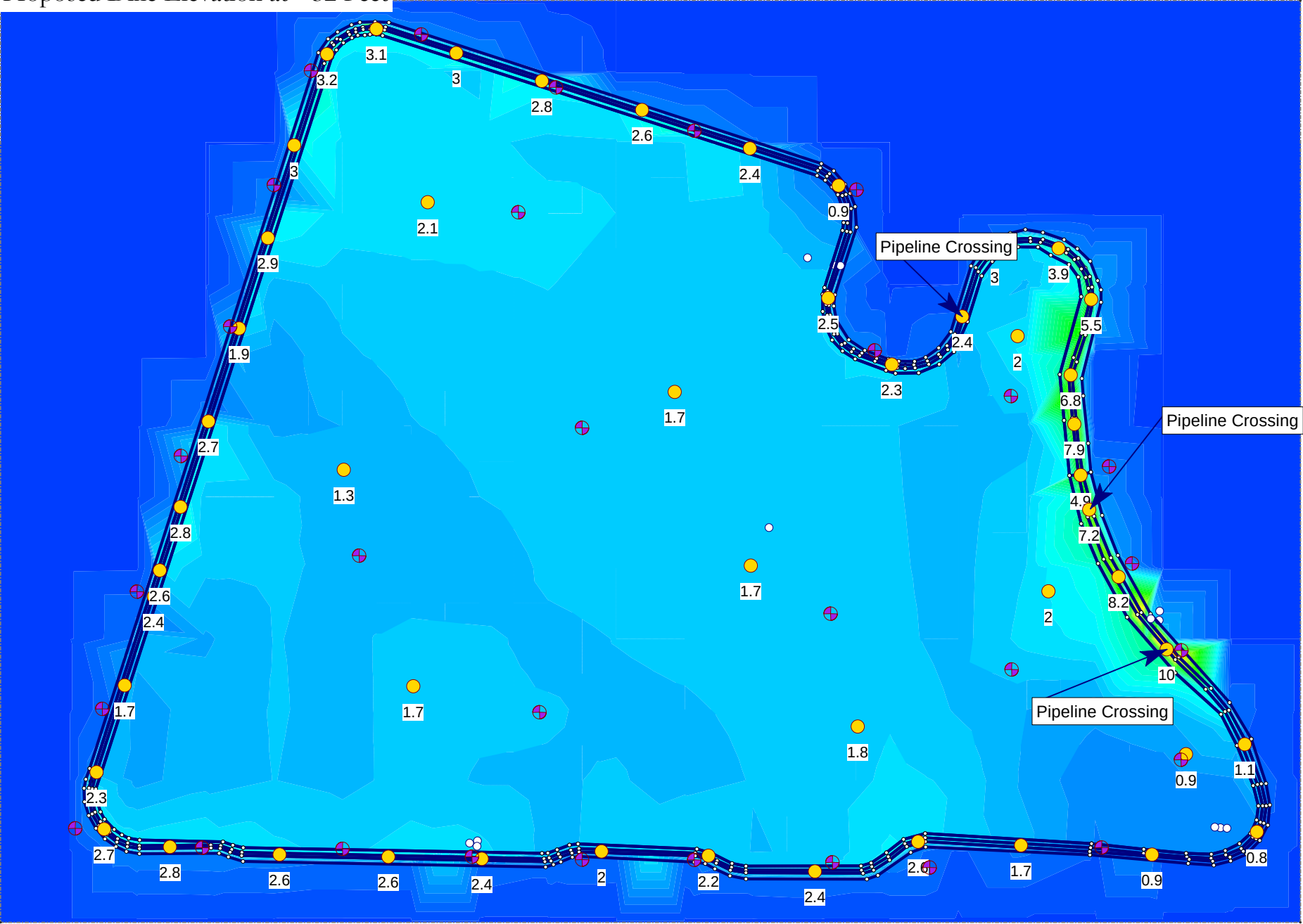


Material Name	Color	Unit Weight (kips/ft3)	Cc	Cr	Pc (ksf)	e0	Cv (ft2/y)
Lean Clay(1)		0.13	0.118	0.037	6.6	0.524	659
Fat Clay (1)		0.119	0.207	0.126	11.6	0.894	1260
Clayey/Silty Clayey Sand/Silty Sand/Silt		0.12	-	-	-	-	-
Lean Clay (2)		0.13	0.118	0.037	6.6	0.524	659
Fat Clay (2)		0.119	0.207	0.126	11.6	0.894	1260

Project: Beltway 8
Project No.HG1910092.2.1
Consolidation Settlement Analysis
Settlement occurred after 20 years
Proposed Dike Elevation at +32 Feet



Project: Beltway 8
Project No.HG1910092.2.1
Consolidation Settlement Analysis
Settlement occurred after 50 years
Proposed Dike Elevation at +32 Feet



Material Name	Color	Unit Weight (kips/ft3)	Cc	Cr	Pc (ksf)	e0	Cv (ft2/y)
Lean Clay(1)		0.13	0.118	0.037	6.6	0.524	659
Fat Clay (1)		0.119	0.207	0.126	11.6	0.894	1260
Clayey/Silty Clayey Sand/Silty Sand/Silt		0.12	-	-	-	-	-
Lean Clay (2)		0.13	0.118	0.037	6.6	0.524	659
Fat Clay (2)		0.119	0.207	0.126	11.6	0.894	1260



SETTLE3 5.006

Project	BW 8 Placement Area		
Analysis Description	Settlement		
Drawn By	NK	Company	HVJ Associates, Inc.
Date	1/31/2020, 4:34:32 PM	File Name	BW 8 - Rev. 1.s3z

Settle3 Analysis Information

BW 8 Placement Area

Project Settings

Document Name	BW 8 - Rev. 1
Project Title	BW 8 Placement Area
Analysis	Settlement
Author	NK
Company	HVJ Associates, Inc.
Date Created	1/31/2020, 4:34:32 PM
Stress Computation Method	Boussinesq
Time-dependent Consolidation Analysis	
Time Units	years
Permeability Units	feet/year
Minimum settlement ratio for subgrade modulus	0.9

Use average properties to calculate layered stresses

Improve consolidation accuracy

Ignore negative effective stresses in settlement calculations

Stage Settings

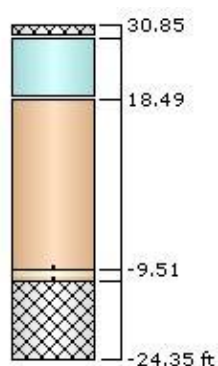
Stage #	Name	Time [years]
1	Stage 1	0
2	Stage 2	1
3	Stage 3	5
4	Stage 4	20
5	Stage 5	50

Soil Layers

Ground Surface Drained: Yes

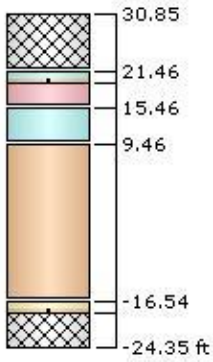
ECP-2014: (4453.98, -725.904)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	10	-28.49	No
2	Fat Clay (1)	28	-18.49	No
3	Fat Clay (2)	0	9.51	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	9.51	No
5	Fat Clay (1)	0	9.51	No
6	Lean Clay(1)	2	9.51	No
7	Lean Clay (2)	0	11.51	Yes
8	Fat Clay (1)	0	11.51	No
9	Fat Clay (2)	0	11.51	Yes
10	Lean Clay(1)	0	11.51	No
11	Lean Clay (2)	0	11.51	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	11.51	No
13	Lean Clay(1)	0	11.51	No
14	Fat Clay (1)	0	11.51	No



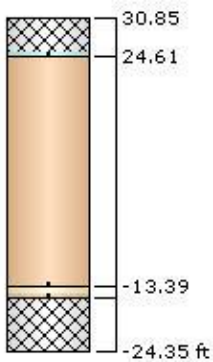
ECP-2015: (3661.12, -817.93)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	2	-21.46	No
2	Fat Clay (1)	0	-19.46	No
3	Fat Clay (2)	4	-19.46	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	6	-15.46	No
5	Fat Clay (1)	26	-9.46	No
6	Lean Clay(1)	2	16.54	No
7	Lean Clay (2)	0	18.54	Yes
8	Fat Clay (1)	0	18.54	No
9	Fat Clay (2)	0	18.54	Yes
10	Lean Clay(1)	0	18.54	No
11	Lean Clay (2)	0	18.54	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	18.54	No
13	Lean Clay(1)	0	18.54	No
14	Fat Clay (1)	0	18.54	No



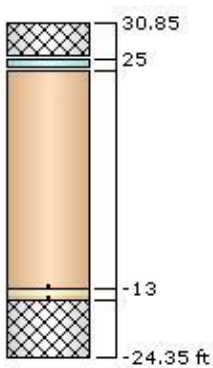
ECP-2016: (3204.69, 352.772)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-24.61	No
2	Fat Clay (1)	38	-24.61	No
3	Fat Clay (2)	0	13.39	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	13.39	No
5	Fat Clay (1)	0	13.39	No
6	Lean Clay(1)	2	13.39	No
7	Lean Clay (2)	0	15.39	Yes
8	Fat Clay (1)	0	15.39	No
9	Fat Clay (2)	0	15.39	Yes
10	Lean Clay(1)	0	15.39	No
11	Lean Clay (2)	0	15.39	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	15.39	No
13	Lean Clay(1)	0	15.39	No
14	Fat Clay (1)	0	15.39	No



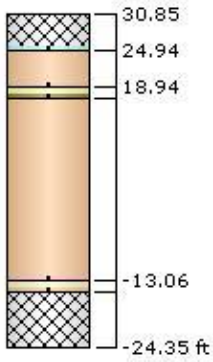
ECP-2017: (3212.06, -794.921)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	2	-25	No
2	Fat Clay (1)	36	-23	No
3	Fat Clay (2)	0	13	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	13	No
5	Fat Clay (1)	0	13	No
6	Lean Clay(1)	2	13	No
7	Lean Clay (2)	0	15	Yes
8	Fat Clay (1)	0	15	No
9	Fat Clay (2)	0	15	Yes
10	Lean Clay(1)	0	15	No
11	Lean Clay (2)	0	15	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	15	No
13	Lean Clay(1)	0	15	No
14	Fat Clay (1)	0	15	No



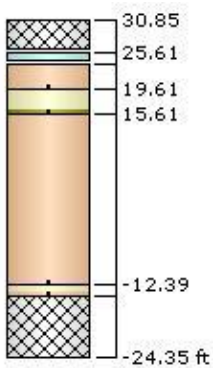
ECP-2018: (2574.54, -783.481)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-24.94	No
2	Fat Clay (1)	6	-24.94	No
3	Fat Clay (2)	0	-18.94	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-18.94	No
5	Fat Clay (1)	0	-18.94	No
6	Lean Clay(1)	2	-18.94	No
7	Lean Clay (2)	0	-16.94	Yes
8	Fat Clay (1)	30	-16.94	No
9	Fat Clay (2)	0	13.06	Yes
10	Lean Clay(1)	2	13.06	No
11	Lean Clay (2)	0	15.06	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	15.06	No
13	Lean Clay(1)	0	15.06	No
14	Fat Clay (1)	0	15.06	No



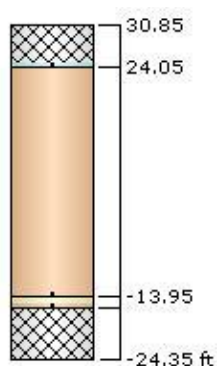
ECP-2019: (2058.05, -782.104)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	2	-25.61	No
2	Fat Clay (1)	4	-23.61	No
3	Fat Clay (2)	0	-19.61	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-19.61	No
5	Fat Clay (1)	0	-19.61	No
6	Lean Clay(1)	4	-19.61	No
7	Lean Clay (2)	0	-15.61	Yes
8	Fat Clay (1)	28	-15.61	No
9	Fat Clay (2)	0	12.39	Yes
10	Lean Clay(1)	2	12.39	No
11	Lean Clay (2)	0	14.39	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	14.39	No
13	Lean Clay(1)	0	14.39	No
14	Fat Clay (1)	0	14.39	No



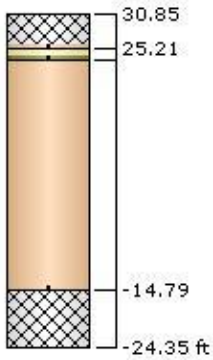
ECP-2020: (1550.17, -768.571)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-24.05	No
2	Fat Clay (1)	38	-24.05	No
3	Fat Clay (2)	0	13.95	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	13.95	No
5	Fat Clay (1)	0	13.95	No
6	Lean Clay(1)	2	13.95	No
7	Lean Clay (2)	0	15.95	Yes
8	Fat Clay (1)	0	15.95	No
9	Fat Clay (2)	0	15.95	Yes
10	Lean Clay(1)	0	15.95	No
11	Lean Clay (2)	0	15.95	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	15.95	No
13	Lean Clay(1)	0	15.95	No
14	Fat Clay (1)	0	15.95	No



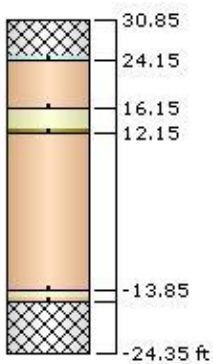
ECP-2021: (1861.27, -101.437)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-25.21	No
2	Fat Clay (1)	0	-25.21	No
3	Fat Clay (2)	0	-25.21	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-25.21	No
5	Fat Clay (1)	0	-25.21	No
6	Lean Clay(1)	2	-25.21	No
7	Lean Clay (2)	0	-23.21	Yes
8	Fat Clay (1)	38	-23.21	No
9	Fat Clay (2)	0	14.79	Yes
10	Lean Clay(1)	0	14.79	No
11	Lean Clay (2)	0	14.79	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	14.79	No
13	Lean Clay(1)	0	14.79	No
14	Fat Clay (1)	0	14.79	No



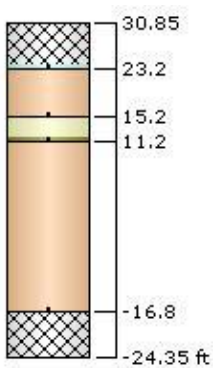
ECP-2022: (953.241, -731.652)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-24.15	No
2	Fat Clay (1)	8	-24.15	No
3	Fat Clay (2)	0	-16.15	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-16.15	No
5	Fat Clay (1)	0	-16.15	No
6	Lean Clay(1)	4	-16.15	No
7	Lean Clay (2)	0	-12.15	Yes
8	Fat Clay (1)	26	-12.15	No
9	Fat Clay (2)	0	13.85	Yes
10	Lean Clay(1)	2	13.85	No
11	Lean Clay (2)	0	15.85	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	15.85	No
13	Lean Clay(1)	0	15.85	No
14	Fat Clay (1)	0	15.85	No



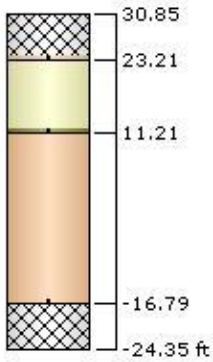
ECP-2023: (305.792, -727.43)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-23.2	No
2	Fat Clay (1)	8	-23.2	No
3	Fat Clay (2)	0	-15.2	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-15.2	No
5	Fat Clay (1)	0	-15.2	No
6	Lean Clay(1)	4	-15.2	No
7	Lean Clay (2)	0	-11.2	Yes
8	Fat Clay (1)	28	-11.2	No
9	Fat Clay (2)	0	16.8	Yes
10	Lean Clay(1)	0	16.8	No
11	Lean Clay (2)	0	16.8	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	16.8	No
13	Lean Clay(1)	0	16.8	No
14	Fat Clay (1)	0	16.8	No



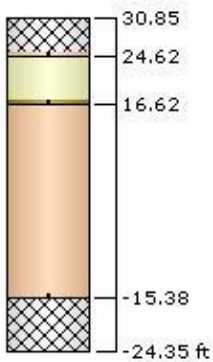
ECP-2024: (-279.144, -637.332)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-23.21	No
2	Fat Clay (1)	0	-23.21	No
3	Fat Clay (2)	0	-23.21	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-23.21	No
5	Fat Clay (1)	0	-23.21	No
6	Lean Clay(1)	12	-23.21	No
7	Lean Clay (2)	0	-11.21	Yes
8	Fat Clay (1)	28	-11.21	No
9	Fat Clay (2)	0	16.79	Yes
10	Lean Clay(1)	0	16.79	No
11	Lean Clay (2)	0	16.79	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	16.79	No
13	Lean Clay(1)	0	16.79	No
14	Fat Clay (1)	0	16.79	No



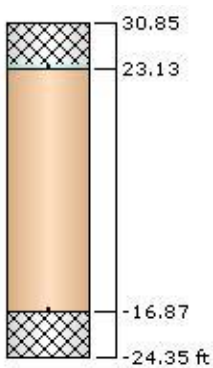
ECP-2025: (-155.239, -86.317)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-24.62	No
2	Fat Clay (1)	0	-24.62	No
3	Fat Clay (2)	0	-24.62	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-24.62	No
5	Fat Clay (1)	0	-24.62	No
6	Lean Clay(1)	8	-24.62	No
7	Lean Clay (2)	0	-16.62	Yes
8	Fat Clay (1)	32	-16.62	No
9	Fat Clay (2)	0	15.38	Yes
10	Lean Clay(1)	0	15.38	No
11	Lean Clay (2)	0	15.38	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	15.38	No
13	Lean Clay(1)	0	15.38	No
14	Fat Clay (1)	0	15.38	No



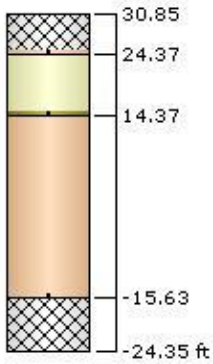
ECP-2026: (4.99, 455.09)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-23.13	No
2	Fat Clay (1)	40	-23.13	No
3	Fat Clay (2)	0	16.87	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	16.87	No
5	Fat Clay (1)	0	16.87	No
6	Lean Clay(1)	0	16.87	No
7	Lean Clay (2)	0	16.87	Yes
8	Fat Clay (1)	0	16.87	No
9	Fat Clay (2)	0	16.87	Yes
10	Lean Clay(1)	0	16.87	No
11	Lean Clay (2)	0	16.87	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	16.87	No
13	Lean Clay(1)	0	16.87	No
14	Fat Clay (1)	0	16.87	No



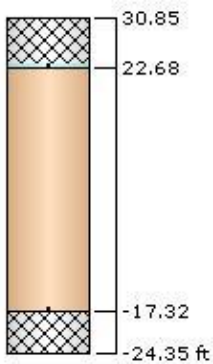
ECP-2027: (1030.08, 621.032)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-24.37	No
2	Fat Clay (1)	0	-24.37	No
3	Fat Clay (2)	0	-24.37	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-24.37	No
5	Fat Clay (1)	0	-24.37	No
6	Lean Clay(1)	10	-24.37	No
7	Lean Clay (2)	0	-14.37	Yes
8	Fat Clay (1)	30	-14.37	No
9	Fat Clay (2)	0	15.63	Yes
10	Lean Clay(1)	0	15.63	No
11	Lean Clay (2)	0	15.63	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	15.63	No
13	Lean Clay(1)	0	15.63	No
14	Fat Clay (1)	0	15.63	No



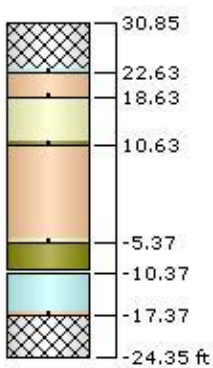
ECP-2028: (208.075, 1081.2)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-22.68	No
2	Fat Clay (1)	40	-22.68	No
3	Fat Clay (2)	0	17.32	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	17.32	No
5	Fat Clay (1)	0	17.32	No
6	Lean Clay(1)	0	17.32	No
7	Lean Clay (2)	0	17.32	Yes
8	Fat Clay (1)	0	17.32	No
9	Fat Clay (2)	0	17.32	Yes
10	Lean Clay(1)	0	17.32	No
11	Lean Clay (2)	0	17.32	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	17.32	No
13	Lean Clay(1)	0	17.32	No
14	Fat Clay (1)	0	17.32	No



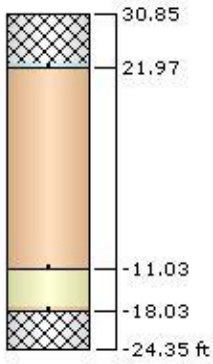
ECP-2029: (434.827, 1677.33)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-22.63	No
2	Fat Clay (1)	4	-22.63	No
3	Fat Clay (2)	0	-18.63	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-18.63	No
5	Fat Clay (1)	0	-18.63	No
6	Lean Clay(1)	8	-18.63	No
7	Lean Clay (2)	0	-10.63	Yes
8	Fat Clay (1)	16	-10.63	No
9	Fat Clay (2)	0	5.37	Yes
10	Lean Clay(1)	0	5.37	No
11	Lean Clay (2)	5	5.37	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	7	10.37	No
13	Lean Clay(1)	0	17.37	No
14	Fat Clay (1)	0	17.37	No



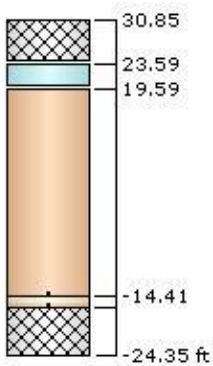
ECP-2030: (636.344, 2330.7)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-21.97	No
2	Fat Clay (1)	33	-21.97	No
3	Fat Clay (2)	0	11.03	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	11.03	No
5	Fat Clay (1)	0	11.03	No
6	Lean Clay(1)	7	11.03	No
7	Lean Clay (2)	0	18.03	Yes
8	Fat Clay (1)	0	18.03	No
9	Fat Clay (2)	0	18.03	Yes
10	Lean Clay(1)	0	18.03	No
11	Lean Clay (2)	0	18.03	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	18.03	No
13	Lean Clay(1)	0	18.03	No
14	Fat Clay (1)	0	18.03	No



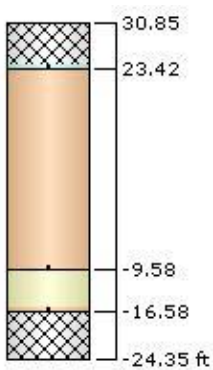
ECP-2031: (807.776, 2858.44)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	4	-23.59	No
2	Fat Clay (1)	34	-19.59	No
3	Fat Clay (2)	0	14.41	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	14.41	No
5	Fat Clay (1)	0	14.41	No
6	Lean Clay(1)	2	14.41	No
7	Lean Clay (2)	0	16.41	Yes
8	Fat Clay (1)	0	16.41	No
9	Fat Clay (2)	0	16.41	Yes
10	Lean Clay(1)	0	16.41	No
11	Lean Clay (2)	0	16.41	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	16.41	No
13	Lean Clay(1)	0	16.41	No
14	Fat Clay (1)	0	16.41	No



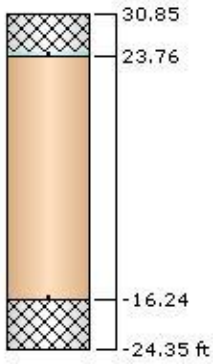
ECP-2032: (1316.23, 3025.15)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-23.42	No
2	Fat Clay (1)	33	-23.42	No
3	Fat Clay (2)	0	9.58	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	9.58	No
5	Fat Clay (1)	0	9.58	No
6	Lean Clay(1)	7	9.58	No
7	Lean Clay (2)	0	16.58	Yes
8	Fat Clay (1)	0	16.58	No
9	Fat Clay (2)	0	16.58	Yes
10	Lean Clay(1)	0	16.58	No
11	Lean Clay (2)	0	16.58	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	16.58	No
13	Lean Clay(1)	0	16.58	No
14	Fat Clay (1)	0	16.58	No



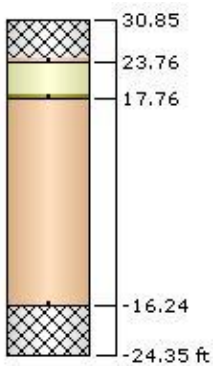
ECP-2033: (1764.01, 2205.09)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-23.76	No
2	Fat Clay (1)	40	-23.76	No
3	Fat Clay (2)	0	16.24	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	16.24	No
5	Fat Clay (1)	0	16.24	No
6	Lean Clay(1)	0	16.24	No
7	Lean Clay (2)	0	16.24	Yes
8	Fat Clay (1)	0	16.24	No
9	Fat Clay (2)	0	16.24	Yes
10	Lean Clay(1)	0	16.24	No
11	Lean Clay (2)	0	16.24	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	16.24	No
13	Lean Clay(1)	0	16.24	No
14	Fat Clay (1)	0	16.24	No



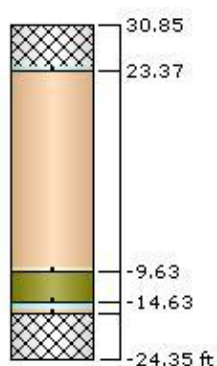
ECP-2034: (1937.49, 2782.03)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-23.76	No
2	Fat Clay (1)	0	-23.76	No
3	Fat Clay (2)	0	-23.76	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-23.76	No
5	Fat Clay (1)	0	-23.76	No
6	Lean Clay(1)	6	-23.76	No
7	Lean Clay (2)	0	-17.76	Yes
8	Fat Clay (1)	34	-17.76	No
9	Fat Clay (2)	0	16.24	Yes
10	Lean Clay(1)	0	16.24	No
11	Lean Clay (2)	0	16.24	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	16.24	No
13	Lean Clay(1)	0	16.24	No
14	Fat Clay (1)	0	16.24	No



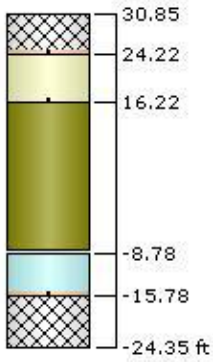
ECP-2035: (2576.14, 2581.07)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-23.37	No
2	Fat Clay (1)	33	-23.37	No
3	Fat Clay (2)	0	9.63	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	9.63	No
5	Fat Clay (1)	0	9.63	No
6	Lean Clay(1)	0	9.63	No
7	Lean Clay (2)	5	9.63	Yes
8	Fat Clay (1)	0	14.63	No
9	Fat Clay (2)	0	14.63	Yes
10	Lean Clay(1)	0	14.63	No
11	Lean Clay (2)	0	14.63	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	2	14.63	No
13	Lean Clay(1)	0	16.63	No
14	Fat Clay (1)	0	16.63	No



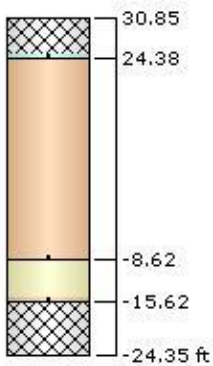
ECP-2036: (3323.6, 2309.1)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-24.22	No
2	Fat Clay (1)	0	-24.22	No
3	Fat Clay (2)	0	-24.22	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-24.22	No
5	Fat Clay (1)	0	-24.22	No
6	Lean Clay(1)	8	-24.22	No
7	Lean Clay (2)	0	-16.22	Yes
8	Fat Clay (1)	0	-16.22	No
9	Fat Clay (2)	0	-16.22	Yes
10	Lean Clay(1)	0	-16.22	No
11	Lean Clay (2)	25	-16.22	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	7	8.78	No
13	Lean Clay(1)	0	15.78	No
14	Fat Clay (1)	0	15.78	No



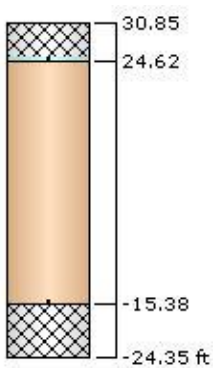
ECP-2037: (3408.03, 1567.98)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-24.38	No
2	Fat Clay (1)	33	-24.38	No
3	Fat Clay (2)	0	8.62	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	8.62	No
5	Fat Clay (1)	0	8.62	No
6	Lean Clay(1)	7	8.62	No
7	Lean Clay (2)	0	15.62	Yes
8	Fat Clay (1)	0	15.62	No
9	Fat Clay (2)	0	15.62	Yes
10	Lean Clay(1)	0	15.62	No
11	Lean Clay (2)	0	15.62	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	15.62	No
13	Lean Clay(1)	0	15.62	No
14	Fat Clay (1)	0	15.62	No



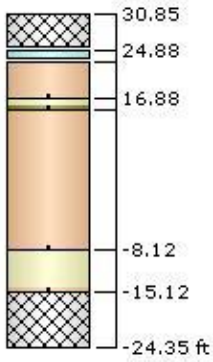
ECP-2038: (2058.41, 1210.46)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-24.62	No
2	Fat Clay (1)	40	-24.62	No
3	Fat Clay (2)	0	15.38	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	15.38	No
5	Fat Clay (1)	0	15.38	No
6	Lean Clay(1)	0	15.38	No
7	Lean Clay (2)	0	15.38	Yes
8	Fat Clay (1)	0	15.38	No
9	Fat Clay (2)	0	15.38	Yes
10	Lean Clay(1)	0	15.38	No
11	Lean Clay (2)	0	15.38	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	15.38	No
13	Lean Clay(1)	0	15.38	No
14	Fat Clay (1)	0	15.38	No



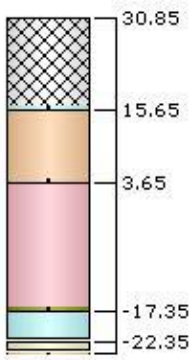
ECP-2039: (4035.96, 1356.5)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	2	-24.88	No
2	Fat Clay (1)	6	-22.88	No
3	Fat Clay (2)	0	-16.88	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-16.88	No
5	Fat Clay (1)	0	-16.88	No
6	Lean Clay(1)	2	-16.88	No
7	Lean Clay (2)	0	-14.88	Yes
8	Fat Clay (1)	23	-14.88	No
9	Fat Clay (2)	0	8.12	Yes
10	Lean Clay(1)	7	8.12	No
11	Lean Clay (2)	0	15.12	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	15.12	No
13	Lean Clay(1)	0	15.12	No
14	Fat Clay (1)	0	15.12	No



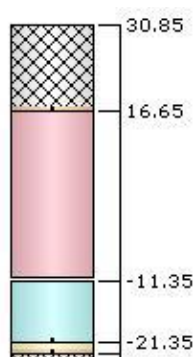
ECP-2040: (4488.44, 1031.76)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-15.65	No
2	Fat Clay (1)	12	-15.65	No
3	Fat Clay (2)	0	-3.65	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-3.65	No
5	Fat Clay (1)	0	-3.65	No
6	Lean Clay(1)	0	-3.65	No
7	Lean Clay (2)	0	-3.65	Yes
8	Fat Clay (1)	0	-3.65	No
9	Fat Clay (2)	21	-3.65	Yes
10	Lean Clay(1)	0	17.35	No
11	Lean Clay (2)	0	17.35	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	5	17.35	No
13	Lean Clay(1)	2	22.35	No
14	Fat Clay (1)	0	24.35	No



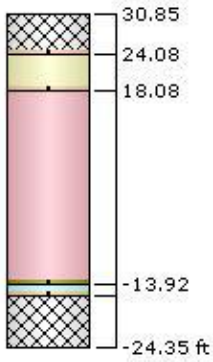
ECP-2041: (4595.01, 584.895)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-16.65	No
2	Fat Clay (1)	0	-16.65	No
3	Fat Clay (2)	28	-16.65	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	10	11.35	No
5	Fat Clay (1)	0	21.35	No
6	Lean Clay(1)	0	21.35	No
7	Lean Clay (2)	0	21.35	Yes
8	Fat Clay (1)	0	21.35	No
9	Fat Clay (2)	0	21.35	Yes
10	Lean Clay(1)	0	21.35	No
11	Lean Clay (2)	0	21.35	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	21.35	No
13	Lean Clay(1)	2	21.35	No
14	Fat Clay (1)	0	23.35	No



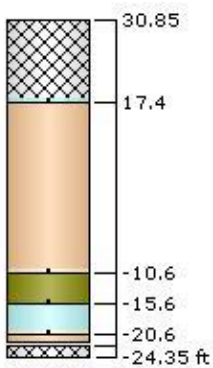
ECP-2042: (4039.33, 95.205)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-24.08	No
2	Fat Clay (1)	0	-24.08	No
3	Fat Clay (2)	0	-24.08	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-24.08	No
5	Fat Clay (1)	0	-24.08	No
6	Lean Clay(1)	6	-24.08	No
7	Lean Clay (2)	0	-18.08	Yes
8	Fat Clay (1)	0	-18.08	No
9	Fat Clay (2)	32	-18.08	Yes
10	Lean Clay(1)	0	13.92	No
11	Lean Clay (2)	0	13.92	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	2	13.92	No
13	Lean Clay(1)	0	15.92	No
14	Fat Clay (1)	0	15.92	No



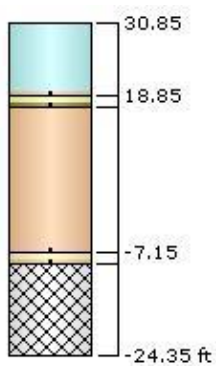
ECP-2043: (4822.14, 183.76)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-17.4	No
2	Fat Clay (1)	28	-17.4	No
3	Fat Clay (2)	0	10.6	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	10.6	No
5	Fat Clay (1)	0	10.6	No
6	Lean Clay(1)	0	10.6	No
7	Lean Clay (2)	5	10.6	Yes
8	Fat Clay (1)	0	15.6	No
9	Fat Clay (2)	0	15.6	Yes
10	Lean Clay(1)	0	15.6	No
11	Lean Clay (2)	0	15.6	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	5	15.6	No
13	Lean Clay(1)	0	20.6	No
14	Fat Clay (1)	2	20.6	No



ECP-2044: (4819.38, -320.617)

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Clayey/Silty Clayey Sand/Silty Sand/Silt	12	-30.85	No
2	Fat Clay (1)	0	-18.85	No
3	Fat Clay (2)	0	-18.85	Yes
4	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	-18.85	No
5	Fat Clay (1)	0	-18.85	No
6	Lean Clay(1)	2	-18.85	No
7	Lean Clay (2)	0	-16.85	Yes
8	Fat Clay (1)	24	-16.85	No
9	Fat Clay (2)	0	7.15	Yes
10	Lean Clay(1)	2	7.15	No
11	Lean Clay (2)	0	9.15	Yes
12	Clayey/Silty Clayey Sand/Silty Sand/Silt	0	9.15	No
13	Lean Clay(1)	0	9.15	No
14	Fat Clay (1)	0	9.15	No



Soil Properties

Property	Lean Clay(1)	Fat Clay (1)	Clayey/Silty Clayey Sand/Silty Sand/Silt	Lean Clay (2)
Color				
Unit Weight [kips/ft ³]	0.13	0.119	0.12	0.13
Saturated Unit Weight [kips/ft ³]	0.13	0.119	0.12	0.13
K0	1	1	1	1
Primary Consolidation	Enabled	Enabled	Disabled	Enabled
Material Type	Non-Linear	Non-Linear		Non-Linear
Cc	0.118	0.207	-	0.118
Cr	0.037	0.126	-	0.037
e0	0.524	0.894	-	0.524
Pc [ksf]	6.6	11.6	-	6.6
Cv [ft ² /y]	659	1260	-	659
Cvr [ft ² /y]	659	1260	-	659
B-bar	1	1	-	1
Undrained Su A [kips/ft ²]	0	0	0	0
Undrained Su S	0.2	0.2	0.2	0.2
Undrained Su m	0.8	0.8	0.8	0.8
Piezo Line ID	1	1	1	1

Property	Fat Clay (2)
Color	
Unit Weight [kips/ft ³]	0.119
Saturated Unit Weight [kips/ft ³]	0.119
K0	1
Primary Consolidation	Enabled
Material Type	Non-Linear
Cc	0.207
Cr	0.126
e0	0.894
Pc [ksf]	11.6
Cv [ft ² /y]	1260
Cvr [ft ² /y]	1260
B-bar	1
Undrained Su A [kips/ft ²]	0
Undrained Su S	0.2
Undrained Su m	0.8
Piezo Line ID	1

Groundwater

Groundwater method	Piezometric Lines
Water Unit Weight	0.0624 kips/ft ³
Generating excess pore pressure above water table	

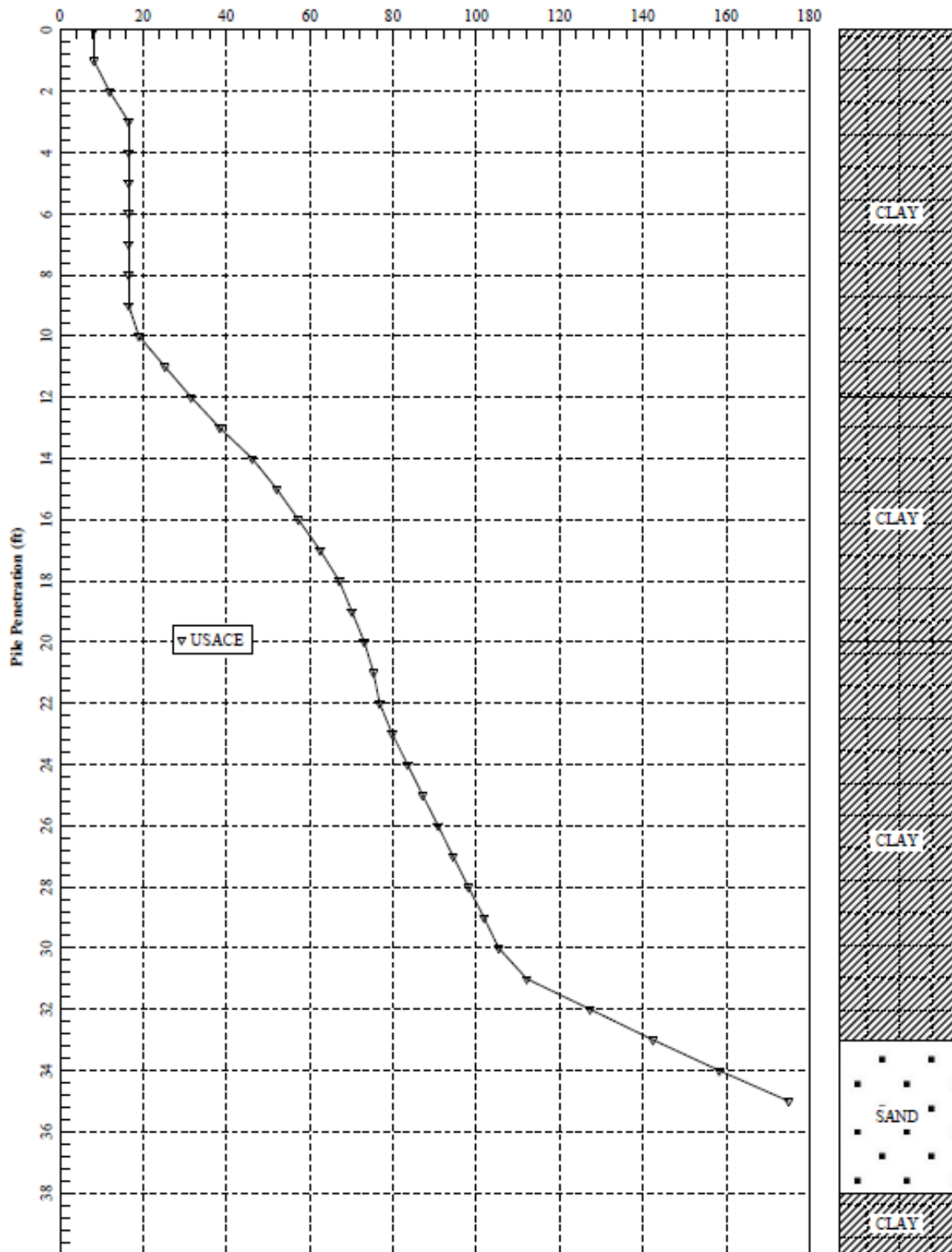
Piezometric Line Entities

ID	Depth (ft)
1	-22.9 ft

APPENDIX J

DRIVEN PILE AXIAL CAPACITY CURVES:
BELTWAY 8 PLACEMENT AREA

Ultimate Compressive Capacity for HP14X89 Steel H-Pile near Boring ECP-2040
Total Capacity (kips)



Notes:

* Allowable axial compressive capacity can be calculated by applying a factor of safety to the total ultimate capacity. Factors of safety should be determined based on USACE EM1110-2-2906 Design of Pile Foundations.



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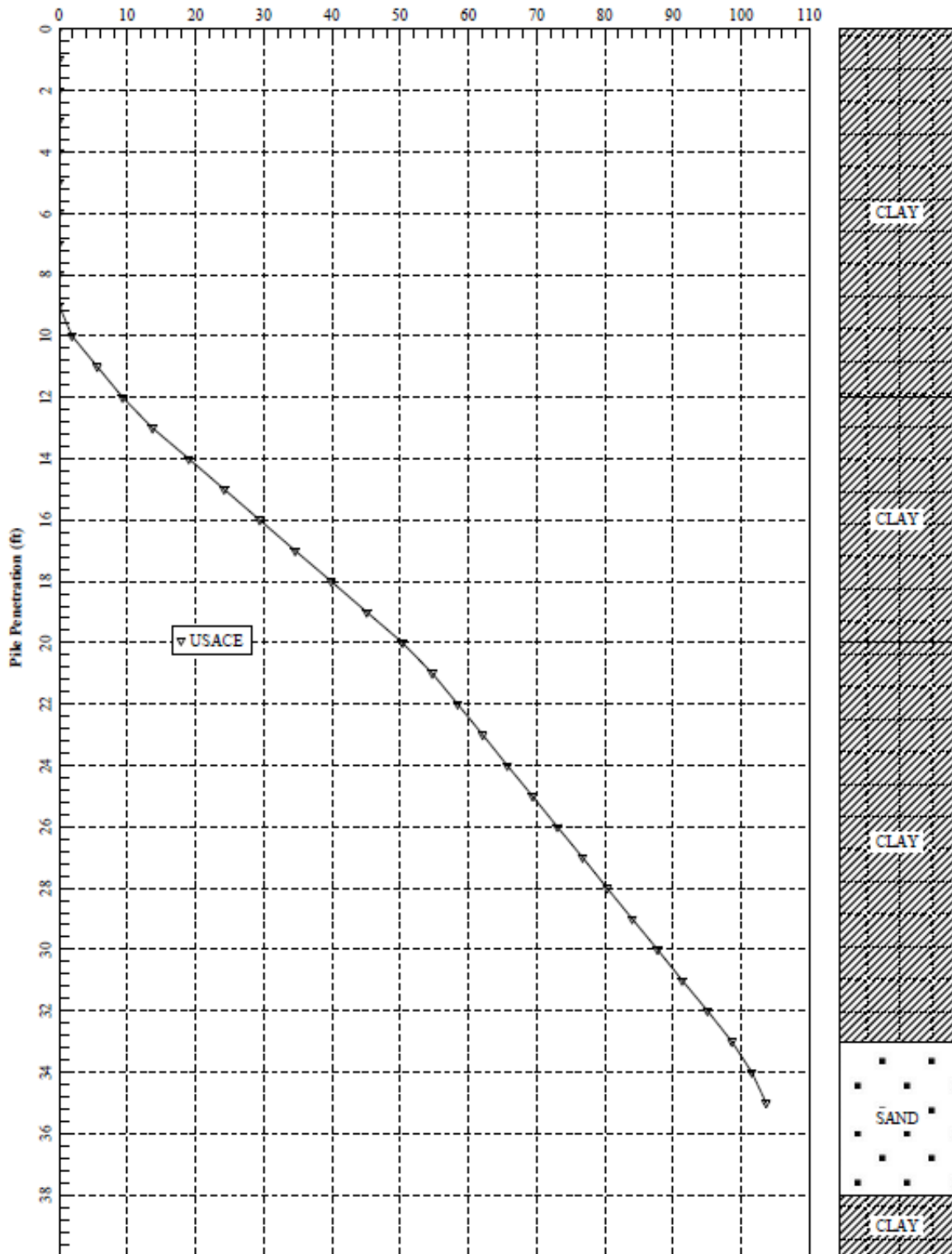
PREPARED BY:
AR

ULTIMATE COMPRESSIVE CAPACITY
OF HP14X89 STEEL H-PILE NEAR
BORING ECP-2040, BELTWAY 8 PLACEMENT AREA

PROJECT NO.:
HG1910092.2.1

DRAWING NO.:
PLATE J-1

Ultimate Tensile Capacity for HP14X89 Steel H-Pile near Boring ECP-2040
Accumulated Skin Friction (kips)



Notes:

* Allowable axial tension capacity can be calculated by applying a factor of safety to the ultimate skin friction capacity. Factors of safety should be determined based on USACE EM1110-2-2906 Design of Pile Foundations.



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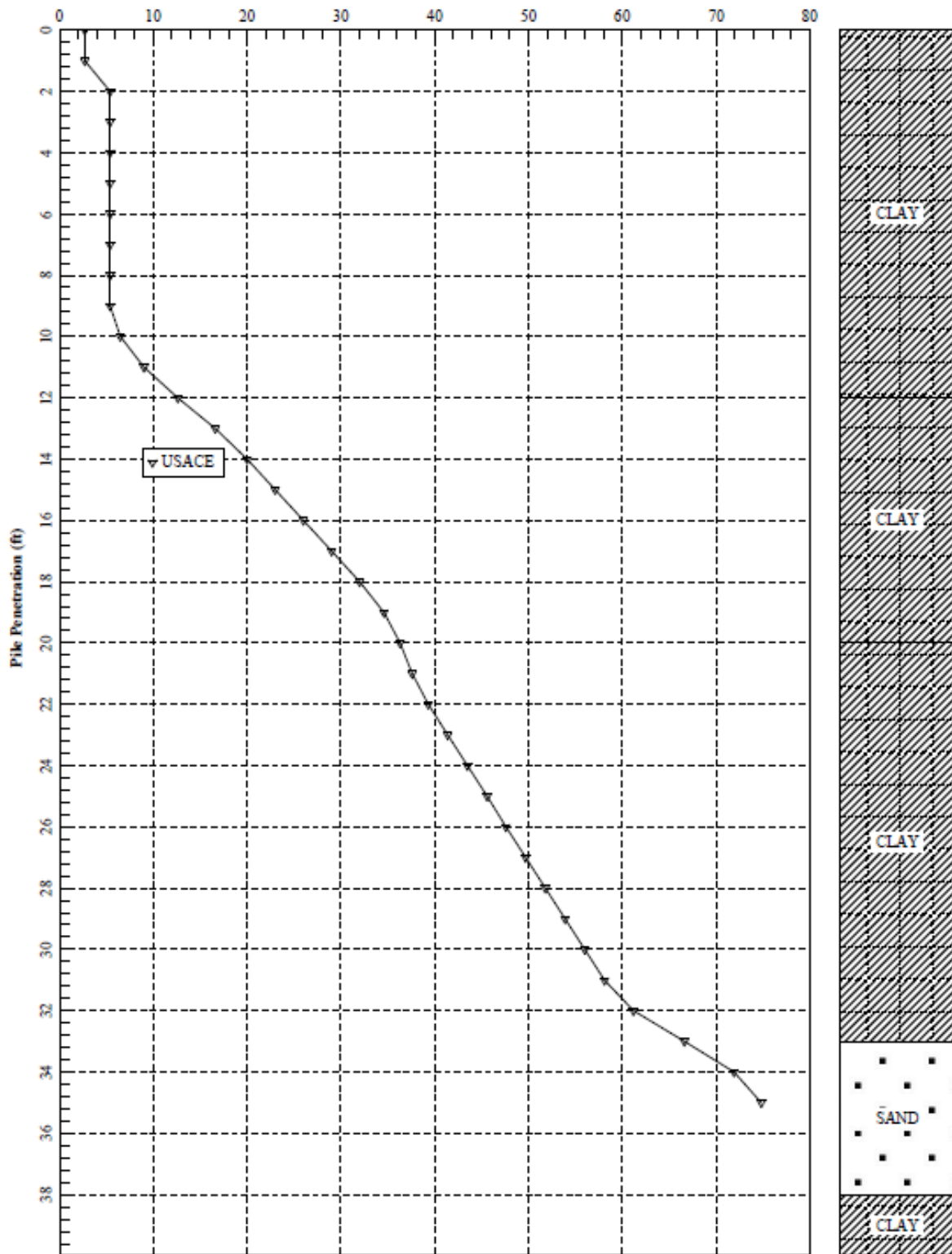
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ULTIMATE AXIAL TENSION CAPACITY
 OF HP14X89 STEEL H-PILE NEAR
 BORING ECP-2040, BELTWAY 8 PLACEMENT AREA

PROJECT NO.:
 HG1910092.2.1

DRAWING NO.:
 PLATE J-2

Ultimate Compressive Capacity for W8X40 Steel H-Pile near Boring ECP-2040
Total Capacity (kips)



Notes:

* Allowable axial compressive capacity can be calculated by applying a factor of safety to the total ultimate capacity. Factors of safety should be determined based on USACE EM1110-2-2906 Design of Pile Foundations.



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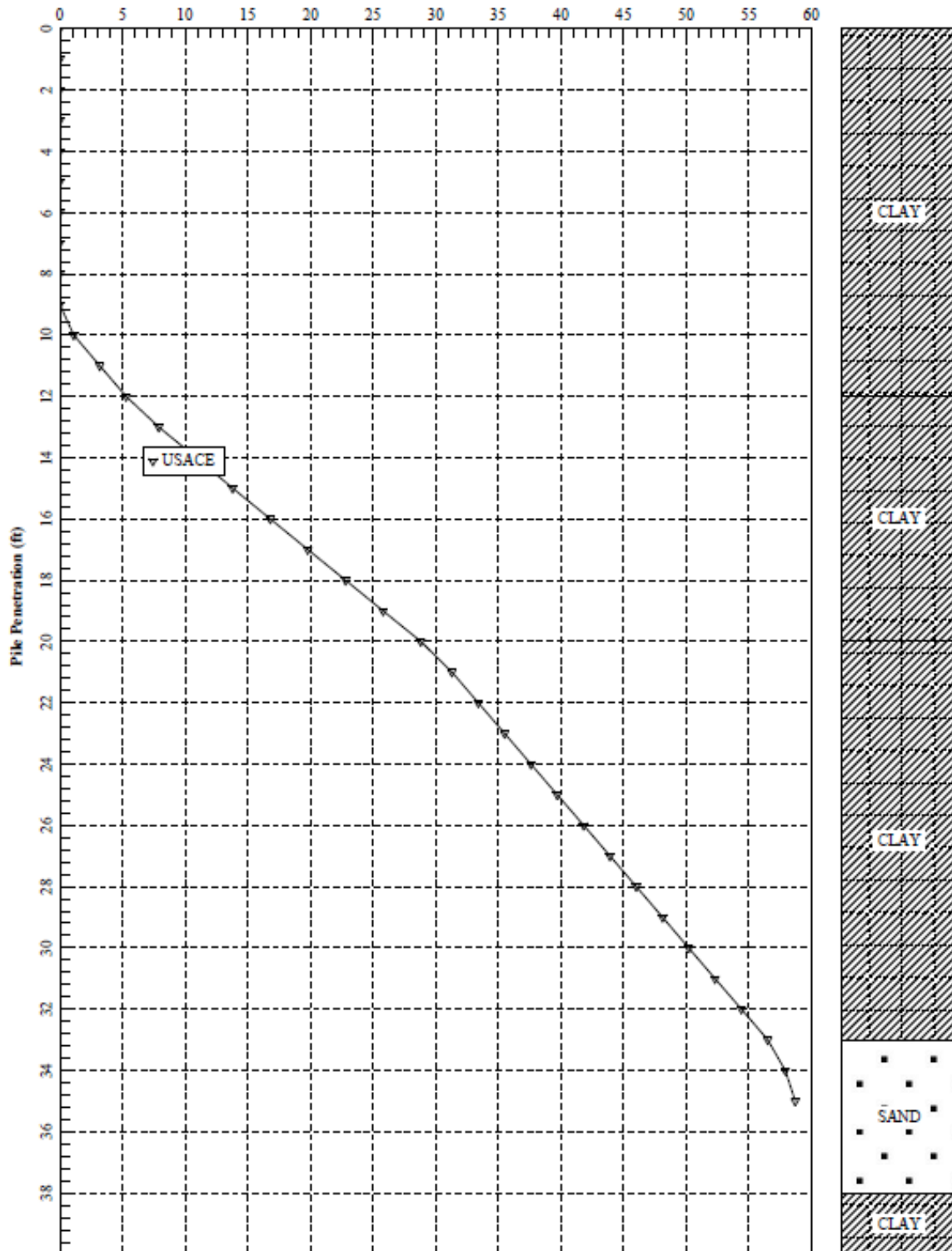
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ULTIMATE COMPRESSIVE CAPACITY
OF W8X40 STEEL H-PILE NEAR
BORING ECP-2040, BELTWAY 8 PLACEMENT AREA

PROJECT NO.:
HG1910092.2.1

DRAWING NO.:
PLATE J-3

**Ultimate Tensile Capacity for W8X40 Steel H-Pile near Boring ECP-2040
Accumulated Skin Friction (kips)**



Notes:

* Allowable axial tension capacity can be calculated by applying a factor of safety to the ultimate skin friction capacity. Factors of safety should be determined based on USACE EM1110-2-2906 Design of Pile Foundations.



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ULTIMATE AXIAL TENSION CAPACITY
OF W8X40 STEEL H-PILE NEAR
BORING ECP-2040, BELTWAY 8 PLACEMENT AREA

PROJECT NO.:
HG1910092.2.1

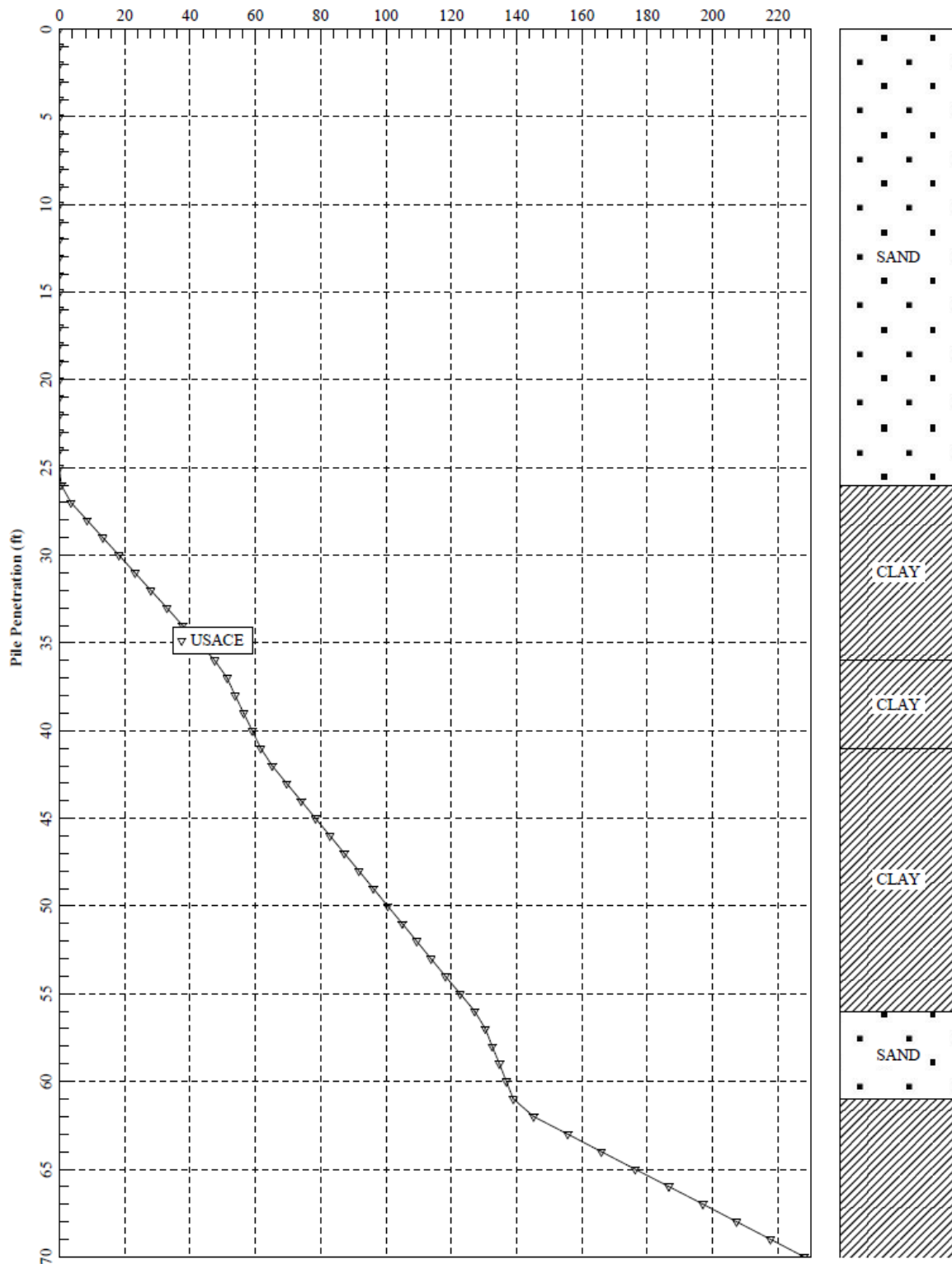
DRAWING NO.:
PLATE J-4

APPENDIX K

DRIVEN PILE AXIAL CAPACITY CURVES: MORGANS POINT

Pile Top
El. +3.0' MLLW

Morgans Point - NZ 38
Accumulated Skin Friction (kips)



Notes:

* * Allowable axial tension capacity can be calculated by applying a factor of safety to the ultimate skin friction capacity. Factors of safety should be determined based on USACE EM1110-2-2906 Design of Pile Foundations.



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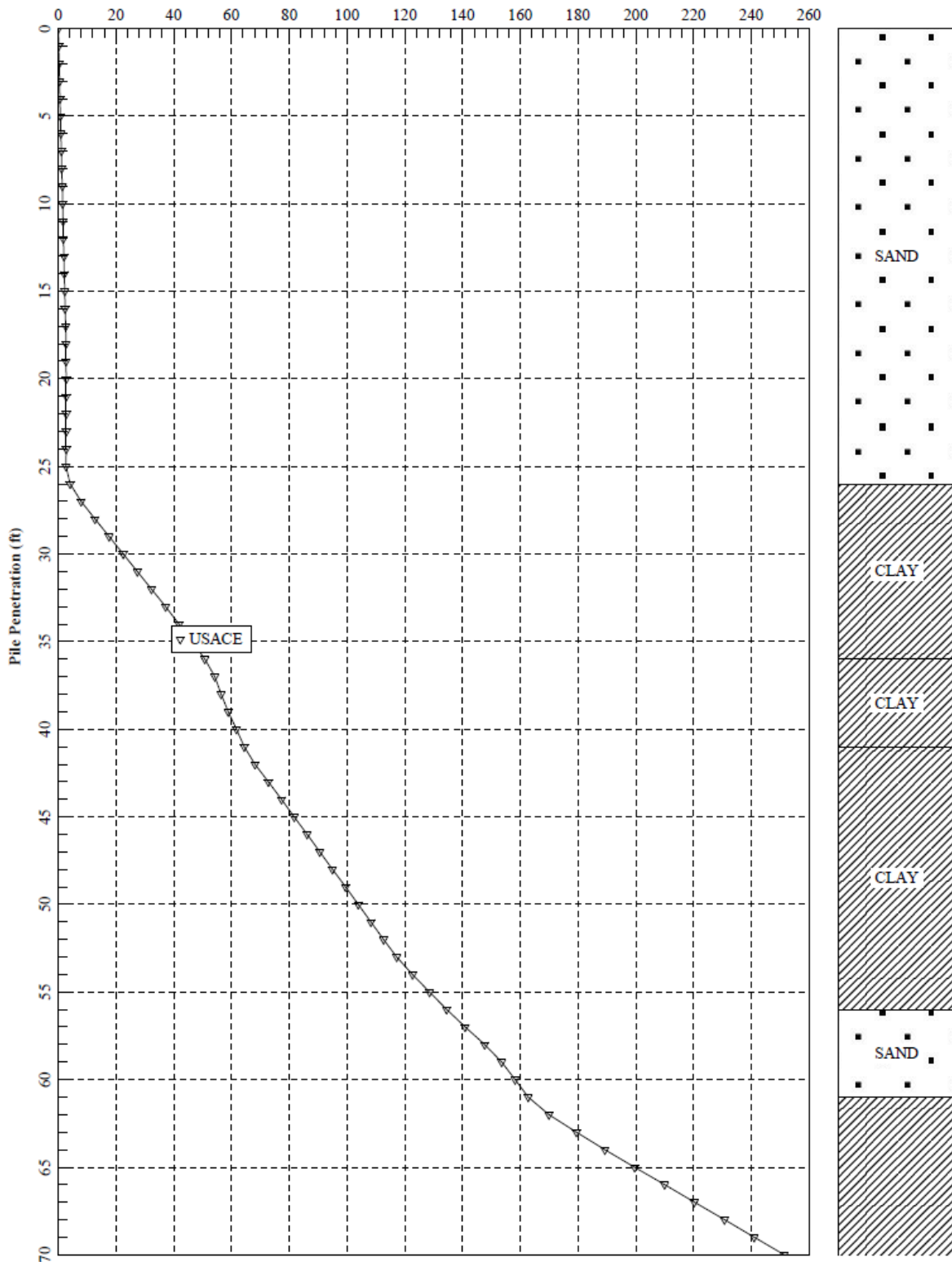
ULTIMATE SKIN FRICTION CAPACITY
MORGANS POINT (BCC1) – BULKHEAD - SHEET PILE
NZ 38

PROJECT NO.:
HG1910092.2.1

DRAWING NO.:
PLATE K-1

Pile Top
El. +3.0' MLLW

Morgans Point - NZ 38
Total Capacity (kips)



Notes:

* Allowable axial compressive capacity can be calculated by applying a factor of safety to the total ultimate capacity. Factors of safety should be determined based on USACE EM1110-2-2906 Design of Pile Foundations.



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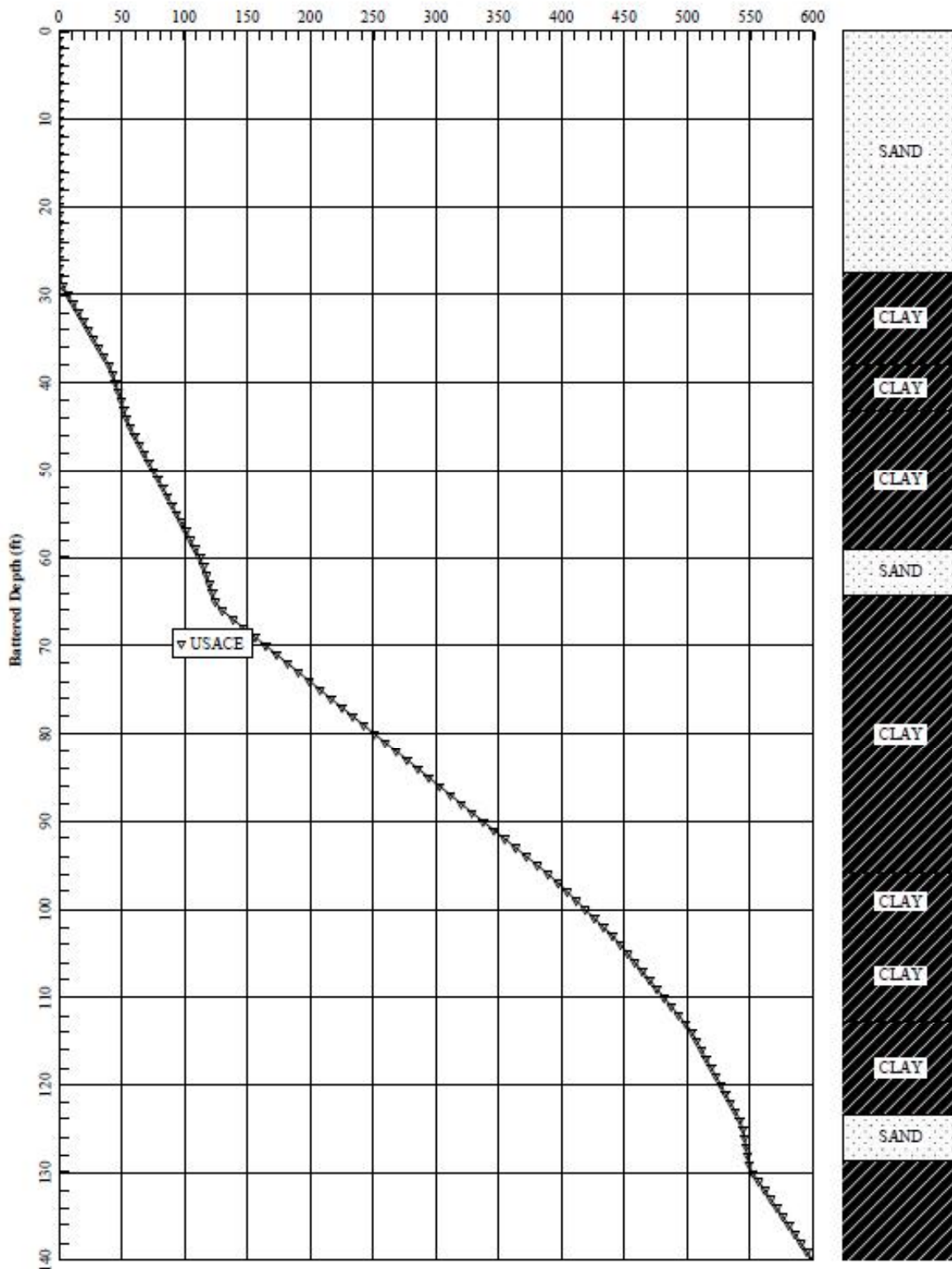
ULTIMATE COMPRESSIVE CAPACITY
MORGANS POINT (BCC1) - BULKHEAD - SHEET PILE
NZ 38

PROJECT NO.:
HG1910092.2.1

DRAWING NO.:
PLATE K-2

Pile Top
El. +3.0' ± B.O.M.L.W.

Morgans Point - Battered Pile HP 14x102
Accumulated Skin Friction (kips)



Notes:

* * Allowable axial tension capacity can be calculated by applying a factor of safety to the ultimate skin friction capacity. Factors of safety should be determined based on USACE EM1110-2-2906 Design of Pile Foundations.



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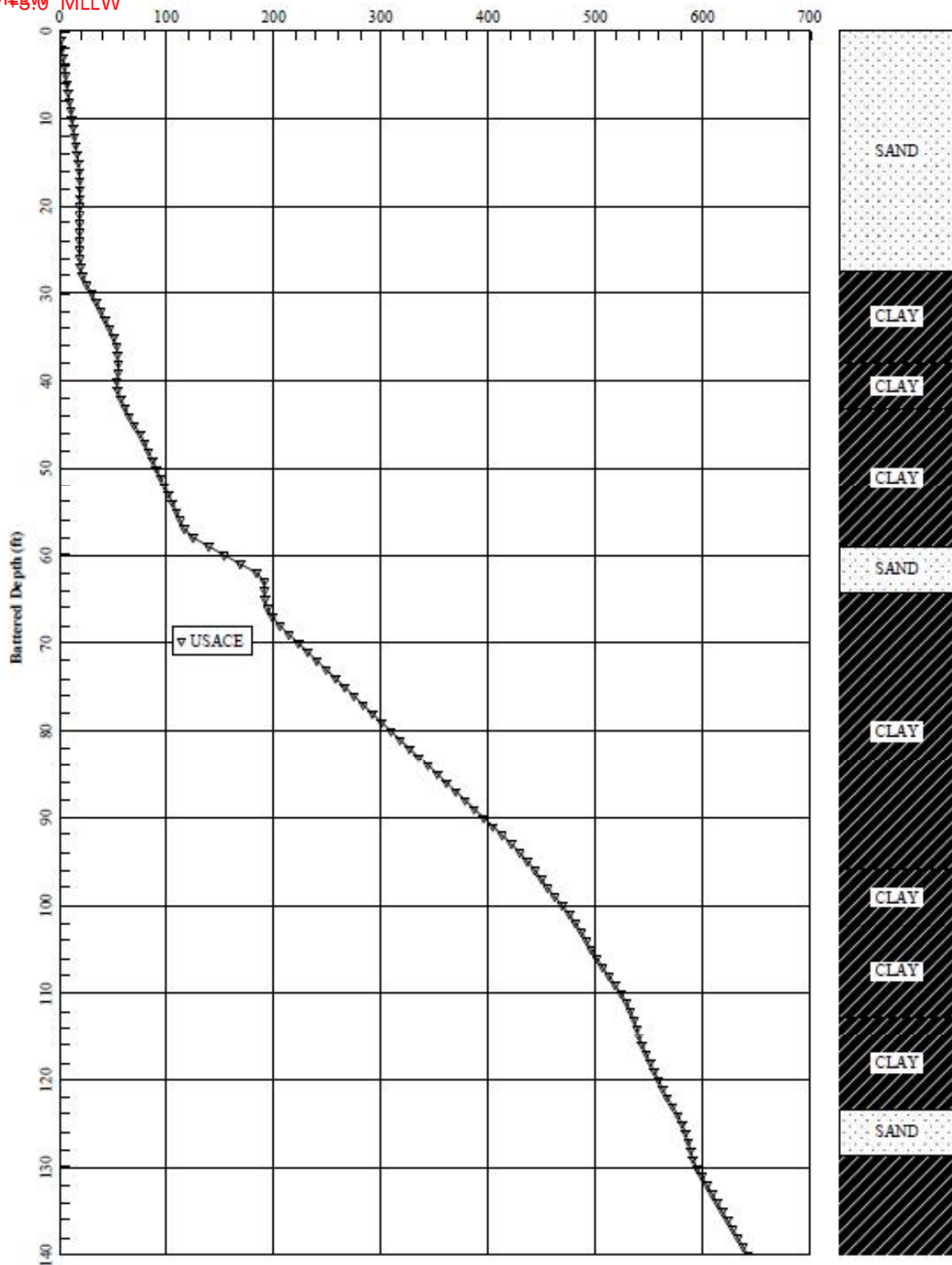
ULTIMATE SKIN FRICTION CAPACITY
MORGANS POINT (BCC1) - BULKHEAD -
BATTERED PILE HP 14 X 102

PROJECT NO.:
HG1910092.2.1

DRAWING NO.:
PLATE K-3

Pile Top
El. +3.0' MLLW

Morgans Point - Battered Pile HP 14x102
Total Capacity (kips)



Notes:

* Allowable axial compressive capacity can be calculated by applying a factor of safety to the total ultimate capacity. Factors of safety should be determined based on USACE EM1110-2-2906 Design of Pile Foundations.



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ULTIMATE COMPRESSIVE CAPACITY
MORGANS POINT (BCC1) – BULKHEAD –
BATTERED PILE HP 14 X 102

PROJECT NO.:
HG1910092.2.1

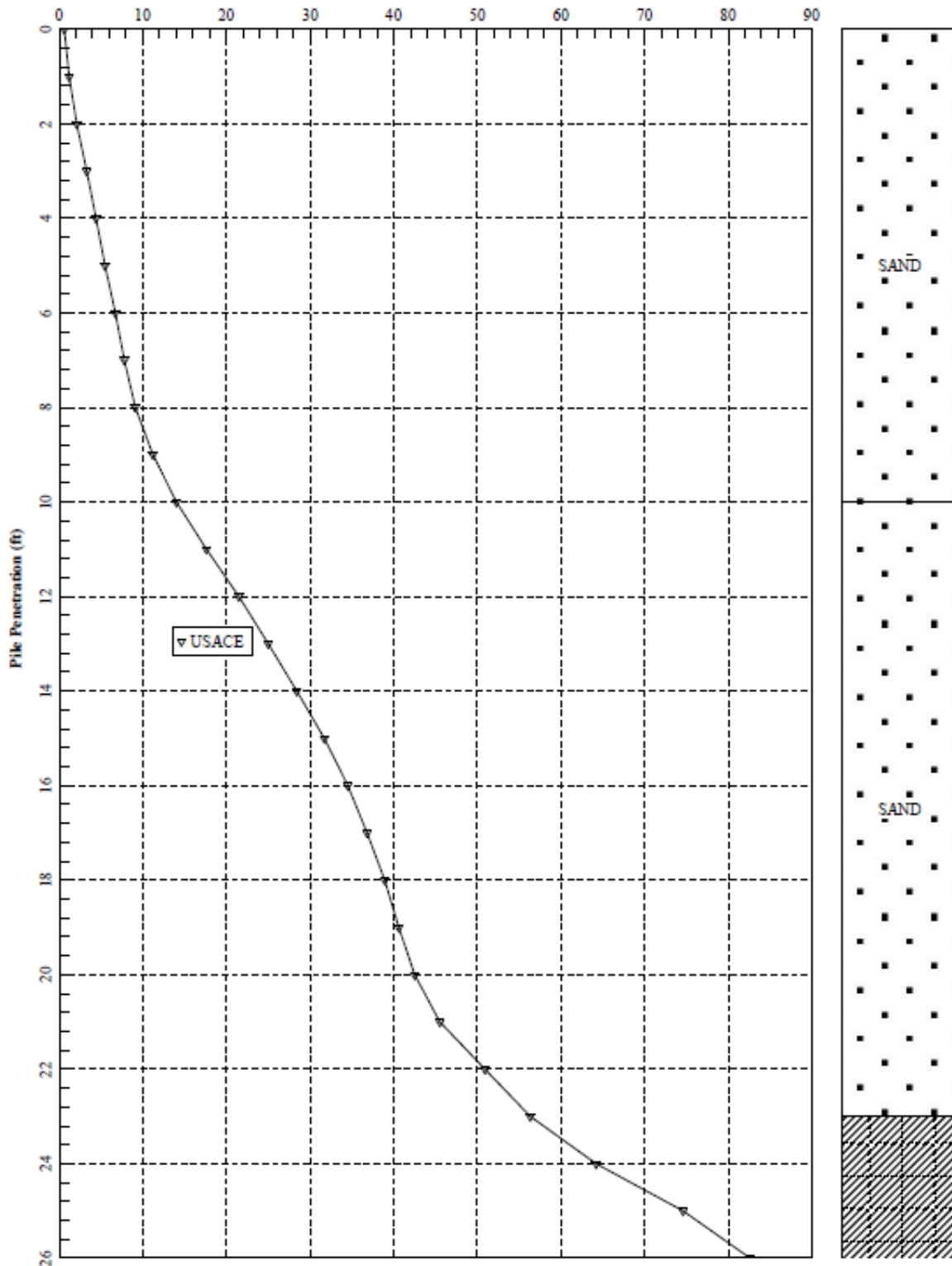
DRAWING NO.:
PLATE K-4

APPENDIX L

DRIVEN PILE AXIAL CAPACITY CURVES:
CELL M12

Soil Parameters for Driven Pile Design - Cell M12 Outfall					
Location & Boring Numbers	Soil Description	Depth, Feet		Total Unit Weight (γ), pcf	Undrained Shear Strength, psf/ Friction Angle (ϕ'), degrees
		Top	Bottom		
Cell M12 Placement Area – Approx. Station 73+00 (Boring ECP-1043)	Sand	0	10	110	26
	Sand	10	23	110	30
	Clay	23	30	130	3,000

Ultimate Compressive Capacity for HP14X89 Steel H-Pile near Dike CL Sta. 73+00, Boring ECP-1043
Total Capacity (kips)



Notes:

* Allowable axial compressive capacity can be calculated by applying a factor of safety to the total ultimate capacity. Factors of safety should be determined based on USACE EM1110-2-2906 Design of Pile Foundations.



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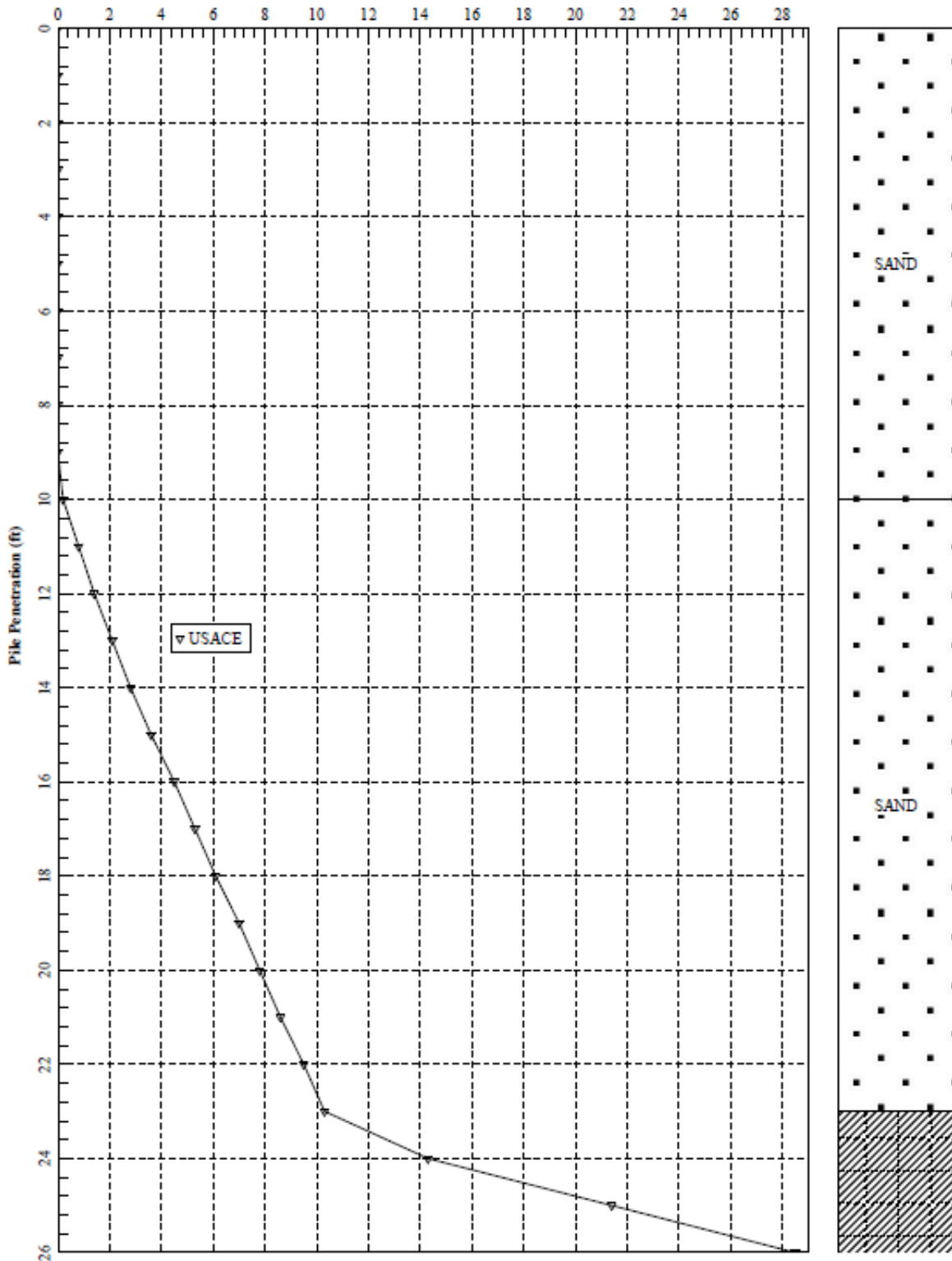
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ULTIMATE COMPRESSIVE CAPACITY
 OF HP14X89 STEEL H-PILE AT DIKE CL STA. 73+00
 BORING ECP-1043, CELL M12 PLACEMENT AREA

PROJECT NO.:
 HG1910092.2.1

DRAWING NO.:
 PLATE L-1

Ultimate Tensile Capacity for W8X40 Steel H-Pile near Dike CL Sta. 73+00, Boring ECP-1043
Accumulated Skin Friction (kips)



Notes:

* Allowable axial tension capacity can be calculated by applying a factor of safety to the ultimate skin friction capacity. Factors of safety should be determined based on USACE EM1110-2-2906 Design of Pile Foundations.



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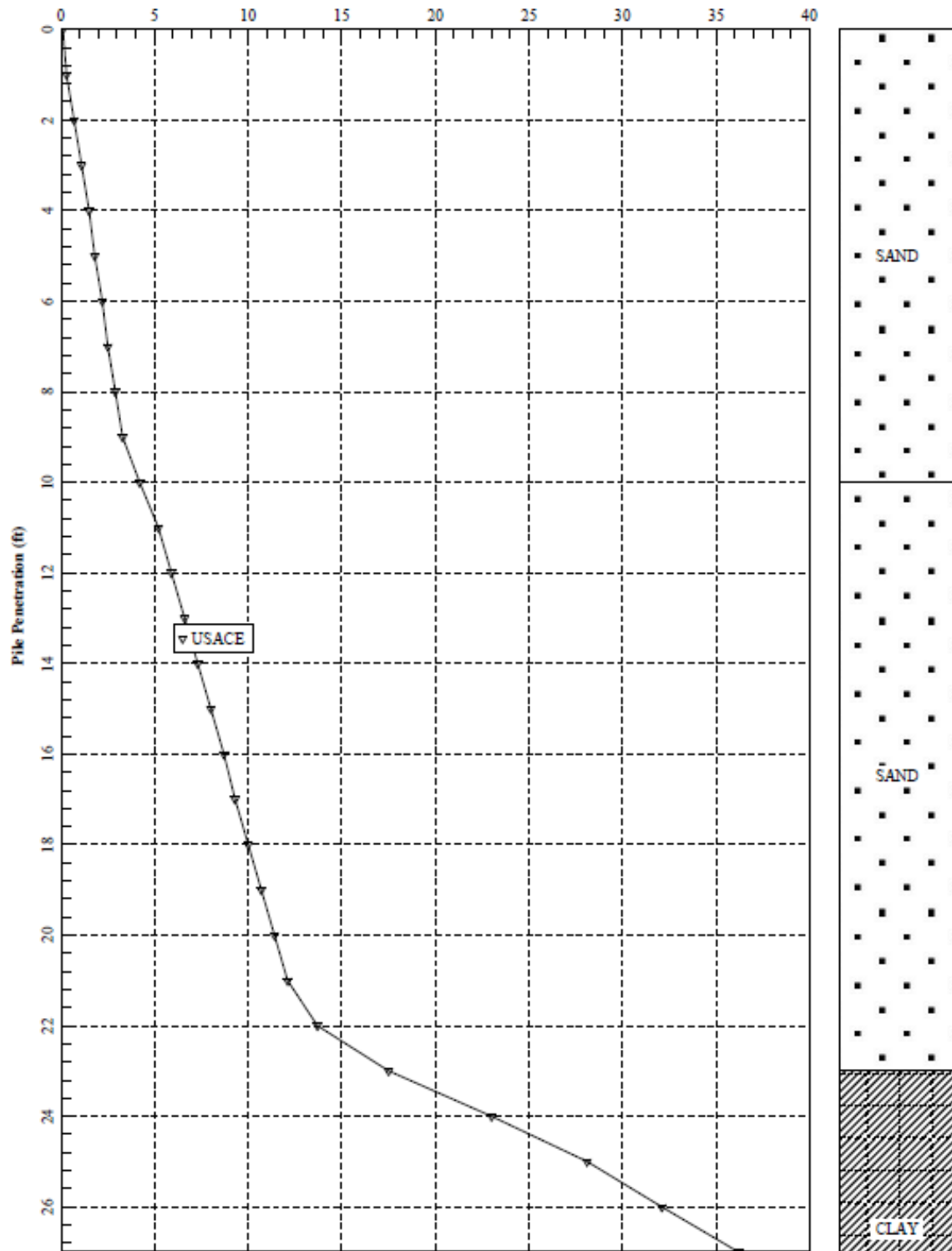
PREPARED BY:
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ULTIMATE AXIAL TENSION CAPACITY
OF HP14X89 STEEL H-PILE AT DIKE CL STA. 73+00
BORING ECP-1043, CELL M12 PLACEMENT AREA

PROJECT NO.:
HG1910092.2.1

DRAWING NO.:
PLATE L-2

Ultimate Compressive Capacity for W8X40 Steel H-Pile near Dike CL Sta. 73+00, Boring ECP-1043
Total Capacity (kips)



Notes:

* Allowable axial compressive capacity can be calculated by applying a factor of safety to the total ultimate capacity. Factors of safety should be determined based on USACE EM1110-2-2906 Design of Pile Foundations.



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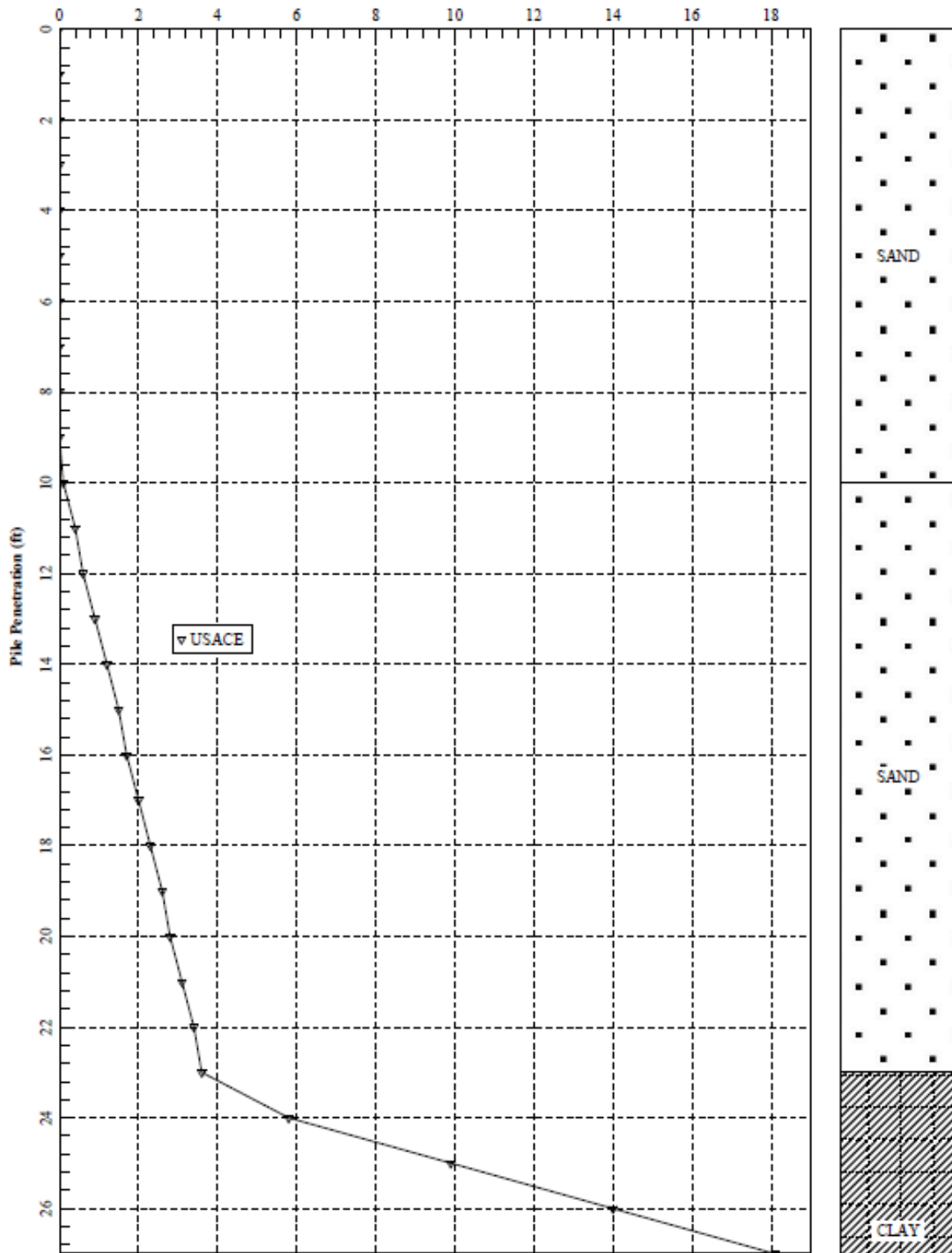
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ULTIMATE COMPRESSIVE CAPACITY
 OF W8X40 STEEL H-PILE AT DIKE CL STA. 73+00
 BORING ECP-1043, CELL M12 PLACEMENT AREA

PROJECT NO.:
 HG1910092.2.1

DRAWING NO.:
 PLATE L-3

Ultimate Tensile Capacity for W8X40 Steel H-Pile near Dike CL Sta. 73+00, Boring ECP-1043
Accumulated Skin Friction (lbf)



Notes:

* Allowable axial tension capacity can be calculated by applying a factor of safety to the ultimate skin friction capacity. Factors of safety should be determined based on USACE EM1110-2-2906 Design of Pile Foundations.



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ULTIMATE AXIAL TENSION CAPACITY
 OF W8X40 STEEL H-PILE AT DIKE CL STA. 73+00
 BORING ECP-1043, CELL M12 PLACEMENT AREA

PROJECT NO.:
 HG1910092.2.1

DRAWING NO.:
 PLATE L-4

APPENDIX M

SETTLE AND PSDDF ANALYSIS: CELL M12

RESULTS OF THE SETTLING ANALYSIS

TITLE: M12 BU Site Capacity - SI New Work - Boring AM-5

Initial storage results using compression settling test data:

Maximum in situ volume	2518727.50 cu yd
------------------------	------------------

Clarification results using zone settling test data:

No calculations were made.

Effluent quality results using flocculent settling test data:

No calculations were made.

Compression settling calculations for maximum in situ volume of material that can be disposed at the specified rate into a given CDF:

$$VOL = AREA * [DH - FB - (PD * \%P / 100\%)]$$

Assume a NTIME, iteratively solve for DTIME and substitute it for NTIME.

$$CEND = A * (NTIME / 2.0)^B$$

$$VOL_F = \frac{DTIME * OPHR * OPD * PRATE * CSITU * FFRAC}{7 * CEND * 100\%}$$

$$VOL_C = \frac{DTIME * OPHR * OPD * PRATE * CSITU * (100\% - FFRAC)}{7 * CSAND * 100\%}$$

$$NVOL = VOL_F + VOL_C$$

$$DTIME = \frac{VOL}{NVOL} * NTIME$$

After convergence,

$$DVOL = PRATE * DTIME * OPHR * OPD / 7$$

where

AREA = minimum area required for initial storage (acres) =	250.00
DH = average dike height or CDF depth (ft) =	11.00
FB = depth of freeboard (ft) =	1.00
PD = average depth of ponding in ponded area (ft) =	1.00
%P = percent of storage area ponded =	100.00
VOL = available storage volume (acre ft), [NVOL is used.] =	2250.00
A, B = compression settling curve coefficients =	198.17, 0.1975
DTIME = disposal period (days), [NTIME is an estimate,] =	167.98
CEND = concentration of fines at end of disposal (g/l) =	475.42
OPHR = operating hours per day of active disposal =	17.00
OPD = average number of days of operation per week =	7.00
PRATE = dredge production rate (cu yd/hr) =	882.00
CSITU = solids concentration of the in situ material (g/l) =	1619.05
FFRAC = fine-grained fraction (percent by weight) =	14.00
VOLC = volume of sands at end of disposal (cu yd) =	2429358.
VOLF = volume of fines at end of disposal (cu yd) =	1200979.
CSAND = solids concentration of settled sands (g/l) =	1443.74
DVOL = in situ volume of the material (cu yd)	2518727.

RESULTS OF THE SETTLING ANALYSIS

TITLE: M12 BU Site Capacity - SI New Work - Boring AM-5 FG Marsh

Initial storage results using compression settling test data:

Maximum in situ volume	1630792.25 cu yd
------------------------	------------------

Clarification results using zone settling test data:

No calculations were made.

Effluent quality results using flocculent settling test data:

No calculations were made.

Compression settling calculations for maximum in situ volume of material that can be disposed at the specified rate into a given CDF:

$$VOL = AREA * [DH - FB - (PD * \%P / 100\%)]$$

Assume a NTIME, iteratively solve for DTIME and substitute it for NTIME.

$$CEND = A * (NTIME / 2.0)^B$$

$$VOL_F = \frac{DTIME * OPHR * OPD * PRATE * CSITU * FFRAC}{7 * CEND * 100\%}$$

$$VOL_C = \frac{DTIME * OPHR * OPD * PRATE * CSITU * (100\% - FFRAC)}{7 * CSAND * 100\%}$$

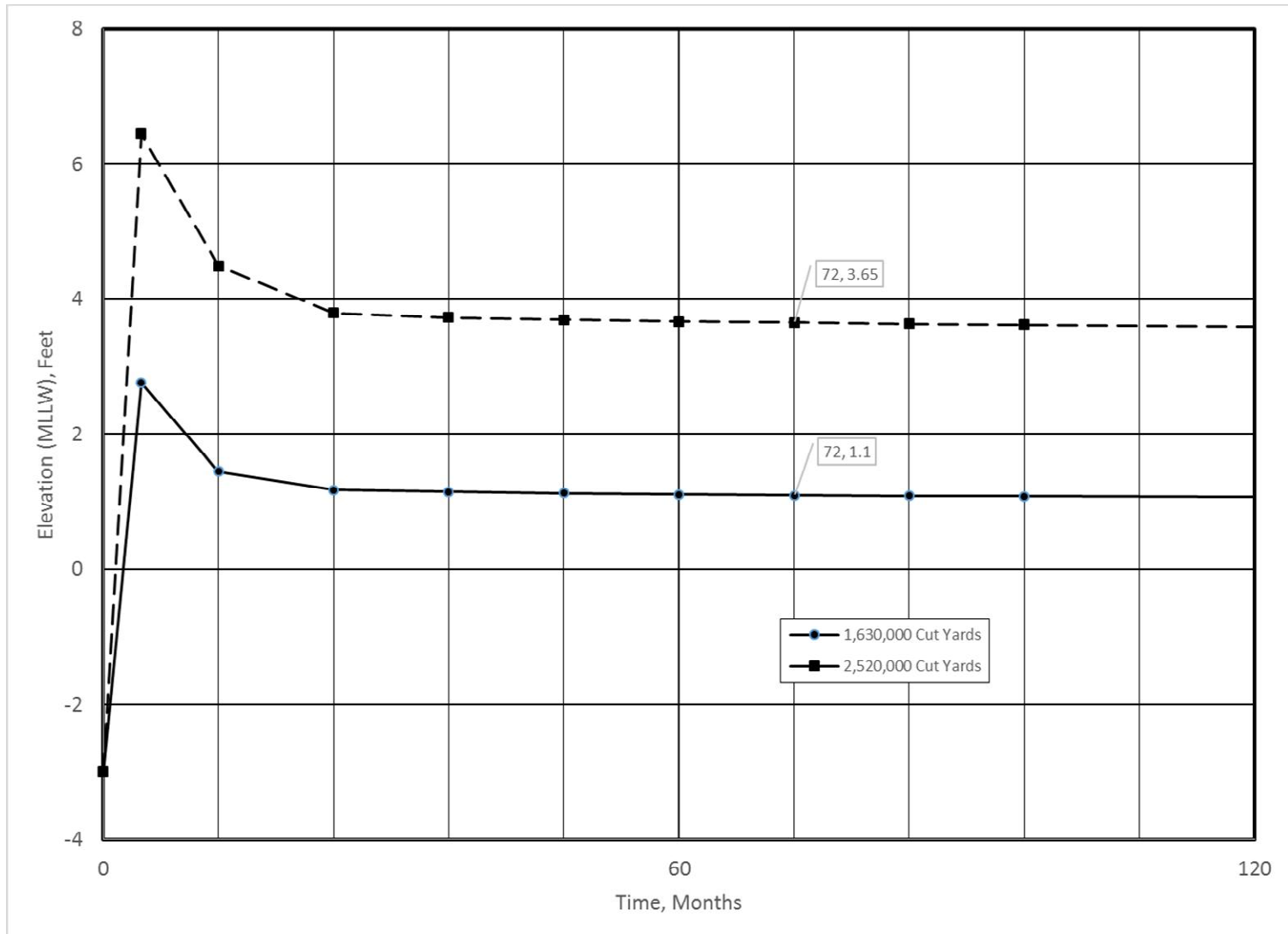
$$NVOL = VOL_F + VOL_C \quad DTIME = \frac{VOL}{NVOL} * NTIME$$

After convergence,

$$DVOL = PRATE * DTIME * OPHR * OPD / 7$$

where

AREA	= minimum area required for initial storage (acres) =	250.00
DH	= average dike height or CDF depth (ft) =	11.00
FB	= depth of freeboard (ft) =	2.00
PD	= average depth of ponding in ponded area (ft) =	3.00
%P	= percent of storage area ponded =	100.00
VOL	= available storage volume (acre ft), [NVOL is used.] =	1500.00
A, B	= compression settling curve coefficients =	198.17, 0.1975
DTIME	= disposal period (days), [NTIME is an estimate,] =	108.76
CEND	= concentration of fines at end of disposal (g/l) =	436.31
OPHR	= operating hours per day of active disposal =	17.00
OPD	= average number of days of operation per week =	7.00
PRATE	= dredge production rate (cu yd/hr) =	882.00
CSITU	= solids concentration of the in situ material (g/l) =	1619.05
FFRAC	= fine-grained fraction (percent by weight) =	14.00
VOLC	= volume of sands at end of disposal (cu yd) =	1572968.
VOLF	= volume of fines at end of disposal (cu yd) =	847318.
CSAND	= solids concentration of settled sands (g/l) =	1443.74
DVOL	= in situ volume of the material (cu yd)	1630792.



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SITE CAPACITY
M12 PLACEMENT AREA
HOUSTON SHIP CHANNEL EXPANSION CHANNEL
IMPROVEMENT PROJECT

PROJECT NO.:

HG1910092.2.1

DRAWING NO.:

PLATE M-1

 Consolidation and desiccation of soft layers---dredged fill

Problem M12 Settlement 2,520,000 Cut Cubic Yards

*****Soil data for compressible foundation*****

Material Type	Layer Thickness	Numbers of Sub-layers	Ca/Cc	Cr/Cc
1	15.00	4	.040	.150

Material type : 1 Specific Gravity of Solids: 2.70

	Void Ratio	Effective Stress	Perm- eability	k/1+e PK	Beta	Dsde	Alpha
I							
1	3.000	.000E+00	.350E-02	.875E-03	.105E-02	-.400E-01	-.350E-04
2	2.750	.100E-01	.230E-02	.613E-03	.893E-03	-.160E+00	-.981E-04
3	2.500	.800E-01	.150E-02	.429E-03	.673E-03	-.580E+00	-.249E-03
4	2.250	.300E+00	.900E-03	.277E-03	.524E-03	-.344E+01	-.953E-03
5	2.000	.180E+01	.500E-03	.167E-03	.336E-03	-.154E+02	-.257E-02
6	1.750	.800E+01	.300E-03	.109E-03	.213E-03	-.964E+02	-.105E-01
7	1.500	.500E+02	.150E-03	.600E-04	.156E-03	-.784E+03	-.470E-01
8	1.250	.400E+03	.700E-04	.311E-04	.900E-04	-.390E+04	-.121E+00
9	1.000	.200E+04	.300E-04	.150E-04	.644E-04	-.640E+04	-.960E-01

*****Soil data for dredged fill*****

Material Type	Specific Gravity	Ca/Cc	Cr/Cc	Saturation Limit	Disication Limit
------------------	---------------------	-------	-------	---------------------	---------------------

M12FIN.PSO

2 2.690 .040 .150 3.400 2.500

Material type : 2

	Void	Effective	Perm-	k/1+e			
I	Ratio	Stress	ability	PK	Beta	Dsde	Alpha
1	10.000	.000E+00	.240E+00	.218E-01	.182E-02	-.150E+00	-.327E-02
2	9.000	.150E+00	.200E+00	.200E-01	.258E-02	-.200E+00	-.400E-02
3	8.000	.400E+00	.150E+00	.167E-01	.437E-02	-.275E+00	-.458E-02
4	7.000	.700E+00	.900E-01	.113E-01	.448E-02	-.550E+00	-.619E-02
5	6.000	.150E+01	.540E-01	.771E-02	.313E-02	-.165E+01	-.127E-01
6	5.000	.400E+01	.300E-01	.500E-02	.367E-02	-.143E+02	-.712E-01
7	4.000	.300E+02	.190E-02	.380E-03	.247E-02	-.198E+03	-.752E-01
8	3.000	.400E+03	.200E-03	.500E-04	.188E-03	-.249E+04	-.124E+00
9	2.000	.500E+04	.100E-04	.333E-05	.467E-04	-.460E+04	-.153E-01

Summary of lifts and print detail

Time	Material	Fill	# Sub-	Void	Start	Dessic.	Print
days	Type	Height	layers	ratio	Day	Month	detai
0.	2	11.6	50	6.00	180.	1	1
120.					180.	1	1
365.					180.	1	1
730.					180.	1	1
1095.					180.	1	1
1460.					180.	1	2
1825.					180.	1	2
2190.					180.	1	2
2555.					180.	1	2
2920.					180.	1	2
3650.					180.	1	2

Summary of monthly rainfall and evaporation potential

Month	Rainfall	Evaporation
1	.250	.340

	M12FIN.PSO	
2	.200	.330
3	.180	.470
4	.220	.580
5	.280	.670
6	.290	.800
7	.310	.780
8	.370	.800
9	.490	.600
10	.220	.520
11	.270	.350
12	.300	.280

*****Calculation data*****

tau	Lower layer Void ratio	Lower layer Permeability	drainage path Length
.276	.900	.10000E-01	z = 2.77

Summary of desiccation parameters

Parameter	Value
Surface Drainage Efficiency	.70
maximum evaporation efficiency	.50
saturation at desiccation limit	.50
maximum crust thickness	.50
time to desic. after initial fill	180.00
month of initial desiccation	1
elevation of fixed water table	-5.00
elevation of top of incompres. found.	-18.00

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*****Initial Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
15.57	15.57	6.36	3.00	3.00	1.41	1
10.85	10.85	4.77	1.41	1.41	1.29	1
7.12	7.12	3.18	1.29	1.29	1.23	1
3.53	3.53	1.59	1.23	1.23	1.21	1
.00	.00	.00	1.21	1.21	1.18	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	
Material						
15.57	907.24	.00	907.24	730.80	176.44	1
10.85	1374.82	170.24	1204.58	1028.15	176.44	1
7.12	1780.08	340.47	1439.61	1263.17	176.44	1
3.53	2176.50	510.71	1665.79	1489.35	176.44	1
.00	2568.83	680.95	1887.88	1711.45	176.44	1

Time = 0. Degree of Consolidation = 0.0%

Total Settlement = .000

Settlement at End of Primary Consolidation = 1.247

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

*****Initial Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
11.60	11.60	1.66	6.00	6.00	10.00	2

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11.37	11.37	1.62	6.00	6.00	5.19	2
11.14	11.14	1.59	6.00	6.00	4.88	2
10.90	10.90	1.56	6.00	6.00	4.75	2
10.67	10.67	1.52	6.00	6.00	4.61	2
10.44	10.44	1.49	6.00	6.00	4.48	2
10.21	10.21	1.46	6.00	6.00	4.34	2
9.98	9.98	1.43	6.00	6.00	4.20	2
9.74	9.74	1.39	6.00	6.00	4.07	2
9.51	9.51	1.36	6.00	6.00	4.00	2
9.28	9.28	1.33	6.00	6.00	3.99	2
9.05	9.05	1.29	6.00	6.00	3.98	2
8.82	8.82	1.26	6.00	6.00	3.97	2
8.58	8.58	1.23	6.00	6.00	3.96	2
8.35	8.35	1.19	6.00	6.00	3.95	2
8.12	8.12	1.16	6.00	6.00	3.94	2
7.89	7.89	1.13	6.00	6.00	3.93	2
7.66	7.66	1.09	6.00	6.00	3.92	2
7.42	7.42	1.06	6.00	6.00	3.91	2
7.19	7.19	1.03	6.00	6.00	3.90	2
6.96	6.96	.99	6.00	6.00	3.89	2
6.73	6.73	.96	6.00	6.00	3.88	2
6.50	6.50	.93	6.00	6.00	3.87	2
6.26	6.26	.89	6.00	6.00	3.86	2
6.03	6.03	.86	6.00	6.00	3.85	2
5.80	5.80	.83	6.00	6.00	3.84	2
5.57	5.57	.80	6.00	6.00	3.83	2
5.34	5.34	.76	6.00	6.00	3.82	2
5.10	5.10	.73	6.00	6.00	3.81	2
4.87	4.87	.70	6.00	6.00	3.80	2
4.64	4.64	.66	6.00	6.00	3.79	2
4.41	4.41	.63	6.00	6.00	3.79	2
4.18	4.18	.60	6.00	6.00	3.78	2
3.94	3.94	.56	6.00	6.00	3.77	2
3.71	3.71	.53	6.00	6.00	3.76	2
3.48	3.48	.50	6.00	6.00	3.75	2
3.25	3.25	.46	6.00	6.00	3.74	2
3.02	3.02	.43	6.00	6.00	3.73	2
2.78	2.78	.40	6.00	6.00	3.72	2
2.55	2.55	.36	6.00	6.00	3.71	2
2.32	2.32	.33	6.00	6.00	3.70	2
2.09	2.09	.30	6.00	6.00	3.69	2
1.86	1.86	.27	6.00	6.00	3.68	2
1.62	1.62	.23	6.00	6.00	3.67	2
1.39	1.39	.20	6.00	6.00	3.66	2
1.16	1.16	.17	6.00	6.00	3.65	2
.93	.93	.13	6.00	6.00	3.64	2
.70	.70	.10	6.00	6.00	3.63	2
.46	.46	.07	6.00	6.00	3.62	2
.23	.23	.03	6.00	6.00	3.61	2
.00	.00	.00	6.00	6.00	3.60	2

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***** Stresses *****

***** Pore Pressures *****

XI Material	Total	Effective	Total	Static	Excess	
11.60	.00	.00	.00	.00	.00	2
11.37	18.14	.00	18.14	14.62	3.53	2
11.14	36.29	.00	36.29	29.23	7.06	2
10.90	54.43	.00	54.43	43.85	10.59	2
10.67	72.58	.00	72.58	58.46	14.11	2
10.44	90.72	.00	90.72	73.08	17.64	2
10.21	108.87	.00	108.87	87.70	21.17	2
9.98	127.01	.00	127.01	102.31	24.70	2
9.74	145.16	.00	145.16	116.93	28.23	2
9.51	163.30	.00	163.30	131.54	31.76	2
9.28	181.45	.00	181.45	146.16	35.29	2
9.05	199.59	.00	199.59	160.78	38.82	2
8.82	217.74	.00	217.74	175.39	42.34	2
8.58	235.88	.00	235.88	190.01	45.87	2
8.35	254.03	.00	254.03	204.62	49.40	2
8.12	272.17	.00	272.17	219.24	52.93	2
7.89	290.32	.00	290.32	233.86	56.46	2
7.66	308.46	.00	308.46	248.47	59.99	2
7.42	326.61	.00	326.61	263.09	63.52	2
7.19	344.75	.00	344.75	277.70	67.05	2
6.96	362.89	.00	362.89	292.32	70.57	2
6.73	381.04	.00	381.04	306.94	74.10	2
6.50	399.18	.00	399.18	321.55	77.63	2
6.26	417.33	.00	417.33	336.17	81.16	2
6.03	435.47	.00	435.47	350.78	84.69	2
5.80	453.62	.00	453.62	365.40	88.22	2
5.57	471.76	.00	471.76	380.02	91.75	2
5.34	489.91	.00	489.91	394.63	95.28	2
5.10	508.05	.00	508.05	409.25	98.80	2
4.87	526.20	.00	526.20	423.86	102.33	2
4.64	544.34	.00	544.34	438.48	105.86	2
4.41	562.49	.00	562.49	453.10	109.39	2
4.18	580.63	.00	580.63	467.71	112.92	2
3.94	598.78	.00	598.78	482.33	116.45	2
3.71	616.92	.00	616.92	496.94	119.98	2
3.48	635.07	.00	635.07	511.56	123.51	2
3.25	653.21	.00	653.21	526.18	127.03	2
3.02	671.35	.00	671.35	540.79	130.56	2
2.78	689.50	.00	689.50	555.41	134.09	2
2.55	707.64	.00	707.64	570.02	137.62	2
2.32	725.79	.00	725.79	584.64	141.15	2
2.09	743.93	.00	743.93	599.26	144.68	2
1.86	762.08	.00	762.08	613.87	148.21	2
1.62	780.22	.00	780.22	628.49	151.73	2
1.39	798.37	.00	798.37	643.10	155.26	2
1.16	816.51	.00	816.51	657.72	158.79	2

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.93	834.66	.00	834.66	672.34	162.32	2
.70	852.80	.00	852.80	686.95	165.85	2
.46	870.95	.00	870.95	701.57	169.38	2
.23	889.09	.00	889.09	716.18	172.91	2
.00	907.24	.00	907.24	730.80	176.44	2

Time = 0. Degree of Consolidation = 0.0%

Total Settlement = .000

Settlement at End of Primary Consolidation = 3.363

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
15.57	14.81	6.36	3.00	1.61	1.41	1
10.85	10.83	4.77	1.41	1.41	1.29	1
7.12	7.10	3.18	1.29	1.29	1.23	1
3.53	3.51	1.59	1.23	1.23	1.21	1
.00	.00	.00	1.21	1.18	1.18	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	
Material						
14.81	818.73	31.33	787.40	642.29	145.11	1
10.83	1239.90	172.73	1067.17	893.22	173.94	1
7.10	1644.98	340.47	1304.51	1128.07	176.44	1
3.51	2041.51	511.95	1529.56	1354.36	175.20	1
.00	2432.78	856.77	1576.01	1575.40	.61	1

Time = 120. Degree of Consolidation = 61.0%

Total Settlement = .755

Settlement at End of Primary Consolidation = 1.247

Settlement caused by Primary Consolidation at time 120. = .755

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Settlement caused by Secondary Compression at time 120. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
11.60	10.20	1.66	6.00	6.00	10.00	2
11.37	9.96	1.62	6.00	6.00	5.19	2
11.14	9.73	1.59	6.00	6.00	4.88	2
10.90	9.50	1.56	6.00	6.00	4.75	2
10.67	9.27	1.52	6.00	6.00	4.61	2
10.44	9.04	1.49	6.00	6.00	4.48	2
10.21	8.80	1.46	6.00	6.00	4.34	2
9.98	8.57	1.43	6.00	5.99	4.20	2
9.74	8.34	1.39	6.00	5.99	4.07	2
9.51	8.11	1.36	6.00	5.98	4.00	2
9.28	7.88	1.33	6.00	5.96	3.99	2
9.05	7.65	1.29	6.00	5.94	3.98	2
8.82	7.42	1.26	6.00	5.91	3.97	2
8.58	7.19	1.23	6.00	5.87	3.96	2
8.35	6.96	1.19	6.00	5.83	3.95	2
8.12	6.74	1.16	6.00	5.78	3.94	2
7.89	6.51	1.13	6.00	5.72	3.93	2
7.66	6.29	1.09	6.00	5.67	3.92	2
7.42	6.07	1.06	6.00	5.61	3.91	2
7.19	5.85	1.03	6.00	5.55	3.90	2
6.96	5.64	.99	6.00	5.48	3.89	2
6.73	5.42	.96	6.00	5.42	3.88	2
6.50	5.21	.93	6.00	5.36	3.87	2
6.26	5.00	.89	6.00	5.30	3.86	2
6.03	4.79	.86	6.00	5.24	3.85	2
5.80	4.59	.83	6.00	5.18	3.84	2
5.57	4.38	.80	6.00	5.13	3.83	2
5.34	4.18	.76	6.00	5.07	3.82	2
5.10	3.98	.73	6.00	5.02	3.81	2
4.87	3.78	.70	6.00	4.96	3.80	2
4.64	3.59	.66	6.00	4.91	3.79	2
4.41	3.39	.63	6.00	4.86	3.79	2
4.18	3.20	.60	6.00	4.81	3.78	2
3.94	3.01	.56	6.00	4.75	3.77	2
3.71	2.82	.53	6.00	4.70	3.76	2
3.48	2.63	.50	6.00	4.65	3.75	2
3.25	2.44	.46	6.00	4.59	3.74	2

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3.02	2.26	.43	6.00	4.54	3.73	2
2.78	2.08	.40	6.00	4.49	3.72	2
2.55	1.89	.36	6.00	4.44	3.71	2
2.32	1.71	.33	6.00	4.39	3.70	2
2.09	1.54	.30	6.00	4.34	3.69	2
1.86	1.36	.27	6.00	4.29	3.68	2
1.62	1.19	.23	6.00	4.25	3.67	2
1.39	1.01	.20	6.00	4.20	3.66	2
1.16	.84	.17	6.00	4.16	3.65	2
.93	.67	.13	6.00	4.12	3.64	2
.70	.50	.10	6.00	4.09	3.63	2
.46	.33	.07	6.00	4.05	3.62	2
.23	.17	.03	6.00	4.02	3.61	2
.00	.00	.00	6.00	4.00	3.60	2

***** Stresses *****

***** Pore Pressures *****

XI Material	Total	Effective	Total	Static	Excess	
10.20	.00	.00	.00	.00	.00	2
9.96	18.14	1.50	16.64	14.62	2.03	2
9.73	36.29	1.50	34.79	29.23	5.56	2
9.50	54.43	1.50	52.93	43.85	9.08	2
9.27	72.57	1.50	71.07	58.46	12.61	2
9.04	90.72	1.51	89.21	73.07	16.14	2
8.80	108.85	1.51	107.34	87.68	19.66	2
8.57	126.98	1.52	125.46	102.28	23.18	2
8.34	145.11	1.54	143.57	116.88	26.69	2
8.11	163.21	1.56	161.65	131.45	30.20	2
7.88	181.29	1.60	179.69	146.00	33.69	2
7.65	199.33	1.65	197.68	160.52	37.17	2
7.42	217.32	1.72	215.60	174.98	40.62	2
7.19	235.24	1.82	233.43	189.37	44.06	2
6.96	253.08	1.93	251.15	203.68	47.47	2
6.74	270.81	2.05	268.76	217.88	50.88	2
6.51	288.44	2.19	286.25	231.98	54.27	2
6.29	305.95	2.33	303.62	245.96	57.65	2
6.07	323.34	2.48	320.85	259.82	61.03	2
5.85	340.59	2.64	337.96	273.55	64.41	2
5.64	357.72	2.79	354.93	287.15	67.78	2
5.42	374.73	2.95	371.78	300.62	71.16	2
5.21	391.60	3.10	388.50	313.97	74.53	2
5.00	408.35	3.25	405.10	327.18	77.91	2
4.79	424.97	3.40	421.57	340.28	81.29	2
4.59	441.47	3.54	437.92	353.25	84.67	2
4.38	457.84	3.69	454.16	366.10	88.06	2
4.18	474.11	3.82	470.28	378.83	91.45	2
3.98	490.25	3.96	486.30	391.45	94.85	2
3.78	506.29	4.93	501.36	403.96	97.41	2
3.59	522.22	6.29	515.92	416.36	99.57	2

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3.39	538.04	7.67	530.37	428.64	101.72	2
3.20	553.74	9.05	544.69	440.82	103.87	2
3.01	569.34	10.43	558.91	452.89	106.02	2
2.82	584.82	11.81	573.01	464.85	108.16	2
2.63	600.20	13.19	587.00	476.69	110.31	2
2.44	615.46	14.56	600.90	488.43	112.47	2
2.26	630.61	15.93	614.69	500.05	114.64	2
2.08	645.66	17.27	628.39	511.57	116.82	2
1.89	660.60	18.59	642.00	522.98	119.03	2
1.71	675.43	19.89	655.54	534.28	121.26	2
1.54	690.16	21.15	669.00	545.48	123.52	2
1.36	704.79	22.38	682.41	556.58	125.83	2
1.19	719.32	23.56	695.76	567.59	128.18	2
1.01	733.76	24.69	709.07	578.50	130.58	2
.84	748.11	25.76	722.36	589.32	133.03	2
.67	762.38	26.77	735.61	600.06	135.55	2
.50	776.57	27.71	748.86	610.72	138.14	2
.33	790.69	28.58	762.11	621.31	140.80	2
.17	804.74	29.38	775.36	631.83	143.53	2
.00	818.73	31.33	787.40	642.29	145.11	2

Time = 120. Degree of Consolidation = 42.%

Total Settlement = 1.405

Settlement at End of Primary Consolidation = 3.363

Settlement caused by Primary Consolidation at time 120. = 1.405

Settlement caused by Secondary Compression at time 120. = .000

Surface Elevation = 6.44

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
15.57	14.72	6.36	3.00	1.48	1.40	1
10.85	10.82	4.77	1.41	1.40	1.28	1
7.12	7.10	3.18	1.29	1.29	1.23	1
3.53	3.51	1.59	1.23	1.23	1.20	1
.00	.00	.00	1.21	1.18	1.18	1

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***** Stresses ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	
Material						
14.72	705.37	83.20	622.17	501.78	120.39	1
10.82	1121.19	185.03	936.16	747.36	188.79	1
7.10	1525.95	340.47	1185.47	981.88	203.59	1
3.51	1922.50	514.66	1407.84	1208.20	199.65	1
.00	2313.60	873.95	1439.65	1429.06	10.59	1

Time = 365. Degree of Consolidation = 66.0%

Total Settlement = .847

Settlement at End of Primary Consolidation = 1.288

Settlement caused by Primary Consolidation at time 365. = .847

Settlement caused by Secondary Compression at time 365. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	
Material						
11.60	8.34	1.66	6.00	2.50	2.50	2
11.37	8.22	1.62	6.00	2.50	2.50	2
11.14	8.11	1.59	6.00	2.50	2.50	2
10.90	7.96	1.56	6.00	4.00	4.11	2
10.67	7.80	1.52	6.00	4.20	4.00	2
10.44	7.62	1.49	6.00	4.27	3.99	2
10.21	7.45	1.46	6.00	4.32	3.98	2
9.98	7.27	1.43	6.00	4.35	3.97	2
9.74	7.09	1.39	6.00	4.37	3.96	2
9.51	6.91	1.36	6.00	4.37	3.95	2
9.28	6.74	1.33	6.00	4.36	3.94	2
9.05	6.56	1.29	6.00	4.35	3.93	2
8.82	6.38	1.26	6.00	4.34	3.92	2
8.58	6.20	1.23	6.00	4.32	3.91	2
8.35	6.03	1.19	6.00	4.30	3.90	2
8.12	5.85	1.16	6.00	4.29	3.89	2
7.89	5.68	1.13	6.00	4.27	3.88	2
7.66	5.50	1.09	6.00	4.25	3.87	2
7.42	5.33	1.06	6.00	4.24	3.86	2
7.19	5.16	1.03	6.00	4.22	3.86	2

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6.96	4.98	.99	6.00	4.21	3.85	2
6.73	4.81	.96	6.00	4.19	3.84	2
6.50	4.64	.93	6.00	4.17	3.83	2
6.26	4.47	.89	6.00	4.16	3.82	2
6.03	4.30	.86	6.00	4.14	3.81	2
5.80	4.13	.83	6.00	4.13	3.80	2
5.57	3.96	.80	6.00	4.12	3.79	2
5.34	3.79	.76	6.00	4.10	3.78	2
5.10	3.62	.73	6.00	4.09	3.77	2
4.87	3.45	.70	6.00	4.08	3.76	2
4.64	3.28	.66	6.00	4.06	3.75	2
4.41	3.12	.63	6.00	4.05	3.74	2
4.18	2.95	.60	6.00	4.04	3.73	2
3.94	2.78	.56	6.00	4.03	3.72	2
3.71	2.62	.53	6.00	4.01	3.71	2
3.48	2.45	.50	6.00	4.00	3.70	2
3.25	2.28	.46	6.00	3.99	3.69	2
3.02	2.12	.43	6.00	3.98	3.68	2
2.78	1.95	.40	6.00	3.97	3.67	2
2.55	1.79	.36	6.00	3.96	3.66	2
2.32	1.62	.33	6.00	3.95	3.65	2
2.09	1.46	.30	6.00	3.94	3.65	2
1.86	1.30	.27	6.00	3.93	3.64	2
1.62	1.13	.23	6.00	3.92	3.63	2
1.39	.97	.20	6.00	3.91	3.62	2
1.16	.81	.17	6.00	3.90	3.61	2
.93	.65	.13	6.00	3.89	3.60	2
.70	.48	.10	6.00	3.88	3.59	2
.46	.32	.07	6.00	3.87	3.58	2
.23	.16	.03	6.00	3.87	3.57	2
.00	.00	.00	6.00	3.86	3.56	2

***** Stresses *****

***** Pore Pressures *****

XI Material	Total	Effective	Total	Static	Excess	
8.34	.00	.00	.00	.00	.00	2
8.22	8.23	8.23	.00	.00	.00	2
8.11	16.45	16.45	.00	.00	.00	2
7.96	27.16	27.16	.00	.00	.00	2
7.80	41.36	24.82	16.54	10.68	5.86	2
7.62	55.82	22.95	32.88	21.61	11.27	2
7.45	70.42	21.62	48.80	32.67	16.13	2
7.27	85.09	20.81	64.28	43.82	20.46	2
7.09	99.82	20.45	79.37	55.02	24.35	2
6.91	114.56	20.42	94.14	66.23	27.91	2
6.74	129.29	20.60	108.69	77.43	31.26	2
6.56	144.00	20.91	123.09	88.61	34.48	2
6.38	158.68	21.28	137.40	99.77	37.63	2
6.20	173.34	21.69	151.64	110.89	40.75	2

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6.03	187.96	22.12	165.84	121.98	43.86	2
5.85	202.54	22.55	180.00	133.04	46.96	2
5.68	217.09	22.97	194.12	144.06	50.06	2
5.50	231.61	23.40	208.21	155.05	53.16	2
5.33	246.09	23.83	222.26	166.00	56.26	2
5.16	260.54	24.24	236.29	176.92	59.37	2
4.98	274.95	24.66	250.29	187.81	62.49	2
4.81	289.33	25.07	264.27	198.66	65.61	2
4.64	303.68	25.47	278.21	209.48	68.74	2
4.47	318.00	25.86	292.14	220.27	71.87	2
4.30	332.28	26.24	306.04	231.02	75.02	2
4.13	346.54	26.62	319.92	241.75	78.17	2
3.96	360.76	26.99	333.78	252.45	81.33	2
3.79	374.96	27.35	347.62	263.11	84.50	2
3.62	389.13	27.70	361.43	273.75	87.68	2
3.45	403.27	28.04	375.23	284.37	90.86	2
3.28	417.38	28.37	389.01	294.95	94.06	2
3.12	431.47	28.70	402.77	305.51	97.26	2
2.95	445.53	29.02	416.51	316.04	100.47	2
2.78	459.56	29.33	430.23	326.54	103.69	2
2.62	473.57	29.63	443.94	337.03	106.91	2
2.45	487.56	29.93	457.63	347.48	110.14	2
2.28	501.52	33.17	468.36	357.92	110.44	2
2.12	515.46	37.19	478.27	368.33	109.94	2
1.95	529.38	41.12	488.25	378.72	109.54	2
1.79	543.27	44.96	498.31	389.08	109.23	2
1.62	557.15	48.71	508.43	399.43	109.01	2
1.46	571.00	52.39	518.61	409.75	108.86	2
1.30	584.83	56.00	528.83	420.06	108.78	2
1.13	598.64	59.55	539.10	430.34	108.76	2
.97	612.44	63.04	549.39	440.60	108.79	2
.81	626.21	66.49	559.72	450.85	108.87	2
.65	639.96	69.89	570.07	461.07	109.00	2
.48	653.70	73.26	580.43	471.28	109.16	2
.32	667.41	76.60	590.81	481.46	109.35	2
.16	681.11	79.91	601.20	491.63	109.57	2
.00	694.78	83.20	611.59	501.78	109.81	2

Time = 365. Degree of Consolidation = 79.0%

Total Settlement = 3.256

Settlement at End of Primary Consolidation = 3.763

Settlement caused by Primary Consolidation at time 365. = 2.991

Settlement caused by Secondary Compression at time 365. = .000

Settlement Due to Desiccation = .265

Surface Elevation = 4.50

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
15.57	14.63	6.36	3.00	1.40	1.40	1
10.85	10.81	4.77	1.41	1.39	1.27	1
7.12	7.10	3.18	1.29	1.29	1.23	1
3.53	3.50	1.59	1.23	1.23	1.20	1
.00	.00	.00	1.21	1.18	1.18	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	
Material						
14.63	667.11	195.82	471.29	457.18	14.11	1
10.81	1078.46	210.89	867.57	698.28	169.28	1
7.10	1482.54	340.47	1142.06	932.13	209.94	1
3.50	1879.11	521.24	1357.87	1158.46	199.41	1
.00	2270.04	876.77	1393.27	1379.16	14.11	1

Time = 730. Degree of Consolidation = 72.%

Total Settlement = .931

Settlement at End of Primary Consolidation = 1.295

Settlement caused by Primary Consolidation at time 730. = .931

Settlement caused by Secondary Compression at time 730. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
11.60	7.72	1.66	6.00	2.50	2.50	2

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11.37	7.61	1.62	6.00	2.50	2.50	2
11.14	7.49	1.59	6.00	2.50	2.50	2
10.90	7.37	1.56	6.00	2.50	2.50	2
10.67	7.26	1.52	6.00	2.79	3.99	2
10.44	7.10	1.49	6.00	3.98	3.98	2
10.21	6.94	1.46	6.00	3.97	3.97	2
9.98	6.78	1.43	6.00	3.96	3.96	2
9.74	6.61	1.39	6.00	3.95	3.95	2
9.51	6.45	1.36	6.00	3.94	3.94	2
9.28	6.28	1.33	6.00	3.93	3.93	2
9.05	6.12	1.29	6.00	3.92	3.92	2
8.82	5.96	1.26	6.00	3.91	3.91	2
8.58	5.80	1.23	6.00	3.90	3.90	2
8.35	5.63	1.19	6.00	3.89	3.90	2
8.12	5.47	1.16	6.00	3.88	3.89	2
7.89	5.31	1.13	6.00	3.87	3.88	2
7.66	5.15	1.09	6.00	3.86	3.87	2
7.42	4.99	1.06	6.00	3.85	3.86	2
7.19	4.83	1.03	6.00	3.84	3.85	2
6.96	4.67	.99	6.00	3.84	3.84	2
6.73	4.51	.96	6.00	3.83	3.83	2
6.50	4.35	.93	6.00	3.82	3.82	2
6.26	4.19	.89	6.00	3.81	3.81	2
6.03	4.03	.86	6.00	3.80	3.80	2
5.80	3.87	.83	6.00	3.79	3.79	2
5.57	3.71	.80	6.00	3.78	3.78	2
5.34	3.55	.76	6.00	3.77	3.77	2
5.10	3.39	.73	6.00	3.76	3.76	2
4.87	3.24	.70	6.00	3.75	3.75	2
4.64	3.08	.66	6.00	3.74	3.74	2
4.41	2.92	.63	6.00	3.73	3.73	2
4.18	2.77	.60	6.00	3.72	3.72	2
3.94	2.61	.56	6.00	3.71	3.71	2
3.71	2.45	.53	6.00	3.70	3.70	2
3.48	2.30	.50	6.00	3.69	3.69	2
3.25	2.14	.46	6.00	3.68	3.69	2
3.02	1.99	.43	6.00	3.67	3.68	2
2.78	1.83	.40	6.00	3.66	3.67	2
2.55	1.68	.36	6.00	3.65	3.66	2
2.32	1.52	.33	6.00	3.64	3.65	2
2.09	1.37	.30	6.00	3.64	3.64	2
1.86	1.22	.27	6.00	3.63	3.63	2
1.62	1.06	.23	6.00	3.62	3.62	2
1.39	.91	.20	6.00	3.61	3.61	2
1.16	.76	.17	6.00	3.60	3.60	2
.93	.61	.13	6.00	3.59	3.59	2
.70	.45	.10	6.00	3.58	3.58	2
.46	.30	.07	6.00	3.57	3.57	2
.23	.15	.03	6.00	3.56	3.56	2
.00	.00	.00	6.00	3.55	3.55	2

M12FIN.PSO

***** Stresses *****

***** Pore Pressures *****

XI Material	Total	Effective	Total	Static	Excess	
7.72	.00	.00	.00	.00	.00	2
7.61	8.23	8.23	.00	.00	.00	2
7.49	16.45	16.45	.00	.00	.00	2
7.37	24.68	24.68	.00	.00	.00	2
7.26	33.50	33.50	.00	.00	.00	2
7.10	46.60	37.03	9.57	9.57	.00	2
6.94	60.51	40.56	19.95	19.95	.00	2
6.78	74.41	44.09	30.32	30.32	.00	2
6.61	88.28	47.62	40.66	40.66	.00	2
6.45	102.13	51.15	50.99	50.99	.00	2
6.28	115.97	54.67	61.29	61.29	.00	2
6.12	129.78	58.20	71.58	71.58	.00	2
5.96	143.58	61.73	81.84	81.84	.00	2
5.80	157.35	65.26	92.09	92.09	.00	2
5.63	171.10	68.79	102.31	102.31	.00	2
5.47	184.84	72.32	112.52	112.52	.00	2
5.31	198.55	75.85	122.71	122.71	.00	2
5.15	212.25	79.38	132.87	132.87	.00	2
4.99	225.92	82.90	143.02	143.02	.00	2
4.83	239.58	86.43	153.14	153.14	.00	2
4.67	253.21	89.96	163.25	163.25	.00	2
4.51	266.82	93.49	173.33	173.33	.00	2
4.35	280.42	97.02	183.40	183.40	.00	2
4.19	293.99	100.55	193.45	193.45	.00	2
4.03	307.55	104.08	203.47	203.47	.00	2
3.87	321.08	107.60	213.48	213.48	.00	2
3.71	334.60	111.13	223.47	223.47	.00	2
3.55	348.09	114.66	233.43	233.43	.00	2
3.39	361.57	118.19	243.38	243.38	.00	2
3.24	375.02	121.72	253.30	253.30	.00	2
3.08	388.46	125.25	263.21	263.21	.00	2
2.92	401.88	128.78	273.10	273.10	.00	2
2.77	415.27	132.31	282.96	282.96	.00	2
2.61	428.65	135.83	292.81	292.81	.00	2
2.45	442.00	139.36	302.64	302.64	.00	2
2.30	455.34	142.89	312.45	312.45	.00	2
2.14	468.65	146.42	322.23	322.23	.00	2
1.99	481.95	149.95	332.00	332.00	.00	2
1.83	495.23	153.48	341.75	341.75	.00	2
1.68	508.48	157.01	351.48	351.48	.00	2
1.52	521.72	160.54	361.19	361.19	.00	2
1.37	534.94	164.06	370.87	370.87	.00	2
1.22	548.13	167.59	380.54	380.54	.00	2
1.06	561.31	171.12	390.19	390.19	.00	2
.91	574.47	174.65	399.82	399.82	.00	2
.76	587.61	178.18	409.43	409.43	.00	2

M12FIN.PSO						
.61	600.72	181.71	419.01	419.01	.00	2
.45	613.82	185.24	428.58	428.58	.00	2
.30	626.90	188.77	438.13	438.13	.00	2
.15	639.96	192.29	447.66	447.66	.00	2
.00	653.00	195.82	457.18	457.18	.00	2

Time = 730. Degree of Consolidation = 92.%

Total Settlement = 3.876

Settlement at End of Primary Consolidation = 3.846

Settlement caused by Primary Consolidation at time 730. = 3.522

Settlement caused by Secondary Compression at time 730. = .000

Settlement Due to Desiccation = .354

Surface Elevation = 3.79

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
15.57	14.59	6.36	3.00	1.39	1.39	1
10.85	10.79	4.77	1.41	1.37	1.27	1
7.12	7.09	3.18	1.29	1.29	1.23	1
3.53	3.50	1.59	1.23	1.23	1.20	1
.00	.00	.00	1.21	1.17	1.17	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	
Material						
14.59	666.24	199.75	466.50	446.21	20.29	1
10.79	1075.89	234.59	841.29	685.62	155.68	1
7.09	1479.29	341.31	1137.99	918.79	219.20	1
3.50	1875.87	526.57	1349.29	1145.13	204.17	1
.00	2266.63	883.34	1383.30	1365.65	17.64	1

Time = 1095. Degree of Consolidation = 74.%

Total Settlement = .971

M12FIN.PSO

Settlement at End of Primary Consolidation = 1.311

Settlement caused by Primary Consolidation at time 1095. = .971

Settlement caused by Secondary Compression at time 1095. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
11.60	7.70	1.66	6.00	2.50	2.50	2
11.37	7.58	1.62	6.00	2.50	2.50	2
11.14	7.46	1.59	6.00	2.50	2.50	2
10.90	7.34	1.56	6.00	2.50	2.50	2
10.67	7.23	1.52	6.00	2.50	2.50	2
10.44	7.08	1.49	6.00	3.96	3.96	2
10.21	6.92	1.46	6.00	3.95	3.95	2
9.98	6.75	1.43	6.00	3.94	3.94	2
9.74	6.59	1.39	6.00	3.93	3.93	2
9.51	6.43	1.36	6.00	3.93	3.93	2
9.28	6.26	1.33	6.00	3.92	3.92	2
9.05	6.10	1.29	6.00	3.91	3.91	2
8.82	5.94	1.26	6.00	3.90	3.90	2
8.58	5.78	1.23	6.00	3.89	3.89	2
8.35	5.62	1.19	6.00	3.88	3.88	2
8.12	5.45	1.16	6.00	3.87	3.87	2
7.89	5.29	1.13	6.00	3.86	3.86	2
7.66	5.13	1.09	6.00	3.85	3.85	2
7.42	4.97	1.06	6.00	3.84	3.84	2
7.19	4.81	1.03	6.00	3.83	3.83	2
6.96	4.65	.99	6.00	3.82	3.82	2
6.73	4.49	.96	6.00	3.81	3.81	2
6.50	4.33	.93	6.00	3.80	3.80	2
6.26	4.17	.89	6.00	3.79	3.79	2
6.03	4.01	.86	6.00	3.78	3.78	2
5.80	3.86	.83	6.00	3.77	3.77	2
5.57	3.70	.80	6.00	3.76	3.76	2
5.34	3.54	.76	6.00	3.75	3.75	2
5.10	3.38	.73	6.00	3.74	3.74	2
4.87	3.23	.70	6.00	3.73	3.73	2
4.64	3.07	.66	6.00	3.72	3.72	2
4.41	2.91	.63	6.00	3.72	3.72	2
4.18	2.76	.60	6.00	3.71	3.71	2

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3.94	2.60	.56	6.00	3.70	3.70	2
3.71	2.45	.53	6.00	3.69	3.69	2
3.48	2.29	.50	6.00	3.68	3.68	2
3.25	2.14	.46	6.00	3.67	3.67	2
3.02	1.98	.43	6.00	3.66	3.66	2
2.78	1.83	.40	6.00	3.65	3.65	2
2.55	1.67	.36	6.00	3.64	3.64	2
2.32	1.52	.33	6.00	3.63	3.63	2
2.09	1.37	.30	6.00	3.62	3.62	2
1.86	1.21	.27	6.00	3.61	3.61	2
1.62	1.06	.23	6.00	3.60	3.60	2
1.39	.91	.20	6.00	3.59	3.59	2
1.16	.76	.17	6.00	3.58	3.58	2
.93	.60	.13	6.00	3.57	3.57	2
.70	.45	.10	6.00	3.56	3.56	2
.46	.30	.07	6.00	3.56	3.55	2
.23	.15	.03	6.00	3.55	3.54	2
.00	.00	.00	6.00	3.54	3.53	2

***** Stresses *****

***** Pore Pressures *****

XI Material	Total	Effective	Total	Static	Excess	
7.70	.00	.00	.00	.00	.00	2
7.58	8.23	8.23	.00	.00	.00	2
7.46	16.45	16.45	.00	.00	.00	2
7.34	24.68	24.68	.00	.00	.00	2
7.23	32.91	32.91	.00	.00	.00	2
7.08	43.60	43.60	.00	.00	.00	2
6.92	57.48	47.12	10.35	10.35	.00	2
6.75	71.34	50.65	20.69	20.69	.00	2
6.59	85.18	54.18	31.00	31.00	.00	2
6.43	99.00	57.71	41.29	41.29	.00	2
6.26	112.81	61.24	51.57	51.57	.00	2
6.10	126.59	64.77	61.82	61.82	.00	2
5.94	140.35	68.30	72.06	72.06	.00	2
5.78	154.09	71.83	82.27	82.27	.00	2
5.62	167.82	75.35	92.46	92.46	.00	2
5.45	181.52	78.88	102.64	102.64	.00	2
5.29	195.20	82.41	112.79	112.79	.00	2
5.13	208.87	85.94	122.93	122.93	.00	2
4.97	222.51	89.47	133.04	133.04	.00	2
4.81	236.13	93.00	143.13	143.13	.00	2
4.65	249.74	96.53	153.21	153.21	.00	2
4.49	263.32	100.06	163.26	163.26	.00	2
4.33	276.88	103.58	173.30	173.30	.00	2
4.17	290.43	107.11	183.31	183.31	.00	2
4.01	303.95	110.64	193.31	193.31	.00	2
3.86	317.45	114.17	203.28	203.28	.00	2
3.70	330.94	117.70	213.24	213.24	.00	2

M12FIN.PSO						
3.54	344.40	121.23	223.17	223.17	.00	2
3.38	357.84	124.76	233.09	233.09	.00	2
3.23	371.27	128.29	242.98	242.98	.00	2
3.07	384.67	131.81	252.86	252.86	.00	2
2.91	398.06	135.34	262.71	262.71	.00	2
2.76	411.42	138.87	272.55	272.55	.00	2
2.60	424.77	142.40	282.37	282.37	.00	2
2.45	438.09	145.93	292.16	292.16	.00	2
2.29	451.39	149.46	301.94	301.94	.00	2
2.14	464.68	152.99	311.69	311.69	.00	2
1.98	477.94	156.52	321.43	321.43	.00	2
1.83	491.19	160.04	331.15	331.15	.00	2
1.67	504.41	163.57	340.84	340.84	.00	2
1.52	517.62	167.10	350.52	350.52	.00	2
1.37	530.80	170.63	360.17	360.17	.00	2
1.21	543.97	174.16	369.81	369.81	.00	2
1.06	557.11	177.69	379.43	379.43	.00	2
.91	570.24	181.22	389.02	389.02	.00	2
.76	583.34	184.74	398.60	398.60	.00	2
.60	596.43	188.10	408.33	408.16	.17	2
.45	609.50	191.27	418.23	417.70	.53	2
.30	622.55	194.26	428.29	427.22	1.07	2
.15	635.58	197.08	438.50	436.72	1.78	2
.00	648.60	199.75	448.86	446.21	2.64	2

Time = 1095. Degree of Consolidation = 91.%

Total Settlement = 3.905

Settlement at End of Primary Consolidation = 3.905

Settlement caused by Primary Consolidation at time 1095. = 3.541

Settlement caused by Secondary Compression at time 1095. = .000

Settlement Due to Desiccation = .364

Surface Elevation = 3.72

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
15.57	14.56	6.36	3.00	1.39	1.39	1

M12FIN.PSO						
10.85	10.78	4.77	1.41	1.36	1.27	1
7.12	7.09	3.18	1.29	1.29	1.23	1
3.53	3.50	1.59	1.23	1.23	1.20	1
.00	.00	.00	1.21	1.17	1.17	1

Time = 1460. Degree of Consolidation = 76.%

Total Settlement = 1.003

Settlement at End of Primary Consolidation = 1.311

Settlement caused by Primary Consolidation at time 1460. = 1.003

Settlement caused by Secondary Compression at time 1460. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
11.60	7.69	1.66	6.00	2.50	2.50	2
11.37	7.58	1.62	6.00	2.50	2.50	2
11.14	7.46	1.59	6.00	2.50	2.50	2
10.90	7.34	1.56	6.00	2.50	2.50	2
10.67	7.23	1.52	6.00	2.50	2.50	2
10.44	7.08	1.49	6.00	3.96	3.96	2
10.21	6.92	1.46	6.00	3.95	3.95	2
9.98	6.75	1.43	6.00	3.94	3.94	2
9.74	6.59	1.39	6.00	3.93	3.93	2
9.51	6.43	1.36	6.00	3.93	3.93	2
9.28	6.26	1.33	6.00	3.92	3.92	2
9.05	6.10	1.29	6.00	3.91	3.91	2
8.82	5.94	1.26	6.00	3.90	3.90	2
8.58	5.78	1.23	6.00	3.89	3.89	2
8.35	5.61	1.19	6.00	3.88	3.88	2
8.12	5.45	1.16	6.00	3.87	3.87	2
7.89	5.29	1.13	6.00	3.86	3.86	2
7.66	5.13	1.09	6.00	3.85	3.85	2
7.42	4.97	1.06	6.00	3.84	3.84	2
7.19	4.81	1.03	6.00	3.83	3.83	2
6.96	4.65	.99	6.00	3.82	3.82	2
6.73	4.49	.96	6.00	3.81	3.81	2
6.50	4.33	.93	6.00	3.80	3.80	2
6.26	4.17	.89	6.00	3.79	3.79	2
6.03	4.01	.86	6.00	3.78	3.78	2

M12FIN.PSO						
5.80	3.86	.83	6.00	3.77	3.77	2
5.57	3.70	.80	6.00	3.76	3.76	2
5.34	3.54	.76	6.00	3.75	3.75	2
5.10	3.38	.73	6.00	3.74	3.74	2
4.87	3.23	.70	6.00	3.73	3.73	2
4.64	3.07	.66	6.00	3.72	3.72	2
4.41	2.91	.63	6.00	3.72	3.72	2
4.18	2.76	.60	6.00	3.71	3.71	2
3.94	2.60	.56	6.00	3.70	3.70	2
3.71	2.44	.53	6.00	3.69	3.69	2
3.48	2.29	.50	6.00	3.68	3.68	2
3.25	2.13	.46	6.00	3.67	3.67	2
3.02	1.98	.43	6.00	3.66	3.66	2
2.78	1.83	.40	6.00	3.65	3.65	2
2.55	1.67	.36	6.00	3.64	3.64	2
2.32	1.52	.33	6.00	3.63	3.63	2
2.09	1.37	.30	6.00	3.62	3.62	2
1.86	1.21	.27	6.00	3.61	3.61	2
1.62	1.06	.23	6.00	3.60	3.60	2
1.39	.91	.20	6.00	3.59	3.59	2
1.16	.76	.17	6.00	3.58	3.58	2
.93	.60	.13	6.00	3.57	3.57	2
.70	.45	.10	6.00	3.56	3.56	2
.46	.30	.07	6.00	3.55	3.55	2
.23	.15	.03	6.00	3.54	3.54	2
.00	.00	.00	6.00	3.54	3.53	2

Time = 1460. Degree of Consolidation = 91.0%

Total Settlement = 3.905

Settlement at End of Primary Consolidation = 3.905

Settlement caused by Primary Consolidation at time 1460. = 3.541

Settlement caused by Secondary Compression at time 1460. = .000

Settlement Due to Desiccation = .364

Surface Elevation = 3.69

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop
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M12FIN.PSO

Material						
15.57	14.54	6.36	3.00	1.39	1.39	1
10.85	10.77	4.77	1.41	1.35	1.27	1
7.12	7.09	3.18	1.29	1.29	1.23	1
3.53	3.50	1.59	1.23	1.23	1.20	1
.00	.00	.00	1.21	1.17	1.17	1

Time = 1825. Degree of Consolidation = 78.0%

Total Settlement = 1.027

Settlement at End of Primary Consolidation = 1.311

Settlement caused by Primary Consolidation at time 1825. = 1.027

Settlement caused by Secondary Compression at time 1825. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
Material	A	XI	Z	Einitial	E	Eeop
11.60	7.69	1.66	6.00	2.50	2.50	2
11.37	7.58	1.62	6.00	2.50	2.50	2
11.14	7.46	1.59	6.00	2.50	2.50	2
10.90	7.34	1.56	6.00	2.50	2.50	2
10.67	7.23	1.52	6.00	2.50	2.50	2
10.44	7.08	1.49	6.00	3.96	3.96	2
10.21	6.92	1.46	6.00	3.95	3.95	2
9.98	6.75	1.43	6.00	3.94	3.94	2
9.74	6.59	1.39	6.00	3.93	3.93	2
9.51	6.43	1.36	6.00	3.93	3.93	2
9.28	6.26	1.33	6.00	3.92	3.92	2
9.05	6.10	1.29	6.00	3.91	3.91	2
8.82	5.94	1.26	6.00	3.90	3.90	2
8.58	5.78	1.23	6.00	3.89	3.89	2
8.35	5.61	1.19	6.00	3.88	3.88	2
8.12	5.45	1.16	6.00	3.87	3.87	2
7.89	5.29	1.13	6.00	3.86	3.86	2
7.66	5.13	1.09	6.00	3.85	3.85	2
7.42	4.97	1.06	6.00	3.84	3.84	2
7.19	4.81	1.03	6.00	3.83	3.83	2
6.96	4.65	.99	6.00	3.82	3.82	2
6.73	4.49	.96	6.00	3.81	3.81	2
6.50	4.33	.93	6.00	3.80	3.80	2

M12FIN.PSO						
6.26	4.17	.89	6.00	3.79	3.79	2
6.03	4.01	.86	6.00	3.78	3.78	2
5.80	3.86	.83	6.00	3.77	3.77	2
5.57	3.70	.80	6.00	3.76	3.76	2
5.34	3.54	.76	6.00	3.75	3.75	2
5.10	3.38	.73	6.00	3.74	3.74	2
4.87	3.23	.70	6.00	3.73	3.73	2
4.64	3.07	.66	6.00	3.72	3.72	2
4.41	2.91	.63	6.00	3.72	3.72	2
4.18	2.76	.60	6.00	3.71	3.71	2
3.94	2.60	.56	6.00	3.70	3.70	2
3.71	2.44	.53	6.00	3.69	3.69	2
3.48	2.29	.50	6.00	3.68	3.68	2
3.25	2.13	.46	6.00	3.67	3.67	2
3.02	1.98	.43	6.00	3.66	3.66	2
2.78	1.83	.40	6.00	3.65	3.65	2
2.55	1.67	.36	6.00	3.64	3.64	2
2.32	1.52	.33	6.00	3.63	3.63	2
2.09	1.37	.30	6.00	3.62	3.62	2
1.86	1.21	.27	6.00	3.61	3.61	2
1.62	1.06	.23	6.00	3.60	3.60	2
1.39	.91	.20	6.00	3.59	3.59	2
1.16	.76	.17	6.00	3.58	3.58	2
.93	.60	.13	6.00	3.57	3.57	2
.70	.45	.10	6.00	3.56	3.56	2
.46	.30	.07	6.00	3.55	3.55	2
.23	.15	.03	6.00	3.54	3.54	2
.00	.00	.00	6.00	3.54	3.53	2

Time = 1825. Degree of Consolidation = 91.0%

Total Settlement = 3.905

Settlement at End of Primary Consolidation = 3.905

Settlement caused by Primary Consolidation at time 1825. = 3.541

Settlement caused by Secondary Compression at time 1825. = .000

Settlement Due to Desiccation = .364

Surface Elevation = 3.67

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****

***** Void Ratios *****

M12FIN.PSO

A	XI	Z	Einitial	E	Eeop	
Material						
15.57	14.52	6.36	3.00	1.39	1.39	1
10.85	10.76	4.77	1.41	1.34	1.27	1
7.12	7.08	3.18	1.29	1.28	1.23	1
3.53	3.50	1.59	1.23	1.23	1.20	1
.00	.00	.00	1.21	1.17	1.17	1

Time = 2190. Degree of Consolidation = 80.0%

Total Settlement = 1.047

Settlement at End of Primary Consolidation = 1.311

Settlement caused by Primary Consolidation at time 2190. = 1.047

Settlement caused by Secondary Compression at time 2190. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	
Material						
11.60	7.69	1.66	6.00	2.50	2.50	2
11.37	7.58	1.62	6.00	2.50	2.50	2
11.14	7.46	1.59	6.00	2.50	2.50	2
10.90	7.34	1.56	6.00	2.50	2.50	2
10.67	7.23	1.52	6.00	2.50	2.50	2
10.44	7.08	1.49	6.00	3.96	3.96	2
10.21	6.92	1.46	6.00	3.95	3.95	2
9.98	6.75	1.43	6.00	3.94	3.94	2
9.74	6.59	1.39	6.00	3.93	3.93	2
9.51	6.43	1.36	6.00	3.93	3.93	2
9.28	6.26	1.33	6.00	3.92	3.92	2
9.05	6.10	1.29	6.00	3.91	3.91	2
8.82	5.94	1.26	6.00	3.90	3.90	2
8.58	5.78	1.23	6.00	3.89	3.89	2
8.35	5.61	1.19	6.00	3.88	3.88	2
8.12	5.45	1.16	6.00	3.87	3.87	2
7.89	5.29	1.13	6.00	3.86	3.86	2
7.66	5.13	1.09	6.00	3.85	3.85	2
7.42	4.97	1.06	6.00	3.84	3.84	2
7.19	4.81	1.03	6.00	3.83	3.83	2
6.96	4.65	.99	6.00	3.82	3.82	2

M12FIN.PSO

6.73	4.49	.96	6.00	3.81	3.81	2
6.50	4.33	.93	6.00	3.80	3.80	2
6.26	4.17	.89	6.00	3.79	3.79	2
6.03	4.01	.86	6.00	3.78	3.78	2
5.80	3.86	.83	6.00	3.77	3.77	2
5.57	3.70	.80	6.00	3.76	3.76	2
5.34	3.54	.76	6.00	3.75	3.75	2
5.10	3.38	.73	6.00	3.74	3.74	2
4.87	3.23	.70	6.00	3.73	3.73	2
4.64	3.07	.66	6.00	3.72	3.72	2
4.41	2.91	.63	6.00	3.72	3.72	2
4.18	2.76	.60	6.00	3.71	3.71	2
3.94	2.60	.56	6.00	3.70	3.70	2
3.71	2.44	.53	6.00	3.69	3.69	2
3.48	2.29	.50	6.00	3.68	3.68	2
3.25	2.13	.46	6.00	3.67	3.67	2
3.02	1.98	.43	6.00	3.66	3.66	2
2.78	1.83	.40	6.00	3.65	3.65	2
2.55	1.67	.36	6.00	3.64	3.64	2
2.32	1.52	.33	6.00	3.63	3.63	2
2.09	1.37	.30	6.00	3.62	3.62	2
1.86	1.21	.27	6.00	3.61	3.61	2
1.62	1.06	.23	6.00	3.60	3.60	2
1.39	.91	.20	6.00	3.59	3.59	2
1.16	.76	.17	6.00	3.58	3.58	2
.93	.60	.13	6.00	3.57	3.57	2
.70	.45	.10	6.00	3.56	3.56	2
.46	.30	.07	6.00	3.55	3.55	2
.23	.15	.03	6.00	3.54	3.54	2
.00	.00	.00	6.00	3.54	3.53	2

Time = 2190. Degree of Consolidation = 91.0%

Total Settlement = 3.905

Settlement at End of Primary Consolidation = 3.905

Settlement caused by Primary Consolidation at time 2190. = 3.541

Settlement caused by Secondary Compression at time 2190. = .000

Settlement Due to Desiccation = .364

Surface Elevation = 3.65

*****Current Conditions in Compressible Foundation*****

M12FIN.PSO

***** Coordinates *****

***** Void Ratios *****

Material	A	XI	Z	Einitial	E	Eeop	
	15.57	14.50	6.36	3.00	1.39	1.39	1
	10.85	10.75	4.77	1.41	1.34	1.27	1
	7.12	7.08	3.18	1.29	1.28	1.23	1
	3.53	3.50	1.59	1.23	1.23	1.20	1
	.00	.00	.00	1.21	1.17	1.17	1

Time = 2555. Degree of Consolidation = 81.0%

Total Settlement = 1.064

Settlement at End of Primary Consolidation = 1.311

Settlement caused by Primary Consolidation at time 2555. = 1.064

Settlement caused by Secondary Compression at time 2555. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

Material	A	XI	Z	Einitial	E	Eeop	
	11.60	7.69	1.66	6.00	2.50	2.50	2
	11.37	7.58	1.62	6.00	2.50	2.50	2
	11.14	7.46	1.59	6.00	2.50	2.50	2
	10.90	7.34	1.56	6.00	2.50	2.50	2
	10.67	7.23	1.52	6.00	2.50	2.50	2
	10.44	7.08	1.49	6.00	3.96	3.96	2
	10.21	6.92	1.46	6.00	3.95	3.95	2
	9.98	6.75	1.43	6.00	3.94	3.94	2
	9.74	6.59	1.39	6.00	3.93	3.93	2
	9.51	6.43	1.36	6.00	3.93	3.93	2
	9.28	6.26	1.33	6.00	3.92	3.92	2
	9.05	6.10	1.29	6.00	3.91	3.91	2
	8.82	5.94	1.26	6.00	3.90	3.90	2
	8.58	5.78	1.23	6.00	3.89	3.89	2
	8.35	5.61	1.19	6.00	3.88	3.88	2
	8.12	5.45	1.16	6.00	3.87	3.87	2
	7.89	5.29	1.13	6.00	3.86	3.86	2
	7.66	5.13	1.09	6.00	3.85	3.85	2
	7.42	4.97	1.06	6.00	3.84	3.84	2

M12FIN.PSO						
7.19	4.81	1.03	6.00	3.83	3.83	2
6.96	4.65	.99	6.00	3.82	3.82	2
6.73	4.49	.96	6.00	3.81	3.81	2
6.50	4.33	.93	6.00	3.80	3.80	2
6.26	4.17	.89	6.00	3.79	3.79	2
6.03	4.01	.86	6.00	3.78	3.78	2
5.80	3.86	.83	6.00	3.77	3.77	2
5.57	3.70	.80	6.00	3.76	3.76	2
5.34	3.54	.76	6.00	3.75	3.75	2
5.10	3.38	.73	6.00	3.74	3.74	2
4.87	3.23	.70	6.00	3.73	3.73	2
4.64	3.07	.66	6.00	3.72	3.72	2
4.41	2.91	.63	6.00	3.72	3.72	2
4.18	2.76	.60	6.00	3.71	3.71	2
3.94	2.60	.56	6.00	3.70	3.70	2
3.71	2.44	.53	6.00	3.69	3.69	2
3.48	2.29	.50	6.00	3.68	3.68	2
3.25	2.13	.46	6.00	3.67	3.67	2
3.02	1.98	.43	6.00	3.66	3.66	2
2.78	1.83	.40	6.00	3.65	3.65	2
2.55	1.67	.36	6.00	3.64	3.64	2
2.32	1.52	.33	6.00	3.63	3.63	2
2.09	1.37	.30	6.00	3.62	3.62	2
1.86	1.21	.27	6.00	3.61	3.61	2
1.62	1.06	.23	6.00	3.60	3.60	2
1.39	.91	.20	6.00	3.59	3.59	2
1.16	.76	.17	6.00	3.58	3.58	2
.93	.60	.13	6.00	3.57	3.57	2
.70	.45	.10	6.00	3.56	3.56	2
.46	.30	.07	6.00	3.55	3.55	2
.23	.15	.03	6.00	3.54	3.54	2
.00	.00	.00	6.00	3.54	3.53	2

Time = 2555. Degree of Consolidation = 91.0%

Total Settlement = 3.905

Settlement at End of Primary Consolidation = 3.905

Settlement caused by Primary Consolidation at time 2555. = 3.541

Settlement caused by Secondary Compression at time 2555. = .000

Settlement Due to Desiccation = .364

Surface Elevation = 3.63

M12FIN.PSO

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
15.57	14.49	6.36	3.00	1.39	1.39	1
10.85	10.74	4.77	1.41	1.33	1.27	1
7.12	7.07	3.18	1.29	1.28	1.23	1
3.53	3.50	1.59	1.23	1.22	1.20	1
.00	.00	.00	1.21	1.17	1.17	1
Time = 2920. Degree of Consolidation = 82.%						
Total Settlement = 1.078						
Settlement at End of Primary Consolidation = 1.311						
Settlement caused by Primary Consolidation at time 2920. = 1.078						
Settlement caused by Secondary Compression at time 2920. = .000						

*****Current Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
11.60	7.69	1.66	6.00	2.50	2.50	2
11.37	7.58	1.62	6.00	2.50	2.50	2
11.14	7.46	1.59	6.00	2.50	2.50	2
10.90	7.34	1.56	6.00	2.50	2.50	2
10.67	7.23	1.52	6.00	2.50	2.50	2
10.44	7.08	1.49	6.00	3.96	3.96	2
10.21	6.92	1.46	6.00	3.95	3.95	2
9.98	6.75	1.43	6.00	3.94	3.94	2
9.74	6.59	1.39	6.00	3.93	3.93	2
9.51	6.43	1.36	6.00	3.93	3.93	2
9.28	6.26	1.33	6.00	3.92	3.92	2
9.05	6.10	1.29	6.00	3.91	3.91	2
8.82	5.94	1.26	6.00	3.90	3.90	2
8.58	5.78	1.23	6.00	3.89	3.89	2
8.35	5.61	1.19	6.00	3.88	3.88	2
8.12	5.45	1.16	6.00	3.87	3.87	2
7.89	5.29	1.13	6.00	3.86	3.86	2

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7.66	5.13	1.09	6.00	3.85	3.85	2
7.42	4.97	1.06	6.00	3.84	3.84	2
7.19	4.81	1.03	6.00	3.83	3.83	2
6.96	4.65	.99	6.00	3.82	3.82	2
6.73	4.49	.96	6.00	3.81	3.81	2
6.50	4.33	.93	6.00	3.80	3.80	2
6.26	4.17	.89	6.00	3.79	3.79	2
6.03	4.01	.86	6.00	3.78	3.78	2
5.80	3.86	.83	6.00	3.77	3.77	2
5.57	3.70	.80	6.00	3.76	3.76	2
5.34	3.54	.76	6.00	3.75	3.75	2
5.10	3.38	.73	6.00	3.74	3.74	2
4.87	3.23	.70	6.00	3.73	3.73	2
4.64	3.07	.66	6.00	3.72	3.72	2
4.41	2.91	.63	6.00	3.72	3.72	2
4.18	2.76	.60	6.00	3.71	3.71	2
3.94	2.60	.56	6.00	3.70	3.70	2
3.71	2.44	.53	6.00	3.69	3.69	2
3.48	2.29	.50	6.00	3.68	3.68	2
3.25	2.13	.46	6.00	3.67	3.67	2
3.02	1.98	.43	6.00	3.66	3.66	2
2.78	1.83	.40	6.00	3.65	3.65	2
2.55	1.67	.36	6.00	3.64	3.64	2
2.32	1.52	.33	6.00	3.63	3.63	2
2.09	1.37	.30	6.00	3.62	3.62	2
1.86	1.21	.27	6.00	3.61	3.61	2
1.62	1.06	.23	6.00	3.60	3.60	2
1.39	.91	.20	6.00	3.59	3.59	2
1.16	.76	.17	6.00	3.58	3.58	2
.93	.60	.13	6.00	3.57	3.57	2
.70	.45	.10	6.00	3.56	3.56	2
.46	.30	.07	6.00	3.55	3.55	2
.23	.15	.03	6.00	3.54	3.54	2
.00	.00	.00	6.00	3.53	3.53	2

Time = 2920. Degree of Consolidation = 91.0%

Total Settlement = 3.905

Settlement at End of Primary Consolidation = 3.905

Settlement caused by Primary Consolidation at time 2920. = 3.541

Settlement caused by Secondary Compression at time 2920. = .000

Settlement Due to Desiccation = .364

Surface Elevation = 3.62

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
15.57	14.47	6.36	3.00	1.39	1.39	1
10.85	10.72	4.77	1.41	1.33	1.27	1
7.12	7.07	3.18	1.29	1.27	1.23	1
3.53	3.49	1.59	1.23	1.22	1.20	1
.00	.00	.00	1.21	1.17	1.17	1
Time = 3650. Degree of Consolidation = 84.%						
Total Settlement = 1.100						
Settlement at End of Primary Consolidation = 1.311						
Settlement caused by Primary Consolidation at time 3650. = 1.100						
Settlement caused by Secondary Compression at time 3650. = .000						

*****Current Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
11.60	7.69	1.66	6.00	2.50	2.50	2
11.37	7.58	1.62	6.00	2.50	2.50	2
11.14	7.46	1.59	6.00	2.50	2.50	2
10.90	7.34	1.56	6.00	2.50	2.50	2
10.67	7.23	1.52	6.00	2.50	2.50	2
10.44	7.08	1.49	6.00	3.96	3.96	2
10.21	6.92	1.46	6.00	3.95	3.95	2
9.98	6.75	1.43	6.00	3.94	3.94	2
9.74	6.59	1.39	6.00	3.93	3.93	2
9.51	6.43	1.36	6.00	3.93	3.93	2
9.28	6.26	1.33	6.00	3.92	3.92	2
9.05	6.10	1.29	6.00	3.91	3.91	2
8.82	5.94	1.26	6.00	3.90	3.90	2
8.58	5.78	1.23	6.00	3.89	3.89	2
8.35	5.61	1.19	6.00	3.88	3.88	2

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8.12	5.45	1.16	6.00	3.87	3.87	2
7.89	5.29	1.13	6.00	3.86	3.86	2
7.66	5.13	1.09	6.00	3.85	3.85	2
7.42	4.97	1.06	6.00	3.84	3.84	2
7.19	4.81	1.03	6.00	3.83	3.83	2
6.96	4.65	.99	6.00	3.82	3.82	2
6.73	4.49	.96	6.00	3.81	3.81	2
6.50	4.33	.93	6.00	3.80	3.80	2
6.26	4.17	.89	6.00	3.79	3.79	2
6.03	4.01	.86	6.00	3.78	3.78	2
5.80	3.86	.83	6.00	3.77	3.77	2
5.57	3.70	.80	6.00	3.76	3.76	2
5.34	3.54	.76	6.00	3.75	3.75	2
5.10	3.38	.73	6.00	3.74	3.74	2
4.87	3.23	.70	6.00	3.73	3.73	2
4.64	3.07	.66	6.00	3.72	3.72	2
4.41	2.91	.63	6.00	3.72	3.72	2
4.18	2.76	.60	6.00	3.71	3.71	2
3.94	2.60	.56	6.00	3.70	3.70	2
3.71	2.44	.53	6.00	3.69	3.69	2
3.48	2.29	.50	6.00	3.68	3.68	2
3.25	2.13	.46	6.00	3.67	3.67	2
3.02	1.98	.43	6.00	3.66	3.66	2
2.78	1.83	.40	6.00	3.65	3.65	2
2.55	1.67	.36	6.00	3.64	3.64	2
2.32	1.52	.33	6.00	3.63	3.63	2
2.09	1.37	.30	6.00	3.62	3.62	2
1.86	1.21	.27	6.00	3.61	3.61	2
1.62	1.06	.23	6.00	3.60	3.60	2
1.39	.91	.20	6.00	3.59	3.59	2
1.16	.76	.17	6.00	3.58	3.58	2
.93	.60	.13	6.00	3.57	3.57	2
.70	.45	.10	6.00	3.56	3.56	2
.46	.30	.07	6.00	3.55	3.55	2
.23	.15	.03	6.00	3.54	3.54	2
.00	.00	.00	6.00	3.53	3.53	2

Time = 3650. Degree of Consolidation = 91.%

Total Settlement = 3.905

Settlement at End of Primary Consolidation = 3.905

Settlement caused by Primary Consolidation at time 3650. = 3.541

Settlement caused by Secondary Compression at time 3650. = .000

Settlement Due to Desiccation = .364

Surface Elevation = 3.59

Consolidation and desiccation of soft layers---dredged fill

Problem	M12 Settlement FG Marsh	1,630,000 Cut Cubic Yards
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*****Soil data for compressible foundation*****
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Material Type	Layer Thickness	Numbers of Sub-layers	Ca/Cc	Cr/Cc
1	15.00	4	.040	.150

Material type : 1 Specific Gravity of Solids: 2.70

	Void	Effective	Perm-	k/1+e			
I	Ratio	Stress	easeability	PK	Beta	Dsde	Alpha
1	3.000	.000E+00	.350E-02	.875E-03	.105E-02	-.400E-01	-.350E-04
2	2.750	.100E-01	.230E-02	.613E-03	.893E-03	-.160E+00	-.981E-04
3	2.500	.800E-01	.150E-02	.429E-03	.673E-03	-.580E+00	-.249E-03
4	2.250	.300E+00	.900E-03	.277E-03	.524E-03	-.344E+01	-.953E-03
5	2.000	.180E+01	.500E-03	.167E-03	.336E-03	-.154E+02	-.257E-02
6	1.750	.800E+01	.300E-03	.109E-03	.213E-03	-.964E+02	-.105E-01
7	1.500	.500E+02	.150E-03	.600E-04	.156E-03	-.784E+03	-.470E-01
8	1.250	.400E+03	.700E-04	.311E-04	.900E-04	-.390E+04	-.121E+00
9	1.000	.200E+04	.300E-04	.150E-04	.644E-04	-.640E+04	-.960E-01

*****Soil data for dredged fill*****

Material Type	Specific Gravity	Ca/Cc	Cr/Cc	Saturation Limit	Disication Limit
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2 2.690 .040 .150 3.400 2.500

Material type : 2

	Void	Effective	Perm-	k/1+e			
I	Ratio	Stress	eability	PK	Beta	Dsde	Alpha
1	10.000	.000E+00	.240E+00	.218E-01	.182E-02	-.150E+00	-.327E-02
2	9.000	.150E+00	.200E+00	.200E-01	.258E-02	-.200E+00	-.400E-02
3	8.000	.400E+00	.150E+00	.167E-01	.437E-02	-.275E+00	-.458E-02
4	7.000	.700E+00	.900E-01	.113E-01	.448E-02	-.550E+00	-.619E-02
5	6.000	.150E+01	.540E-01	.771E-02	.313E-02	-.165E+01	-.127E-01
6	5.000	.400E+01	.300E-01	.500E-02	.367E-02	-.143E+02	-.712E-01
7	4.000	.300E+02	.190E-02	.380E-03	.247E-02	-.198E+03	-.752E-01
8	3.000	.400E+03	.200E-03	.500E-04	.188E-03	-.249E+04	-.124E+00
9	2.000	.500E+04	.100E-04	.333E-05	.467E-04	-.460E+04	-.153E-01

Summary of lifts and print detail

Time	Material	Fill	# Sub-	Void	Start	Dessic.	Print
days	Type	Height	layers	ratio	Day	Month	detai
0.	2	7.6	50	6.00	180.	1	1
120.					180.	1	1
365.					180.	1	1
730.					180.	1	1
1095.					180.	1	1
1460.					180.	1	2
1825.					180.	1	2
2190.					180.	1	2
2555.					180.	1	2
2920.					180.	1	2
3650.					180.	1	2

Summary of monthly rainfall and evaporation potential

Month	Rainfall	Evaporation
1	.250	.340

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2	.200	.330
3	.180	.470
4	.220	.580
5	.280	.670
6	.290	.800
7	.310	.780
8	.370	.800
9	.490	.600
10	.220	.520
11	.270	.350
12	.300	.280

*****Calculation data*****

tau	Lower layer Void ratio	Lower layer Permeability	drainage path Length
.118	.900	.10000E-01	z = 2.77

Summary of desiccation parameters

Parameter	Value
Surface Drainage Efficiency	.70
maximum evaporation efficiency	.50
saturation at desiccation limit	.50
maximum crust thickness	.50
time to desic. after initial fill	180.00
month of initial desiccation	1
elevation of fixed water table	-5.00
elevation of top of incompres. found.	-18.00

*****Initial Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
15.57	15.57	6.36	3.00	3.00	1.45	1
10.85	10.85	4.77	1.41	1.41	1.33	1
7.12	7.12	3.18	1.29	1.29	1.24	1
3.53	3.53	1.59	1.23	1.23	1.21	1
.00	.00	.00	1.21	1.21	1.19	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	
Material						
15.57	594.40	.00	594.40	478.80	115.60	1
10.85	1061.98	170.24	891.74	776.15	115.60	1
7.12	1467.24	340.47	1126.77	1011.17	115.60	1
3.53	1863.66	510.71	1352.95	1237.35	115.60	1
.00	2255.99	680.95	1575.04	1459.45	115.60	1

Time = 0. Degree of Consolidation = 0.0%

Total Settlement = .000

Settlement at End of Primary Consolidation = 1.097

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

*****Initial Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
7.60	7.60	1.09	6.00	6.00	10.00	2

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7.45	7.45	1.06	6.00	6.00	5.68	2
7.30	7.30	1.04	6.00	6.00	4.98	2
7.14	7.14	1.02	6.00	6.00	4.89	2
6.99	6.99	1.00	6.00	6.00	4.80	2
6.84	6.84	.98	6.00	6.00	4.71	2
6.69	6.69	.96	6.00	6.00	4.62	2
6.54	6.54	.93	6.00	6.00	4.53	2
6.38	6.38	.91	6.00	6.00	4.44	2
6.23	6.23	.89	6.00	6.00	4.35	2
6.08	6.08	.87	6.00	6.00	4.26	2
5.93	5.93	.85	6.00	6.00	4.18	2
5.78	5.78	.83	6.00	6.00	4.09	2
5.62	5.62	.80	6.00	6.00	4.00	2
5.47	5.47	.78	6.00	6.00	3.99	2
5.32	5.32	.76	6.00	6.00	3.99	2
5.17	5.17	.74	6.00	6.00	3.98	2
5.02	5.02	.72	6.00	6.00	3.97	2
4.86	4.86	.69	6.00	6.00	3.97	2
4.71	4.71	.67	6.00	6.00	3.96	2
4.56	4.56	.65	6.00	6.00	3.96	2
4.41	4.41	.63	6.00	6.00	3.95	2
4.26	4.26	.61	6.00	6.00	3.94	2
4.10	4.10	.59	6.00	6.00	3.94	2
3.95	3.95	.56	6.00	6.00	3.93	2
3.80	3.80	.54	6.00	6.00	3.92	2
3.65	3.65	.52	6.00	6.00	3.92	2
3.50	3.50	.50	6.00	6.00	3.91	2
3.34	3.34	.48	6.00	6.00	3.91	2
3.19	3.19	.46	6.00	6.00	3.90	2
3.04	3.04	.43	6.00	6.00	3.89	2
2.89	2.89	.41	6.00	6.00	3.89	2
2.74	2.74	.39	6.00	6.00	3.88	2
2.58	2.58	.37	6.00	6.00	3.87	2
2.43	2.43	.35	6.00	6.00	3.87	2
2.28	2.28	.33	6.00	6.00	3.86	2
2.13	2.13	.30	6.00	6.00	3.86	2
1.98	1.98	.28	6.00	6.00	3.85	2
1.82	1.82	.26	6.00	6.00	3.84	2
1.67	1.67	.24	6.00	6.00	3.84	2
1.52	1.52	.22	6.00	6.00	3.83	2
1.37	1.37	.20	6.00	6.00	3.82	2
1.22	1.22	.17	6.00	6.00	3.82	2
1.06	1.06	.15	6.00	6.00	3.81	2
.91	.91	.13	6.00	6.00	3.81	2
.76	.76	.11	6.00	6.00	3.80	2
.61	.61	.09	6.00	6.00	3.79	2
.46	.46	.07	6.00	6.00	3.79	2
.30	.30	.04	6.00	6.00	3.78	2
.15	.15	.02	6.00	6.00	3.77	2
.00	.00	.00	6.00	6.00	3.77	2

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***** Stresses *****		***** Pore Pressures *****				
XI	Total	Effective	Total	Static	Excess	
Material						
7.60	.00	.00	.00	.00	.00	2
7.45	11.89	.00	11.89	9.58	2.31	2
7.30	23.78	.00	23.78	19.15	4.62	2
7.14	35.66	.00	35.66	28.73	6.94	2
6.99	47.55	.00	47.55	38.30	9.25	2
6.84	59.44	.00	59.44	47.88	11.56	2
6.69	71.33	.00	71.33	57.46	13.87	2
6.54	83.22	.00	83.22	67.03	16.18	2
6.38	95.10	.00	95.10	76.61	18.50	2
6.23	106.99	.00	106.99	86.18	20.81	2
6.08	118.88	.00	118.88	95.76	23.12	2
5.93	130.77	.00	130.77	105.34	25.43	2
5.78	142.66	.00	142.66	114.91	27.74	2
5.62	154.54	.00	154.54	124.49	30.06	2
5.47	166.43	.00	166.43	134.06	32.37	2
5.32	178.32	.00	178.32	143.64	34.68	2
5.17	190.21	.00	190.21	153.22	36.99	2
5.02	202.09	.00	202.09	162.79	39.30	2
4.86	213.98	.00	213.98	172.37	41.61	2
4.71	225.87	.00	225.87	181.94	43.93	2
4.56	237.76	.00	237.76	191.52	46.24	2
4.41	249.65	.00	249.65	201.10	48.55	2
4.26	261.53	.00	261.53	210.67	50.86	2
4.10	273.42	.00	273.42	220.25	53.17	2
3.95	285.31	.00	285.31	229.82	55.49	2
3.80	297.20	.00	297.20	239.40	57.80	2
3.65	309.09	.00	309.09	248.98	60.11	2
3.50	320.97	.00	320.97	258.55	62.42	2
3.34	332.86	.00	332.86	268.13	64.73	2
3.19	344.75	.00	344.75	277.70	67.05	2
3.04	356.64	.00	356.64	287.28	69.36	2
2.89	368.53	.00	368.53	296.86	71.67	2
2.74	380.41	.00	380.41	306.43	73.98	2
2.58	392.30	.00	392.30	316.01	76.29	2
2.43	404.19	.00	404.19	325.58	78.61	2
2.28	416.08	.00	416.08	335.16	80.92	2
2.13	427.97	.00	427.97	344.74	83.23	2
1.98	439.85	.00	439.85	354.31	85.54	2
1.82	451.74	.00	451.74	363.89	87.85	2
1.67	463.63	.00	463.63	373.46	90.16	2
1.52	475.52	.00	475.52	383.04	92.48	2
1.37	487.40	.00	487.40	392.62	94.79	2
1.22	499.29	.00	499.29	402.19	97.10	2
1.06	511.18	.00	511.18	411.77	99.41	2
.91	523.07	.00	523.07	421.34	101.72	2
.76	534.96	.00	534.96	430.92	104.04	2

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.61	546.84	.00	546.84	440.50	106.35	2
.46	558.73	.00	558.73	450.07	108.66	2
.30	570.62	.00	570.62	459.65	110.97	2
.15	582.51	.00	582.51	469.22	113.28	2
.00	594.40	.00	594.40	478.80	115.60	2

Time = 0. Degree of Consolidation = 0.0%

Total Settlement = .000

Settlement at End of Primary Consolidation = 2.049

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
15.57	14.84	6.36	3.00	1.66	1.45	1
10.85	10.83	4.77	1.41	1.41	1.33	1
7.12	7.11	3.18	1.29	1.29	1.24	1
3.53	3.51	1.59	1.23	1.23	1.21	1
.00	.00	.00	1.21	1.19	1.19	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	
Material						
14.84	524.08	23.73	500.34	408.48	91.86	1
10.83	946.80	171.52	775.28	660.97	114.31	1
7.11	1351.95	340.47	1011.48	895.88	115.60	1
3.51	1748.45	510.71	1237.74	1122.14	115.60	1
.00	2140.10	796.32	1343.77	1343.55	.22	1

Time = 120. Degree of Consolidation = 66.0%

Total Settlement = .723

Settlement at End of Primary Consolidation = 1.097

Settlement caused by Primary Consolidation at time 120. = .723

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Settlement caused by Secondary Compression at time 120. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
7.60	6.48	1.09	6.00	6.00	10.00	2
7.45	6.33	1.06	6.00	5.83	5.68	2
7.30	6.19	1.04	6.00	5.75	4.98	2
7.14	6.04	1.02	6.00	5.68	4.89	2
6.99	5.90	1.00	6.00	5.63	4.80	2
6.84	5.75	.98	6.00	5.59	4.71	2
6.69	5.61	.96	6.00	5.55	4.62	2
6.54	5.47	.93	6.00	5.51	4.53	2
6.38	5.33	.91	6.00	5.47	4.44	2
6.23	5.19	.89	6.00	5.44	4.35	2
6.08	5.05	.87	6.00	5.40	4.26	2
5.93	4.91	.85	6.00	5.37	4.18	2
5.78	4.77	.83	6.00	5.33	4.09	2
5.62	4.63	.80	6.00	5.30	4.00	2
5.47	4.50	.78	6.00	5.27	3.99	2
5.32	4.36	.76	6.00	5.24	3.99	2
5.17	4.23	.74	6.00	5.21	3.98	2
5.02	4.09	.72	6.00	5.17	3.97	2
4.86	3.96	.69	6.00	5.14	3.97	2
4.71	3.83	.67	6.00	5.11	3.96	2
4.56	3.69	.65	6.00	5.09	3.96	2
4.41	3.56	.63	6.00	5.06	3.95	2
4.26	3.43	.61	6.00	5.03	3.94	2
4.10	3.30	.59	6.00	5.00	3.94	2
3.95	3.17	.56	6.00	4.97	3.93	2
3.80	3.04	.54	6.00	4.95	3.92	2
3.65	2.91	.52	6.00	4.92	3.92	2
3.50	2.78	.50	6.00	4.89	3.91	2
3.34	2.66	.48	6.00	4.86	3.91	2
3.19	2.53	.46	6.00	4.84	3.90	2
3.04	2.40	.43	6.00	4.81	3.89	2
2.89	2.28	.41	6.00	4.78	3.89	2
2.74	2.15	.39	6.00	4.76	3.88	2
2.58	2.03	.37	6.00	4.73	3.87	2
2.43	1.90	.35	6.00	4.70	3.87	2
2.28	1.78	.33	6.00	4.67	3.86	2
2.13	1.66	.30	6.00	4.64	3.86	2

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1.98	1.53	.28	6.00	4.62	3.85	2
1.82	1.41	.26	6.00	4.59	3.84	2
1.67	1.29	.24	6.00	4.56	3.84	2
1.52	1.17	.22	6.00	4.53	3.83	2
1.37	1.05	.20	6.00	4.50	3.82	2
1.22	.93	.17	6.00	4.48	3.82	2
1.06	.81	.15	6.00	4.45	3.81	2
.91	.69	.13	6.00	4.42	3.81	2
.76	.58	.11	6.00	4.39	3.80	2
.61	.46	.09	6.00	4.36	3.79	2
.46	.34	.07	6.00	4.33	3.79	2
.30	.23	.04	6.00	4.30	3.78	2
.15	.11	.02	6.00	4.27	3.77	2
.00	.00	.00	6.00	4.24	3.77	2

***** Stresses *****

***** Pore Pressures *****

XI Material	Total	Effective	Total	Static	Excess	
6.48	.00	.00	.00	.00	.00	2
6.33	11.76	1.91	9.85	9.45	.40	2
6.19	23.36	2.13	21.23	18.74	2.49	2
6.04	34.86	2.29	32.57	27.92	4.65	2
5.90	46.28	2.42	43.86	37.03	6.83	2
5.75	57.63	2.53	55.10	46.07	9.03	2
5.61	68.93	2.63	66.30	55.06	11.24	2
5.47	80.17	2.73	77.44	63.99	13.46	2
5.33	91.36	2.82	88.54	72.87	15.68	2
5.19	102.50	2.91	99.60	81.70	17.90	2
5.05	113.60	2.99	110.60	90.48	20.12	2
4.91	124.64	3.08	121.56	99.21	22.35	2
4.77	135.64	3.16	132.48	107.90	24.58	2
4.63	146.60	3.25	143.35	116.54	26.81	2
4.50	157.51	3.33	154.18	125.14	29.04	2
4.36	168.37	3.41	164.97	133.70	31.27	2
4.23	179.20	3.49	175.71	142.21	33.50	2
4.09	189.98	3.56	186.41	150.67	35.74	2
3.96	200.71	3.64	197.08	159.10	37.98	2
3.83	211.41	3.71	207.70	167.48	40.21	2
3.69	222.07	3.79	218.28	175.83	42.45	2
3.56	232.68	3.86	228.83	184.13	44.69	2
3.43	243.26	3.93	239.33	192.40	46.93	2
3.30	253.80	4.00	249.81	200.63	49.18	2
3.17	264.31	4.68	259.62	208.82	50.80	2
3.04	274.77	5.39	269.38	216.97	52.41	2
2.91	285.20	6.10	279.10	225.09	54.01	2
2.78	295.59	6.81	288.78	233.17	55.61	2
2.66	305.94	7.52	298.43	241.21	57.22	2
2.53	316.26	8.23	308.03	249.21	58.82	2
2.40	326.54	8.94	317.60	257.18	60.42	2

M12FGFIN.PSO						
2.28	336.78	9.65	327.13	265.11	62.02	2
2.15	346.98	10.37	336.62	273.00	63.61	2
2.03	357.15	11.08	346.07	280.86	65.21	2
1.90	367.28	11.80	355.48	288.67	66.80	2
1.78	377.37	12.52	364.85	296.45	68.39	2
1.66	387.42	13.25	374.18	304.19	69.98	2
1.53	397.44	13.97	383.46	311.89	71.57	2
1.41	407.41	14.70	392.71	319.56	73.15	2
1.29	417.35	15.43	401.92	327.18	74.74	2
1.17	427.25	16.16	411.09	334.77	76.31	2
1.05	437.11	16.90	420.21	342.32	77.89	2
.93	446.93	17.64	429.29	349.83	79.46	2
.81	456.71	18.39	438.33	357.30	81.03	2
.69	466.46	19.14	447.32	364.73	82.59	2
.58	476.16	19.89	456.27	372.12	84.15	2
.46	485.82	20.65	465.18	379.48	85.70	2
.34	495.45	21.41	474.04	386.79	87.25	2
.23	505.03	22.18	482.85	394.06	88.79	2
.11	514.57	22.95	491.62	401.29	90.33	2
.00	524.08	23.73	500.34	408.48	91.86	2

Time = 120. Degree of Consolidation = 54.%

Total Settlement = 1.116

Settlement at End of Primary Consolidation = 2.049

Settlement caused by Primary Consolidation at time 120. = 1.116

Settlement caused by Secondary Compression at time 120. = .000

Surface Elevation = 2.76

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
15.57	14.73	6.36	3.00	1.49	1.44	1
10.85	10.83	4.77	1.41	1.41	1.32	1
7.12	7.10	3.18	1.29	1.29	1.24	1
3.53	3.51	1.59	1.23	1.23	1.21	1
.00	.00	.00	1.21	1.19	1.19	1

M12FGFIN.PSO

***** Stresses ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	
Material						
14.73	452.20	70.13	382.06	309.44	72.62	1
10.83	868.47	182.69	685.78	555.48	130.30	1
7.10	1273.31	340.47	932.83	790.08	142.75	1
3.51	1669.85	510.71	1159.14	1016.38	142.75	1
.00	2061.37	812.14	1249.23	1237.67	11.56	1

Time = 365. Degree of Consolidation = 73.0%

Total Settlement = .832

Settlement at End of Primary Consolidation = 1.135

Settlement caused by Primary Consolidation at time 365. = .832

Settlement caused by Secondary Compression at time 365. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	
Material						
7.60	5.28	1.09	6.00	2.50	2.50	2
7.45	5.21	1.06	6.00	2.50	2.50	2
7.30	5.13	1.04	6.00	2.50	2.50	2
7.14	5.06	1.02	6.00	2.50	2.50	2
6.99	4.98	1.00	6.00	2.50	2.50	2
6.84	4.91	.98	6.00	2.66	4.11	2
6.69	4.81	.96	6.00	4.12	4.02	2
6.54	4.70	.93	6.00	4.14	4.00	2
6.38	4.59	.91	6.00	4.15	3.99	2
6.23	4.48	.89	6.00	4.15	3.98	2
6.08	4.37	.87	6.00	4.16	3.98	2
5.93	4.25	.85	6.00	4.16	3.97	2
5.78	4.14	.83	6.00	4.15	3.96	2
5.62	4.03	.80	6.00	4.15	3.96	2
5.47	3.92	.78	6.00	4.15	3.95	2
5.32	3.81	.76	6.00	4.14	3.95	2
5.17	3.69	.74	6.00	4.13	3.94	2
5.02	3.58	.72	6.00	4.12	3.93	2
4.86	3.47	.69	6.00	4.12	3.93	2
4.71	3.36	.67	6.00	4.11	3.92	2

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4.56	3.25	.65	6.00	4.10	3.91	2
4.41	3.14	.63	6.00	4.09	3.91	2
4.26	3.03	.61	6.00	4.08	3.90	2
4.10	2.92	.59	6.00	4.08	3.90	2
3.95	2.81	.56	6.00	4.07	3.89	2
3.80	2.70	.54	6.00	4.06	3.88	2
3.65	2.59	.52	6.00	4.05	3.88	2
3.50	2.48	.50	6.00	4.05	3.87	2
3.34	2.37	.48	6.00	4.04	3.86	2
3.19	2.26	.46	6.00	4.03	3.86	2
3.04	2.15	.43	6.00	4.02	3.85	2
2.89	2.04	.41	6.00	4.02	3.85	2
2.74	1.93	.39	6.00	4.01	3.84	2
2.58	1.83	.37	6.00	4.00	3.83	2
2.43	1.72	.35	6.00	3.99	3.83	2
2.28	1.61	.33	6.00	3.99	3.82	2
2.13	1.50	.30	6.00	3.98	3.81	2
1.98	1.39	.28	6.00	3.97	3.81	2
1.82	1.28	.26	6.00	3.97	3.80	2
1.67	1.18	.24	6.00	3.96	3.80	2
1.52	1.07	.22	6.00	3.95	3.79	2
1.37	.96	.20	6.00	3.95	3.78	2
1.22	.85	.17	6.00	3.94	3.78	2
1.06	.75	.15	6.00	3.93	3.77	2
.91	.64	.13	6.00	3.93	3.76	2
.76	.53	.11	6.00	3.92	3.76	2
.61	.43	.09	6.00	3.92	3.75	2
.46	.32	.07	6.00	3.91	3.75	2
.30	.21	.04	6.00	3.90	3.74	2
.15	.11	.02	6.00	3.90	3.73	2
.00	.00	.00	6.00	3.89	3.73	2

***** Stresses *****

***** Pore Pressures *****

XI Material	Total	Effective	Total	Static	Excess	
5.28	.00	.00	.00	.00	.00	2
5.21	5.39	5.39	.00	.00	.00	2
5.13	10.78	10.78	.00	.00	.00	2
5.06	16.17	16.17	.00	.00	.00	2
4.98	21.56	21.56	.00	.00	.00	2
4.91	27.16	27.16	.00	.00	.00	2
4.81	35.72	26.79	8.93	6.25	2.68	2
4.70	45.05	26.47	18.58	13.27	5.31	2
4.59	54.40	26.23	28.17	20.30	7.87	2
4.48	63.75	26.05	37.70	27.35	10.35	2
4.37	73.11	25.96	47.16	34.40	12.76	2
4.25	82.48	25.93	56.55	41.45	15.10	2
4.14	91.84	25.97	65.87	48.50	17.37	2
4.03	101.21	26.07	75.14	55.55	19.59	2

M12FGFIN.PSO

3.92	110.56	26.20	84.36	62.60	21.76	2
3.81	119.91	26.37	93.54	69.63	23.91	2
3.69	129.25	26.55	102.69	76.66	26.03	2
3.58	138.58	26.75	111.82	83.68	28.14	2
3.47	147.89	26.96	120.93	90.68	30.25	2
3.36	157.20	27.17	130.02	97.68	32.35	2
3.25	166.49	27.39	139.11	104.66	34.45	2
3.14	175.78	27.60	148.18	111.63	36.55	2
3.03	185.05	27.81	157.24	118.59	38.65	2
2.92	194.31	28.02	166.30	125.54	40.75	2
2.81	203.56	28.22	175.34	132.48	42.86	2
2.70	212.80	28.43	184.38	139.41	44.97	2
2.59	222.03	28.63	193.40	146.33	47.08	2
2.48	231.25	28.83	202.42	153.23	49.19	2
2.37	240.46	29.03	211.43	160.13	51.31	2
2.26	249.66	29.22	220.44	167.02	53.42	2
2.15	258.85	29.41	229.43	173.89	55.54	2
2.04	268.02	29.60	238.42	180.76	57.66	2
1.93	277.19	29.79	247.40	187.61	59.78	2
1.83	286.35	29.98	256.37	194.46	61.91	2
1.72	295.50	32.35	263.15	201.29	61.86	2
1.61	304.64	34.93	269.70	208.12	61.58	2
1.50	313.76	37.49	276.28	214.94	61.34	2
1.39	322.88	40.00	282.88	221.75	61.14	2
1.28	331.99	42.48	289.51	228.54	60.97	2
1.18	341.10	44.93	296.17	235.33	60.83	2
1.07	350.19	47.34	302.84	242.11	60.73	2
.96	359.27	49.73	309.54	248.89	60.65	2
.85	368.35	52.09	316.26	255.65	60.61	2
.75	377.41	54.42	322.99	262.40	60.59	2
.64	386.47	56.73	329.74	269.15	60.60	2
.53	395.52	59.01	336.51	275.88	60.62	2
.43	404.56	61.27	343.29	282.61	60.67	2
.32	413.59	63.51	350.08	289.33	60.74	2
.21	422.61	65.74	356.88	296.05	60.83	2
.11	431.63	67.94	363.69	302.75	60.94	2
.00	440.64	70.14	370.50	309.45	61.06	2

Time = 365. Degree of Consolidation = 82.0%

Total Settlement = 2.315

Settlement at End of Primary Consolidation = 2.439

Settlement caused by Primary Consolidation at time 365. = 2.007

Settlement caused by Secondary Compression at time 365. = .000

Settlement Due to Desiccation = .309

Surface Elevation = 1.45

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
15.57	14.67	6.36	3.00	1.44	1.44	1
10.85	10.82	4.77	1.41	1.39	1.31	1
7.12	7.10	3.18	1.29	1.29	1.24	1
3.53	3.51	1.59	1.23	1.23	1.21	1
.00	.00	.00	1.21	1.18	1.18	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	
Material						
14.67	439.71	138.60	301.11	284.73	16.39	1
10.82	852.69	206.97	645.72	527.46	118.25	1
7.10	1256.87	340.47	916.40	761.41	154.99	1
3.51	1653.49	510.71	1142.78	987.79	154.99	1
.00	2044.90	819.75	1225.14	1208.96	16.18	1

Time = 730. Degree of Consolidation = 78.0%

Total Settlement = .895

Settlement at End of Primary Consolidation = 1.154

Settlement caused by Primary Consolidation at time 730. = .895

Settlement caused by Secondary Compression at time 730. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
7.60	5.07	1.09	6.00	2.50	2.50	2

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7.45	5.00	1.06	6.00	2.50	2.50	2
7.30	4.92	1.04	6.00	2.50	2.50	2
7.14	4.84	1.02	6.00	2.50	2.50	2
6.99	4.77	1.00	6.00	2.50	2.50	2
6.84	4.69	.98	6.00	2.50	2.50	2
6.69	4.62	.96	6.00	2.50	2.50	2
6.54	4.52	.93	6.00	3.97	3.97	2
6.38	4.41	.91	6.00	3.97	3.97	2
6.23	4.30	.89	6.00	3.96	3.96	2
6.08	4.20	.87	6.00	3.96	3.96	2
5.93	4.09	.85	6.00	3.95	3.95	2
5.78	3.98	.83	6.00	3.94	3.94	2
5.62	3.87	.80	6.00	3.94	3.94	2
5.47	3.77	.78	6.00	3.93	3.93	2
5.32	3.66	.76	6.00	3.92	3.92	2
5.17	3.55	.74	6.00	3.92	3.92	2
5.02	3.45	.72	6.00	3.91	3.91	2
4.86	3.34	.69	6.00	3.91	3.91	2
4.71	3.23	.67	6.00	3.90	3.90	2
4.56	3.13	.65	6.00	3.89	3.89	2
4.41	3.02	.63	6.00	3.89	3.89	2
4.26	2.91	.61	6.00	3.88	3.88	2
4.10	2.81	.59	6.00	3.87	3.87	2
3.95	2.70	.56	6.00	3.87	3.87	2
3.80	2.60	.54	6.00	3.86	3.86	2
3.65	2.49	.52	6.00	3.86	3.86	2
3.50	2.39	.50	6.00	3.85	3.85	2
3.34	2.28	.48	6.00	3.84	3.84	2
3.19	2.18	.46	6.00	3.84	3.84	2
3.04	2.07	.43	6.00	3.83	3.83	2
2.89	1.97	.41	6.00	3.82	3.82	2
2.74	1.86	.39	6.00	3.82	3.82	2
2.58	1.76	.37	6.00	3.81	3.81	2
2.43	1.65	.35	6.00	3.81	3.81	2
2.28	1.55	.33	6.00	3.80	3.80	2
2.13	1.44	.30	6.00	3.79	3.79	2
1.98	1.34	.28	6.00	3.79	3.79	2
1.82	1.24	.26	6.00	3.78	3.78	2
1.67	1.13	.24	6.00	3.77	3.77	2
1.52	1.03	.22	6.00	3.77	3.77	2
1.37	.93	.20	6.00	3.76	3.76	2
1.22	.82	.17	6.00	3.76	3.76	2
1.06	.72	.15	6.00	3.75	3.75	2
.91	.62	.13	6.00	3.74	3.74	2
.76	.51	.11	6.00	3.74	3.74	2
.61	.41	.09	6.00	3.73	3.73	2
.46	.31	.07	6.00	3.72	3.72	2
.30	.20	.04	6.00	3.72	3.72	2
.15	.10	.02	6.00	3.71	3.71	2
.00	.00	.00	6.00	3.71	3.71	2

M12FGFIN.PSO

***** Stresses *****

***** Pore Pressures *****

XI Material	Total	Effective	Total	Static	Excess	
5.07	.00	.00	.00	.00	.00	2
5.00	5.39	5.39	.00	.00	.00	2
4.92	10.78	10.78	.00	.00	.00	2
4.84	16.17	16.17	.00	.00	.00	2
4.77	21.56	21.56	.00	.00	.00	2
4.69	26.95	26.95	.00	.00	.00	2
4.62	32.34	32.34	.00	.00	.00	2
4.52	39.39	39.39	.00	.00	.00	2
4.41	48.50	41.70	6.80	6.80	.00	2
4.30	57.61	44.01	13.59	13.59	.00	2
4.20	66.70	46.33	20.38	20.38	.00	2
4.09	75.79	48.64	27.15	27.15	.00	2
3.98	84.87	50.95	33.92	33.92	.00	2
3.87	93.94	53.26	40.68	40.68	.00	2
3.77	103.00	55.57	47.43	47.43	.00	2
3.66	112.05	57.89	54.17	54.17	.00	2
3.55	121.10	60.20	60.90	60.90	.00	2
3.45	130.13	62.51	67.63	67.63	.00	2
3.34	139.16	64.82	74.34	74.34	.00	2
3.23	148.18	67.13	81.05	81.05	.00	2
3.13	157.19	69.45	87.75	87.75	.00	2
3.02	166.19	71.76	94.44	94.44	.00	2
2.91	175.19	74.07	101.12	101.12	.00	2
2.81	184.17	76.38	107.79	107.79	.00	2
2.70	193.15	78.69	114.45	114.45	.00	2
2.60	202.12	81.00	121.11	121.11	.00	2
2.49	211.07	83.32	127.76	127.76	.00	2
2.39	220.02	85.63	134.40	134.40	.00	2
2.28	228.97	87.94	141.03	141.03	.00	2
2.18	237.90	90.25	147.65	147.65	.00	2
2.07	246.82	92.56	154.26	154.26	.00	2
1.97	255.74	94.88	160.86	160.86	.00	2
1.86	264.65	97.19	167.46	167.46	.00	2
1.76	273.55	99.50	174.05	174.05	.00	2
1.65	282.44	101.81	180.63	180.63	.00	2
1.55	291.32	104.12	187.20	187.20	.00	2
1.44	300.19	106.44	193.76	193.76	.00	2
1.34	309.06	108.75	200.31	200.31	.00	2
1.24	317.92	111.06	206.86	206.86	.00	2
1.13	326.76	113.37	213.39	213.39	.00	2
1.03	335.60	115.68	219.92	219.92	.00	2
.93	344.43	118.00	226.44	226.44	.00	2
.82	353.26	120.31	232.95	232.95	.00	2
.72	362.07	122.62	239.45	239.45	.00	2
.62	370.88	124.93	245.94	245.94	.00	2
.51	379.67	127.24	252.43	252.43	.00	2

M12FGFIN.PSO						
.41	388.46	129.55	258.91	258.91	.00	2
.31	397.24	131.87	265.37	265.37	.00	2
.20	406.01	134.18	271.83	271.83	.00	2
.10	414.77	136.44	278.33	278.28	.05	2
.00	423.53	138.60	284.93	284.73	.21	2

Time = 730. Degree of Consolidation = 86.%

Total Settlement = 2.527

Settlement at End of Primary Consolidation = 2.527

Settlement caused by Primary Consolidation at time 730. = 2.180

Settlement caused by Secondary Compression at time 730. = .000

Settlement Due to Desiccation = .347

Surface Elevation = 1.18

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
15.57	14.64	6.36	3.00	1.44	1.44	1
10.85	10.81	4.77	1.41	1.37	1.31	1
7.12	7.10	3.18	1.29	1.29	1.24	1
3.53	3.51	1.59	1.23	1.23	1.21	1
.00	.00	.00	1.21	1.18	1.18	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	
Material						
14.64	439.71	138.65	301.06	284.72	16.34	1
10.81	851.42	225.42	626.00	526.20	99.80	1
7.10	1255.11	340.47	914.64	759.65	154.99	1
3.51	1651.78	510.71	1141.07	986.09	154.99	1
.00	2043.13	819.75	1223.38	1207.20	16.18	1

Time = 1095. Degree of Consolidation = 80.%

Total Settlement = .923

M12FGFIN.PSO

Settlement at End of Primary Consolidation = 1.154

Settlement caused by Primary Consolidation at time 1095. = .923

Settlement caused by Secondary Compression at time 1095. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
Material	A	XI	Z	Einitial	E	Eeop
	7.60	5.07	1.09	6.00	2.50	2.50
	7.45	5.00	1.06	6.00	2.50	2.50
	7.30	4.92	1.04	6.00	2.50	2.50
	7.14	4.84	1.02	6.00	2.50	2.50
	6.99	4.77	1.00	6.00	2.50	2.50
	6.84	4.69	.98	6.00	2.50	2.50
	6.69	4.62	.96	6.00	2.50	2.50
	6.54	4.52	.93	6.00	3.97	3.97
	6.38	4.41	.91	6.00	3.97	3.97
	6.23	4.30	.89	6.00	3.96	3.96
	6.08	4.20	.87	6.00	3.96	3.96
	5.93	4.09	.85	6.00	3.95	3.95
	5.78	3.98	.83	6.00	3.94	3.94
	5.62	3.87	.80	6.00	3.94	3.94
	5.47	3.77	.78	6.00	3.93	3.93
	5.32	3.66	.76	6.00	3.92	3.92
	5.17	3.55	.74	6.00	3.92	3.92
	5.02	3.45	.72	6.00	3.91	3.91
	4.86	3.34	.69	6.00	3.91	3.91
	4.71	3.23	.67	6.00	3.90	3.90
	4.56	3.13	.65	6.00	3.89	3.89
	4.41	3.02	.63	6.00	3.89	3.89
	4.26	2.91	.61	6.00	3.88	3.88
	4.10	2.81	.59	6.00	3.87	3.87
	3.95	2.70	.56	6.00	3.87	3.87
	3.80	2.60	.54	6.00	3.86	3.86
	3.65	2.49	.52	6.00	3.86	3.86
	3.50	2.39	.50	6.00	3.85	3.85
	3.34	2.28	.48	6.00	3.84	3.84
	3.19	2.18	.46	6.00	3.84	3.84
	3.04	2.07	.43	6.00	3.83	3.83
	2.89	1.97	.41	6.00	3.82	3.82
	2.74	1.86	.39	6.00	3.82	3.82

M12FGFIN.PSO

2.58	1.76	.37	6.00	3.81	3.81	2
2.43	1.65	.35	6.00	3.81	3.81	2
2.28	1.55	.33	6.00	3.80	3.80	2
2.13	1.44	.30	6.00	3.79	3.79	2
1.98	1.34	.28	6.00	3.79	3.79	2
1.82	1.24	.26	6.00	3.78	3.78	2
1.67	1.13	.24	6.00	3.77	3.77	2
1.52	1.03	.22	6.00	3.77	3.77	2
1.37	.93	.20	6.00	3.76	3.76	2
1.22	.82	.17	6.00	3.76	3.76	2
1.06	.72	.15	6.00	3.75	3.75	2
.91	.62	.13	6.00	3.74	3.74	2
.76	.51	.11	6.00	3.74	3.74	2
.61	.41	.09	6.00	3.73	3.73	2
.46	.31	.07	6.00	3.72	3.72	2
.30	.20	.04	6.00	3.72	3.72	2
.15	.10	.02	6.00	3.71	3.71	2
.00	.00	.00	6.00	3.71	3.71	2

***** Stresses *****

***** Pore Pressures *****

XI Material	Total	Effective	Total	Static	Excess	
5.07	.00	.00	.00	.00	.00	2
5.00	5.39	5.39	.00	.00	.00	2
4.92	10.78	10.78	.00	.00	.00	2
4.84	16.17	16.17	.00	.00	.00	2
4.77	21.56	21.56	.00	.00	.00	2
4.69	26.95	26.95	.00	.00	.00	2
4.62	32.34	32.34	.00	.00	.00	2
4.52	39.39	39.39	.00	.00	.00	2
4.41	48.50	41.70	6.80	6.80	.00	2
4.30	57.61	44.01	13.59	13.59	.00	2
4.20	66.70	46.33	20.38	20.38	.00	2
4.09	75.79	48.64	27.15	27.15	.00	2
3.98	84.87	50.95	33.92	33.92	.00	2
3.87	93.94	53.26	40.68	40.68	.00	2
3.77	103.00	55.57	47.43	47.43	.00	2
3.66	112.05	57.89	54.17	54.17	.00	2
3.55	121.10	60.20	60.90	60.90	.00	2
3.45	130.13	62.51	67.63	67.63	.00	2
3.34	139.16	64.82	74.34	74.34	.00	2
3.23	148.18	67.13	81.05	81.05	.00	2
3.13	157.19	69.45	87.75	87.75	.00	2
3.02	166.19	71.76	94.44	94.44	.00	2
2.91	175.19	74.07	101.12	101.12	.00	2
2.81	184.17	76.38	107.79	107.79	.00	2
2.70	193.15	78.69	114.45	114.45	.00	2
2.60	202.12	81.00	121.11	121.11	.00	2
2.49	211.07	83.32	127.76	127.76	.00	2

M12FGFIN.PSO

2.39	220.02	85.63	134.40	134.40	.00	2
2.28	228.97	87.94	141.03	141.03	.00	2
2.18	237.90	90.25	147.65	147.65	.00	2
2.07	246.82	92.56	154.26	154.26	.00	2
1.97	255.74	94.88	160.86	160.86	.00	2
1.86	264.65	97.19	167.46	167.46	.00	2
1.76	273.55	99.50	174.05	174.05	.00	2
1.65	282.44	101.81	180.63	180.63	.00	2
1.55	291.32	104.12	187.20	187.20	.00	2
1.44	300.19	106.44	193.76	193.76	.00	2
1.34	309.06	108.75	200.31	200.31	.00	2
1.24	317.92	111.06	206.86	206.86	.00	2
1.13	326.76	113.37	213.39	213.39	.00	2
1.03	335.60	115.68	219.92	219.92	.00	2
.93	344.43	118.00	226.44	226.44	.00	2
.82	353.26	120.31	232.95	232.95	.00	2
.72	362.07	122.62	239.45	239.45	.00	2
.62	370.88	124.93	245.94	245.94	.00	2
.51	379.67	127.24	252.43	252.43	.00	2
.41	388.46	129.55	258.91	258.91	.00	2
.31	397.24	131.87	265.37	265.37	.00	2
.20	406.01	134.18	271.83	271.83	.00	2
.10	414.77	136.47	278.30	278.28	.02	2
.00	423.53	138.65	284.88	284.72	.15	2

Time = 1095. Degree of Consolidation = 86.0%

Total Settlement = 2.527

Settlement at End of Primary Consolidation = 2.527

Settlement caused by Primary Consolidation at time 1095. = 2.180

Settlement caused by Secondary Compression at time 1095. = .000

Settlement Due to Desiccation = .347

Surface Elevation = 1.15

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
15.57	14.62	6.36	3.00	1.44	1.44	1

M12FGFIN.PSO						
10.85	10.80	4.77	1.41	1.37	1.31	1
7.12	7.10	3.18	1.29	1.29	1.24	1
3.53	3.51	1.59	1.23	1.23	1.21	1
.00	.00	.00	1.21	1.18	1.18	1

Time = 1460. Degree of Consolidation = 82.%

Total Settlement = .944

Settlement at End of Primary Consolidation = 1.154

Settlement caused by Primary Consolidation at time 1460. = .944

Settlement caused by Secondary Compression at time 1460. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
7.60	5.07	1.09	6.00	2.50	2.50	2
7.45	5.00	1.06	6.00	2.50	2.50	2
7.30	4.92	1.04	6.00	2.50	2.50	2
7.14	4.84	1.02	6.00	2.50	2.50	2
6.99	4.77	1.00	6.00	2.50	2.50	2
6.84	4.69	.98	6.00	2.50	2.50	2
6.69	4.62	.96	6.00	2.50	2.50	2
6.54	4.52	.93	6.00	3.97	3.97	2
6.38	4.41	.91	6.00	3.97	3.97	2
6.23	4.30	.89	6.00	3.96	3.96	2
6.08	4.20	.87	6.00	3.96	3.96	2
5.93	4.09	.85	6.00	3.95	3.95	2
5.78	3.98	.83	6.00	3.94	3.94	2
5.62	3.87	.80	6.00	3.94	3.94	2
5.47	3.77	.78	6.00	3.93	3.93	2
5.32	3.66	.76	6.00	3.92	3.92	2
5.17	3.55	.74	6.00	3.92	3.92	2
5.02	3.45	.72	6.00	3.91	3.91	2
4.86	3.34	.69	6.00	3.91	3.91	2
4.71	3.23	.67	6.00	3.90	3.90	2
4.56	3.13	.65	6.00	3.89	3.89	2
4.41	3.02	.63	6.00	3.89	3.89	2
4.26	2.91	.61	6.00	3.88	3.88	2
4.10	2.81	.59	6.00	3.87	3.87	2
3.95	2.70	.56	6.00	3.87	3.87	2

M12FGFIN.PSO						
3.80	2.60	.54	6.00	3.86	3.86	2
3.65	2.49	.52	6.00	3.86	3.86	2
3.50	2.39	.50	6.00	3.85	3.85	2
3.34	2.28	.48	6.00	3.84	3.84	2
3.19	2.18	.46	6.00	3.84	3.84	2
3.04	2.07	.43	6.00	3.83	3.83	2
2.89	1.97	.41	6.00	3.82	3.82	2
2.74	1.86	.39	6.00	3.82	3.82	2
2.58	1.76	.37	6.00	3.81	3.81	2
2.43	1.65	.35	6.00	3.81	3.81	2
2.28	1.55	.33	6.00	3.80	3.80	2
2.13	1.44	.30	6.00	3.79	3.79	2
1.98	1.34	.28	6.00	3.79	3.79	2
1.82	1.24	.26	6.00	3.78	3.78	2
1.67	1.13	.24	6.00	3.77	3.77	2
1.52	1.03	.22	6.00	3.77	3.77	2
1.37	.93	.20	6.00	3.76	3.76	2
1.22	.82	.17	6.00	3.76	3.76	2
1.06	.72	.15	6.00	3.75	3.75	2
.91	.62	.13	6.00	3.74	3.74	2
.76	.51	.11	6.00	3.74	3.74	2
.61	.41	.09	6.00	3.73	3.73	2
.46	.31	.07	6.00	3.72	3.72	2
.30	.20	.04	6.00	3.72	3.72	2
.15	.10	.02	6.00	3.71	3.71	2
.00	.00	.00	6.00	3.71	3.71	2

Time = 1460. Degree of Consolidation = 86.0%

Total Settlement = 2.527

Settlement at End of Primary Consolidation = 2.527

Settlement caused by Primary Consolidation at time 1460. = 2.180

Settlement caused by Secondary Compression at time 1460. = .000

Settlement Due to Desiccation = .347

Surface Elevation = 1.13

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****		
A	XI	Z	Einitial	E	Eeop

M12FGFIN.PSO

Material

15.57	14.61	6.36	3.00	1.44	1.44	1
10.85	10.80	4.77	1.41	1.36	1.31	1
7.12	7.10	3.18	1.29	1.29	1.24	1
3.53	3.51	1.59	1.23	1.23	1.21	1
.00	.00	.00	1.21	1.18	1.18	1

Time = 1825. Degree of Consolidation = 83.0%

Total Settlement = .959

Settlement at End of Primary Consolidation = 1.154

Settlement caused by Primary Consolidation at time 1825. = .959

Settlement caused by Secondary Compression at time 1825. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

Material	A	XI	Z	Einitial	E	Eeop	
	7.60	5.07	1.09	6.00	2.50	2.50	2
	7.45	5.00	1.06	6.00	2.50	2.50	2
	7.30	4.92	1.04	6.00	2.50	2.50	2
	7.14	4.84	1.02	6.00	2.50	2.50	2
	6.99	4.77	1.00	6.00	2.50	2.50	2
	6.84	4.69	.98	6.00	2.50	2.50	2
	6.69	4.62	.96	6.00	2.50	2.50	2
	6.54	4.52	.93	6.00	3.97	3.97	2
	6.38	4.41	.91	6.00	3.97	3.97	2
	6.23	4.30	.89	6.00	3.96	3.96	2
	6.08	4.20	.87	6.00	3.96	3.96	2
	5.93	4.09	.85	6.00	3.95	3.95	2
	5.78	3.98	.83	6.00	3.94	3.94	2
	5.62	3.87	.80	6.00	3.94	3.94	2
	5.47	3.77	.78	6.00	3.93	3.93	2
	5.32	3.66	.76	6.00	3.92	3.92	2
	5.17	3.55	.74	6.00	3.92	3.92	2
	5.02	3.45	.72	6.00	3.91	3.91	2
	4.86	3.34	.69	6.00	3.91	3.91	2
	4.71	3.23	.67	6.00	3.90	3.90	2
	4.56	3.13	.65	6.00	3.89	3.89	2
	4.41	3.02	.63	6.00	3.89	3.89	2
	4.26	2.91	.61	6.00	3.88	3.88	2

M12FGFIN.PSO						
4.10	2.81	.59	6.00	3.87	3.87	2
3.95	2.70	.56	6.00	3.87	3.87	2
3.80	2.60	.54	6.00	3.86	3.86	2
3.65	2.49	.52	6.00	3.86	3.86	2
3.50	2.39	.50	6.00	3.85	3.85	2
3.34	2.28	.48	6.00	3.84	3.84	2
3.19	2.18	.46	6.00	3.84	3.84	2
3.04	2.07	.43	6.00	3.83	3.83	2
2.89	1.97	.41	6.00	3.82	3.82	2
2.74	1.86	.39	6.00	3.82	3.82	2
2.58	1.76	.37	6.00	3.81	3.81	2
2.43	1.65	.35	6.00	3.81	3.81	2
2.28	1.55	.33	6.00	3.80	3.80	2
2.13	1.44	.30	6.00	3.79	3.79	2
1.98	1.34	.28	6.00	3.79	3.79	2
1.82	1.24	.26	6.00	3.78	3.78	2
1.67	1.13	.24	6.00	3.77	3.77	2
1.52	1.03	.22	6.00	3.77	3.77	2
1.37	.93	.20	6.00	3.76	3.76	2
1.22	.82	.17	6.00	3.76	3.76	2
1.06	.72	.15	6.00	3.75	3.75	2
.91	.62	.13	6.00	3.74	3.74	2
.76	.51	.11	6.00	3.74	3.74	2
.61	.41	.09	6.00	3.73	3.73	2
.46	.31	.07	6.00	3.72	3.72	2
.30	.20	.04	6.00	3.72	3.72	2
.15	.10	.02	6.00	3.71	3.71	2
.00	.00	.00	6.00	3.71	3.71	2

Time = 1825. Degree of Consolidation = 86.0%

Total Settlement = 2.527

Settlement at End of Primary Consolidation = 2.527

Settlement caused by Primary Consolidation at time 1825. = 2.180

Settlement caused by Secondary Compression at time 1825. = .000

Settlement Due to Desiccation = .347

Surface Elevation = 1.11

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****

***** Void Ratios *****

M12FGFIN.PSO

A	XI	Z	Einitial	E	Eeop	
Material						
15.57	14.60	6.36	3.00	1.44	1.44	1
10.85	10.79	4.77	1.41	1.35	1.31	1
7.12	7.10	3.18	1.29	1.29	1.24	1
3.53	3.51	1.59	1.23	1.23	1.21	1
.00	.00	.00	1.21	1.18	1.18	1

Time = 2190. Degree of Consolidation = 84.0%

Total Settlement = .971

Settlement at End of Primary Consolidation = 1.154

Settlement caused by Primary Consolidation at time 2190. = .971

Settlement caused by Secondary Compression at time 2190. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
7.60	5.07	1.09	6.00	2.50	2.50	2
7.45	5.00	1.06	6.00	2.50	2.50	2
7.30	4.92	1.04	6.00	2.50	2.50	2
7.14	4.84	1.02	6.00	2.50	2.50	2
6.99	4.77	1.00	6.00	2.50	2.50	2
6.84	4.69	.98	6.00	2.50	2.50	2
6.69	4.62	.96	6.00	2.50	2.50	2
6.54	4.52	.93	6.00	3.97	3.97	2
6.38	4.41	.91	6.00	3.97	3.97	2
6.23	4.30	.89	6.00	3.96	3.96	2
6.08	4.20	.87	6.00	3.96	3.96	2
5.93	4.09	.85	6.00	3.95	3.95	2
5.78	3.98	.83	6.00	3.94	3.94	2
5.62	3.87	.80	6.00	3.94	3.94	2
5.47	3.77	.78	6.00	3.93	3.93	2
5.32	3.66	.76	6.00	3.92	3.92	2
5.17	3.55	.74	6.00	3.92	3.92	2
5.02	3.45	.72	6.00	3.91	3.91	2
4.86	3.34	.69	6.00	3.91	3.91	2
4.71	3.23	.67	6.00	3.90	3.90	2
4.56	3.13	.65	6.00	3.89	3.89	2

M12FGFIN.PSO						
4.41	3.02	.63	6.00	3.89	3.89	2
4.26	2.91	.61	6.00	3.88	3.88	2
4.10	2.81	.59	6.00	3.87	3.87	2
3.95	2.70	.56	6.00	3.87	3.87	2
3.80	2.60	.54	6.00	3.86	3.86	2
3.65	2.49	.52	6.00	3.86	3.86	2
3.50	2.39	.50	6.00	3.85	3.85	2
3.34	2.28	.48	6.00	3.84	3.84	2
3.19	2.18	.46	6.00	3.84	3.84	2
3.04	2.07	.43	6.00	3.83	3.83	2
2.89	1.97	.41	6.00	3.82	3.82	2
2.74	1.86	.39	6.00	3.82	3.82	2
2.58	1.76	.37	6.00	3.81	3.81	2
2.43	1.65	.35	6.00	3.81	3.81	2
2.28	1.55	.33	6.00	3.80	3.80	2
2.13	1.44	.30	6.00	3.79	3.79	2
1.98	1.34	.28	6.00	3.79	3.79	2
1.82	1.24	.26	6.00	3.78	3.78	2
1.67	1.13	.24	6.00	3.77	3.77	2
1.52	1.03	.22	6.00	3.77	3.77	2
1.37	.93	.20	6.00	3.76	3.76	2
1.22	.82	.17	6.00	3.76	3.76	2
1.06	.72	.15	6.00	3.75	3.75	2
.91	.62	.13	6.00	3.74	3.74	2
.76	.51	.11	6.00	3.74	3.74	2
.61	.41	.09	6.00	3.73	3.73	2
.46	.31	.07	6.00	3.72	3.72	2
.30	.20	.04	6.00	3.72	3.72	2
.15	.10	.02	6.00	3.71	3.71	2
.00	.00	.00	6.00	3.71	3.71	2

Time = 2190. Degree of Consolidation = 86.0%

Total Settlement = 2.527

Settlement at End of Primary Consolidation = 2.527

Settlement caused by Primary Consolidation at time 2190. = 2.180

Settlement caused by Secondary Compression at time 2190. = .000

Settlement Due to Desiccation = .347

Surface Elevation = 1.10

*****Current Conditions in Compressible Foundation*****

M12FGFIN.PSO

***** Coordinates *****

***** Void Ratios *****

Material	A	XI	Z	Einitial	E	Eeop	
	15.57	14.59	6.36	3.00	1.44	1.44	1
	10.85	10.78	4.77	1.41	1.35	1.31	1
	7.12	7.10	3.18	1.29	1.29	1.24	1
	3.53	3.51	1.59	1.23	1.23	1.21	1
	.00	.00	.00	1.21	1.18	1.18	1

Time = 2555. Degree of Consolidation = 85.0%

Total Settlement = .980

Settlement at End of Primary Consolidation = 1.154

Settlement caused by Primary Consolidation at time 2555. = .980

Settlement caused by Secondary Compression at time 2555. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

Material	A	XI	Z	Einitial	E	Eeop	
	7.60	5.07	1.09	6.00	2.50	2.50	2
	7.45	5.00	1.06	6.00	2.50	2.50	2
	7.30	4.92	1.04	6.00	2.50	2.50	2
	7.14	4.84	1.02	6.00	2.50	2.50	2
	6.99	4.77	1.00	6.00	2.50	2.50	2
	6.84	4.69	.98	6.00	2.50	2.50	2
	6.69	4.62	.96	6.00	2.50	2.50	2
	6.54	4.52	.93	6.00	3.97	3.97	2
	6.38	4.41	.91	6.00	3.97	3.97	2
	6.23	4.30	.89	6.00	3.96	3.96	2
	6.08	4.20	.87	6.00	3.96	3.96	2
	5.93	4.09	.85	6.00	3.95	3.95	2
	5.78	3.98	.83	6.00	3.94	3.94	2
	5.62	3.87	.80	6.00	3.94	3.94	2
	5.47	3.77	.78	6.00	3.93	3.93	2
	5.32	3.66	.76	6.00	3.92	3.92	2
	5.17	3.55	.74	6.00	3.92	3.92	2
	5.02	3.45	.72	6.00	3.91	3.91	2
	4.86	3.34	.69	6.00	3.91	3.91	2

M12FGFIN.PSO						
4.71	3.23	.67	6.00	3.90	3.90	2
4.56	3.13	.65	6.00	3.89	3.89	2
4.41	3.02	.63	6.00	3.89	3.89	2
4.26	2.91	.61	6.00	3.88	3.88	2
4.10	2.81	.59	6.00	3.87	3.87	2
3.95	2.70	.56	6.00	3.87	3.87	2
3.80	2.60	.54	6.00	3.86	3.86	2
3.65	2.49	.52	6.00	3.86	3.86	2
3.50	2.39	.50	6.00	3.85	3.85	2
3.34	2.28	.48	6.00	3.84	3.84	2
3.19	2.18	.46	6.00	3.84	3.84	2
3.04	2.07	.43	6.00	3.83	3.83	2
2.89	1.97	.41	6.00	3.82	3.82	2
2.74	1.86	.39	6.00	3.82	3.82	2
2.58	1.76	.37	6.00	3.81	3.81	2
2.43	1.65	.35	6.00	3.81	3.81	2
2.28	1.55	.33	6.00	3.80	3.80	2
2.13	1.44	.30	6.00	3.79	3.79	2
1.98	1.34	.28	6.00	3.79	3.79	2
1.82	1.24	.26	6.00	3.78	3.78	2
1.67	1.13	.24	6.00	3.77	3.77	2
1.52	1.03	.22	6.00	3.77	3.77	2
1.37	.93	.20	6.00	3.76	3.76	2
1.22	.82	.17	6.00	3.76	3.76	2
1.06	.72	.15	6.00	3.75	3.75	2
.91	.62	.13	6.00	3.74	3.74	2
.76	.51	.11	6.00	3.74	3.74	2
.61	.41	.09	6.00	3.73	3.73	2
.46	.31	.07	6.00	3.72	3.72	2
.30	.20	.04	6.00	3.72	3.72	2
.15	.10	.02	6.00	3.71	3.71	2
.00	.00	.00	6.00	3.71	3.71	2

Time = 2555. Degree of Consolidation = 86.%

Total Settlement = 2.527

Settlement at End of Primary Consolidation = 2.527

Settlement caused by Primary Consolidation at time 2555. = 2.180

Settlement caused by Secondary Compression at time 2555. = .000

Settlement Due to Desiccation = .347

Surface Elevation = 1.09

M12FGFIN.PSO

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
15.57	14.58	6.36	3.00	1.44	1.44	1
10.85	10.78	4.77	1.41	1.35	1.31	1
7.12	7.10	3.18	1.29	1.29	1.24	1
3.53	3.51	1.59	1.23	1.23	1.21	1
.00	.00	.00	1.21	1.18	1.18	1
Time = 2920. Degree of Consolidation = 86.%						
Total Settlement = .988						
Settlement at End of Primary Consolidation = 1.154						
Settlement caused by Primary Consolidation at time 2920. = .988						
Settlement caused by Secondary Compression at time 2920. = .000						

*****Current Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
7.60	5.07	1.09	6.00	2.50	2.50	2
7.45	5.00	1.06	6.00	2.50	2.50	2
7.30	4.92	1.04	6.00	2.50	2.50	2
7.14	4.84	1.02	6.00	2.50	2.50	2
6.99	4.77	1.00	6.00	2.50	2.50	2
6.84	4.69	.98	6.00	2.50	2.50	2
6.69	4.62	.96	6.00	2.50	2.50	2
6.54	4.52	.93	6.00	3.97	3.97	2
6.38	4.41	.91	6.00	3.97	3.97	2
6.23	4.30	.89	6.00	3.96	3.96	2
6.08	4.20	.87	6.00	3.96	3.96	2
5.93	4.09	.85	6.00	3.95	3.95	2
5.78	3.98	.83	6.00	3.94	3.94	2
5.62	3.87	.80	6.00	3.94	3.94	2
5.47	3.77	.78	6.00	3.93	3.93	2
5.32	3.66	.76	6.00	3.92	3.92	2
5.17	3.55	.74	6.00	3.92	3.92	2

M12FGFIN.PSO						
5.02	3.45	.72	6.00	3.91	3.91	2
4.86	3.34	.69	6.00	3.91	3.91	2
4.71	3.23	.67	6.00	3.90	3.90	2
4.56	3.13	.65	6.00	3.89	3.89	2
4.41	3.02	.63	6.00	3.89	3.89	2
4.26	2.91	.61	6.00	3.88	3.88	2
4.10	2.81	.59	6.00	3.87	3.87	2
3.95	2.70	.56	6.00	3.87	3.87	2
3.80	2.60	.54	6.00	3.86	3.86	2
3.65	2.49	.52	6.00	3.86	3.86	2
3.50	2.39	.50	6.00	3.85	3.85	2
3.34	2.28	.48	6.00	3.84	3.84	2
3.19	2.18	.46	6.00	3.84	3.84	2
3.04	2.07	.43	6.00	3.83	3.83	2
2.89	1.97	.41	6.00	3.82	3.82	2
2.74	1.86	.39	6.00	3.82	3.82	2
2.58	1.76	.37	6.00	3.81	3.81	2
2.43	1.65	.35	6.00	3.81	3.81	2
2.28	1.55	.33	6.00	3.80	3.80	2
2.13	1.44	.30	6.00	3.79	3.79	2
1.98	1.34	.28	6.00	3.79	3.79	2
1.82	1.24	.26	6.00	3.78	3.78	2
1.67	1.13	.24	6.00	3.77	3.77	2
1.52	1.03	.22	6.00	3.77	3.77	2
1.37	.93	.20	6.00	3.76	3.76	2
1.22	.82	.17	6.00	3.76	3.76	2
1.06	.72	.15	6.00	3.75	3.75	2
.91	.62	.13	6.00	3.74	3.74	2
.76	.51	.11	6.00	3.74	3.74	2
.61	.41	.09	6.00	3.73	3.73	2
.46	.31	.07	6.00	3.72	3.72	2
.30	.20	.04	6.00	3.72	3.72	2
.15	.10	.02	6.00	3.71	3.71	2
.00	.00	.00	6.00	3.71	3.71	2

Time = 2920. Degree of Consolidation = 86.%

Total Settlement = 2.527

Settlement at End of Primary Consolidation = 2.527

Settlement caused by Primary Consolidation at time 2920. = 2.180

Settlement caused by Secondary Compression at time 2920. = .000

Settlement Due to Desiccation = .347

Surface Elevation = 1.09

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
Material	A	XI	Z	Einitial	E	Eeop
	15.57	14.57	6.36	3.00	1.44	1.44
	10.85	10.77	4.77	1.41	1.35	1.31
	7.12	7.10	3.18	1.29	1.28	1.24
	3.53	3.51	1.59	1.23	1.23	1.21
	.00	.00	.00	1.21	1.18	1.18
Time = 3650. Degree of Consolidation = 87.%						
Total Settlement = .999						
Settlement at End of Primary Consolidation = 1.154						
Settlement caused by Primary Consolidation at time 3650. = .999						
Settlement caused by Secondary Compression at time 3650. = .000						

*****Current Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
Material	A	XI	Z	Einitial	E	Eeop
	7.60	5.07	1.09	6.00	2.50	2.50
	7.45	5.00	1.06	6.00	2.50	2.50
	7.30	4.92	1.04	6.00	2.50	2.50
	7.14	4.84	1.02	6.00	2.50	2.50
	6.99	4.77	1.00	6.00	2.50	2.50
	6.84	4.69	.98	6.00	2.50	2.50
	6.69	4.62	.96	6.00	2.50	2.50
	6.54	4.52	.93	6.00	3.97	3.97
	6.38	4.41	.91	6.00	3.97	3.97
	6.23	4.30	.89	6.00	3.96	3.96
	6.08	4.20	.87	6.00	3.96	3.96
	5.93	4.09	.85	6.00	3.95	3.95
	5.78	3.98	.83	6.00	3.94	3.94
	5.62	3.87	.80	6.00	3.94	3.94
	5.47	3.77	.78	6.00	3.93	3.93

M12FGFIN.PSO						
5.32	3.66	.76	6.00	3.92	3.92	2
5.17	3.55	.74	6.00	3.92	3.92	2
5.02	3.45	.72	6.00	3.91	3.91	2
4.86	3.34	.69	6.00	3.91	3.91	2
4.71	3.23	.67	6.00	3.90	3.90	2
4.56	3.13	.65	6.00	3.89	3.89	2
4.41	3.02	.63	6.00	3.89	3.89	2
4.26	2.91	.61	6.00	3.88	3.88	2
4.10	2.81	.59	6.00	3.87	3.87	2
3.95	2.70	.56	6.00	3.87	3.87	2
3.80	2.60	.54	6.00	3.86	3.86	2
3.65	2.49	.52	6.00	3.86	3.86	2
3.50	2.39	.50	6.00	3.85	3.85	2
3.34	2.28	.48	6.00	3.84	3.84	2
3.19	2.18	.46	6.00	3.84	3.84	2
3.04	2.07	.43	6.00	3.83	3.83	2
2.89	1.97	.41	6.00	3.82	3.82	2
2.74	1.86	.39	6.00	3.82	3.82	2
2.58	1.76	.37	6.00	3.81	3.81	2
2.43	1.65	.35	6.00	3.81	3.81	2
2.28	1.55	.33	6.00	3.80	3.80	2
2.13	1.44	.30	6.00	3.79	3.79	2
1.98	1.34	.28	6.00	3.79	3.79	2
1.82	1.24	.26	6.00	3.78	3.78	2
1.67	1.13	.24	6.00	3.77	3.77	2
1.52	1.03	.22	6.00	3.77	3.77	2
1.37	.93	.20	6.00	3.76	3.76	2
1.22	.82	.17	6.00	3.76	3.76	2
1.06	.72	.15	6.00	3.75	3.75	2
.91	.62	.13	6.00	3.74	3.74	2
.76	.51	.11	6.00	3.74	3.74	2
.61	.41	.09	6.00	3.73	3.73	2
.46	.31	.07	6.00	3.72	3.72	2
.30	.20	.04	6.00	3.72	3.72	2
.15	.10	.02	6.00	3.71	3.71	2
.00	.00	.00	6.00	3.71	3.71	2

Time = 3650. Degree of Consolidation = 86.%

Total Settlement = 2.527

Settlement at End of Primary Consolidation = 2.527

Settlement caused by Primary Consolidation at time 3650. = 2.180

Settlement caused by Secondary Compression at time 3650. = .000

Settlement Due to Desiccation = .347

Surface Elevation = 1.07

APPENDIX N

SETTLE AND PSDDF ANALYSIS: BW 8 PA

RESULTS OF THE SETTLING ANALYSIS

TITLE: BW8 Placement Area Capacity, Boring AM-5 Data

Initial storage results using compression settling test data:

Maximum in situ volume	1854366.62 cu yd
------------------------	------------------

Clarification results using zone settling test data:

No calculations were made.

Effluent quality results using flocculent settling test data:

No calculations were made.

Compression settling calculations for maximum in situ volume of material that can be disposed at the specified rate into a given CDF:

$$VOL = AREA * [DH - FB - (PD * \%P / 100\%)]$$

Assume a NTIME, iteratively solve for DTIME and substitute it for NTIME.

$$CEND = A * (NTIME / 2.0)^B$$

$$VOL_F = \frac{DTIME * OPHR * OPD * PRATE * CSITU * FFRAC}{7 * CEND * 100\%}$$

$$VOL_C = \frac{DTIME * OPHR * OPD * PRATE * CSITU * (100\% - FFRAC)}{7 * CSAND * 100\%}$$

$$NVOL = VOL_F + VOL_C$$

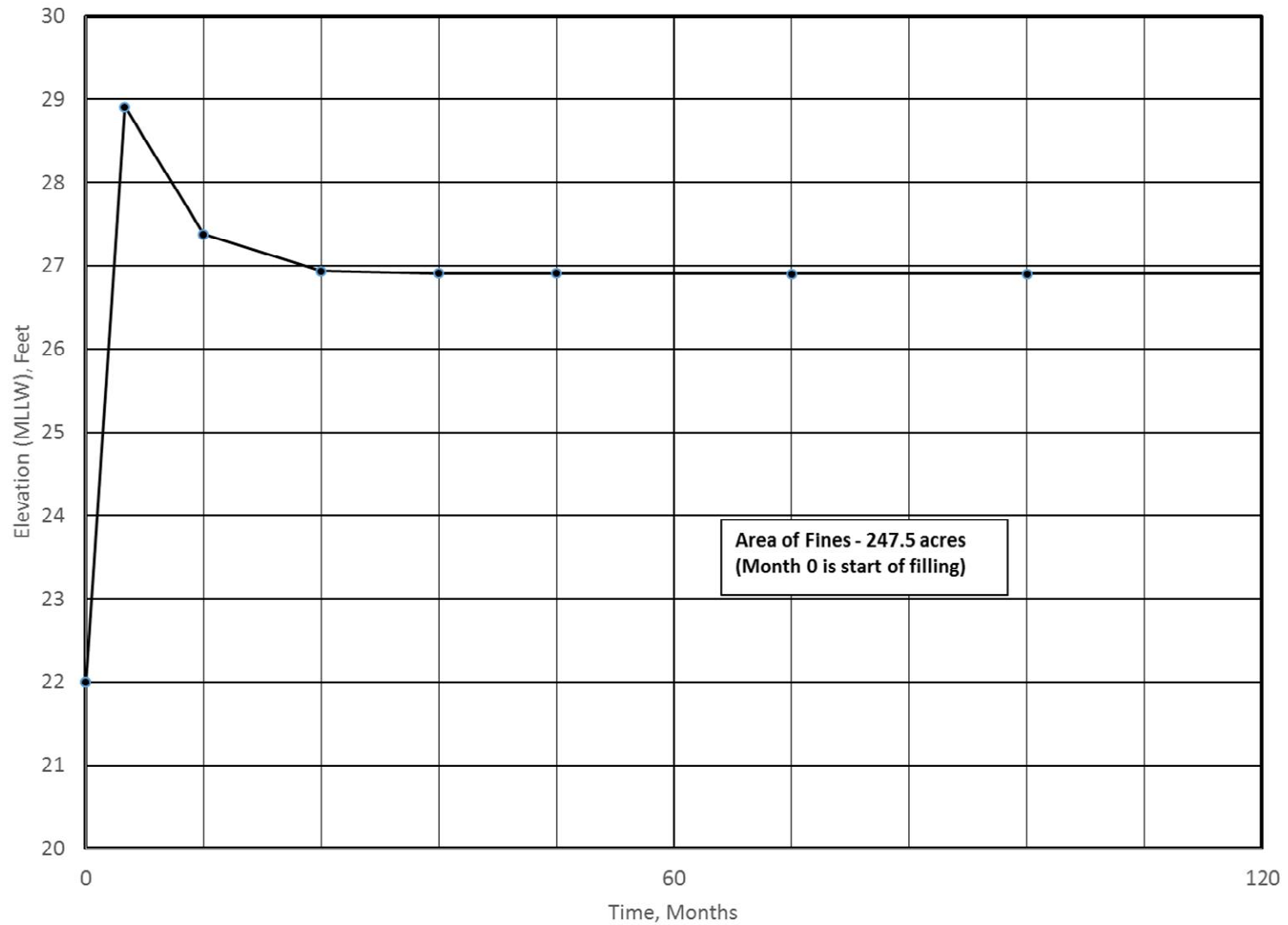
$$DTIME = \frac{VOL}{NVOL} * NTIME$$

After convergence,

$$DVOL = PRATE * DTIME * OPHR * OPD / 7$$

where

AREA = minimum area required for initial storage (acres) =	315.00
DH = average dike height or CDF depth (ft) =	10.00
FB = depth of freeboard (ft) =	2.00
PD = average depth of ponding in ponded area (ft) =	1.00
%P = percent of storage area ponded =	100.00
VOL = available storage volume (acre ft), [NVOL is used.] =	2205.00
A, B = compression settling curve coefficients =	198.17, 0.1975
DTIME = disposal period (days), [NTIME is an estimate,] =	123.67
CEND = concentration of fines at end of disposal (g/l) =	447.53
OPHR = operating hours per day of active disposal =	17.00
OPD = average number of days of operation per week =	7.00
PRATE = dredge production rate (cu yd/hr) =	882.00
CSITU = solids concentration of the in situ material (g/l) =	1223.02
FFRAC = fine-grained fraction (percent by weight) =	53.00
VOLC = volume of sands at end of disposal (cu yd) =	871787.
VOLF = volume of fines at end of disposal (cu yd) =	2686570.
CSAND = solids concentration of settled sands (g/l) =	1223.02
DVOL = in situ volume of the material (cu yd)	1854367.



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DATE: 11/25/2020

APPROVED BY:
MH

PREPARED BY:
AR

SITE CAPACITY
BELTWAY 8 PLACEMENT AREA
HOUSTON SHIP CHANNEL EXPANSION CHANNEL
IMPROVEMENT PROJECT

PROJECT NO.:

HG1910092.2.1

DRAWING NO.:

PLATE N-1

 Consolidation and desiccation of soft layers---dredged fill

Problem BW8 Settlement

*****Soil data for compressible foundation*****

Material Type	Layer Thickness	Numbers of Sub-layers	Ca/Cc	Cr/Cc
1	25.00	4	.040	.150

Material type : 1

Specific Gravity of Solids: 2.70

	Void Ratio	Effective Stress	Perm- eability	k/1+e PK	Beta	Dsde	Alpha
1	.466	.000E+00	.133E-05	.907E-06	-.619E-06	-.250E+06	-.227E+00
2	.464	.500E+03	.133E-05	.908E-06	-.116E-03	-.167E+06	-.151E+00
3	.460	.100E+04	.234E-05	.160E-05	-.328E-03	-.167E+06	-.267E+00
4	.455	.200E+04	.562E-05	.386E-05	-.175E-03	-.231E+06	-.891E+00
5	.447	.400E+04	.562E-05	.388E-05	-.269E-05	-.286E+06	-.111E+01
6	.434	.800E+04	.562E-05	.392E-05	-.274E-05	-.375E+06	-.147E+01
7	.415	.160E+05	.562E-05	.397E-05	-.277E-05	-.421E+06	-.167E+01

*****Soil data for dredged fill*****

Material Type	Specific Gravity	Ca/Cc	Cr/Cc	Saturation Limit	Disication Limit
2	2.690	.040	.150	3.400	2.500

Material type : 2

	Void	Effective	Perm-	k/1+e			
I	Ratio	Stress	ability	PK	Beta	Dsde	Alpha
1	10.000	.000E+00	.240E+00	.218E-01	.182E-02	-.150E+00	-.327E-02
2	9.000	.150E+00	.200E+00	.200E-01	.258E-02	-.200E+00	-.400E-02
3	8.000	.400E+00	.150E+00	.167E-01	.437E-02	-.275E+00	-.458E-02
4	7.000	.700E+00	.900E-01	.113E-01	.448E-02	-.550E+00	-.619E-02
5	6.000	.150E+01	.540E-01	.771E-02	.313E-02	-.165E+01	-.127E-01
6	5.000	.400E+01	.300E-01	.500E-02	.367E-02	-.143E+02	-.712E-01
7	4.000	.300E+02	.190E-02	.380E-03	.247E-02	-.198E+03	-.752E-01
8	3.000	.400E+03	.200E-03	.500E-04	.188E-03	-.249E+04	-.124E+00
9	2.000	.500E+04	.100E-04	.333E-05	.467E-04	-.460E+04	-.153E-01

Summary of lifts and print detail

Time	Material	Fill	# Sub-	Void	Start	Dessic.	Print
days	Type	Height	layers	ratio	Day	Month	detai
0.	2	8.1	50	6.00	180.	1	1
120.					180.	1	1
365.					180.	1	1
730.					180.	1	1
1095.					180.	1	1
1460.					180.	1	1
2190.					180.	1	2
2920.					180.	1	2
3650.					180.	1	2
8760.					180.	1	2

Summary of monthly rainfall and evaporation potential

Month	Rainfall	Evaporation
1	.250	.340
2	.200	.330
3	.180	.470

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4	.220	.580
5	.280	.670
6	.290	.800
7	.310	.780
8	.370	.800
9	.490	.600
10	.220	.520
11	.270	.350
12	.300	.280

*****Calculation data*****

tau	Lower layer Void ratio	Lower layer Permeability	drainage path Length
.134	.900	.10000E-01	z = 2.77

Summary of desiccation parameters

Parameter	Value
Surface Drainage Efficiency	.70
maximum evaporation efficiency	.50
saturation at desiccation limit	.50
maximum crust thickness	1.50
time to desic. after initial fill	180.00
month of initial desiccation	1
elevation of fixed water table	-10.00
elevation of top of incompres. found.	-3.00

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*****Initial Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
25.00	25.00	17.11	.47	.47	.47	1
18.73	18.73	12.83	.46	.46	.46	1
12.48	12.48	8.56	.46	.46	.46	1
6.23	6.23	4.28	.46	.46	.46	1
.00	.00	.00	.46	.46	.46	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	
Material						
25.00	633.50	.00	633.50	510.30	123.20	1
18.73	1486.56	458.14	1028.43	905.23	123.20	1
12.48	2338.78	916.27	1422.51	1299.31	123.20	1
6.23	3190.19	1374.40	1815.79	1692.59	123.20	1
.00	4040.97	1832.53	2208.43	2085.23	123.20	1

Time = 0. Degree of Consolidation = 0.0%

Total Settlement = .000

Settlement at End of Primary Consolidation = .012

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

*****Initial Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
8.10	8.10	1.16	6.00	6.00	10.00	2
7.94	7.94	1.13	6.00	6.00	5.61	2
7.78	7.78	1.11	6.00	6.00	4.96	2
7.61	7.61	1.09	6.00	6.00	4.87	2

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7.45	7.45	1.06	6.00	6.00	4.77	2
7.29	7.29	1.04	6.00	6.00	4.68	2
7.13	7.13	1.02	6.00	6.00	4.59	2
6.97	6.97	1.00	6.00	6.00	4.49	2
6.80	6.80	.97	6.00	6.00	4.40	2
6.64	6.64	.95	6.00	6.00	4.30	2
6.48	6.48	.93	6.00	6.00	4.21	2
6.32	6.32	.90	6.00	6.00	4.11	2
6.16	6.16	.88	6.00	6.00	4.02	2
5.99	5.99	.86	6.00	6.00	3.99	2
5.83	5.83	.83	6.00	6.00	3.99	2
5.67	5.67	.81	6.00	6.00	3.98	2
5.51	5.51	.79	6.00	6.00	3.97	2
5.35	5.35	.76	6.00	6.00	3.97	2
5.18	5.18	.74	6.00	6.00	3.96	2
5.02	5.02	.72	6.00	6.00	3.95	2
4.86	4.86	.69	6.00	6.00	3.95	2
4.70	4.70	.67	6.00	6.00	3.94	2
4.54	4.54	.65	6.00	6.00	3.93	2
4.37	4.37	.62	6.00	6.00	3.93	2
4.21	4.21	.60	6.00	6.00	3.92	2
4.05	4.05	.58	6.00	6.00	3.91	2
3.89	3.89	.56	6.00	6.00	3.91	2
3.73	3.73	.53	6.00	6.00	3.90	2
3.56	3.56	.51	6.00	6.00	3.89	2
3.40	3.40	.49	6.00	6.00	3.89	2
3.24	3.24	.46	6.00	6.00	3.88	2
3.08	3.08	.44	6.00	6.00	3.87	2
2.92	2.92	.42	6.00	6.00	3.87	2
2.75	2.75	.39	6.00	6.00	3.86	2
2.59	2.59	.37	6.00	6.00	3.85	2
2.43	2.43	.35	6.00	6.00	3.85	2
2.27	2.27	.32	6.00	6.00	3.84	2
2.11	2.11	.30	6.00	6.00	3.83	2
1.94	1.94	.28	6.00	6.00	3.83	2
1.78	1.78	.25	6.00	6.00	3.82	2
1.62	1.62	.23	6.00	6.00	3.81	2
1.46	1.46	.21	6.00	6.00	3.81	2
1.30	1.30	.19	6.00	6.00	3.80	2
1.13	1.13	.16	6.00	6.00	3.79	2
.97	.97	.14	6.00	6.00	3.79	2
.81	.81	.12	6.00	6.00	3.78	2
.65	.65	.09	6.00	6.00	3.77	2
.49	.49	.07	6.00	6.00	3.77	2
.32	.32	.05	6.00	6.00	3.76	2
.16	.16	.02	6.00	6.00	3.75	2
.00	.00	.00	6.00	6.00	3.75	2

***** Stresses *****

***** Pore Pressures *****

		BW8FINM.PSO				
XI	Total	Effective	Total	Static	Excess	
Material						
8.10	.00	.00	.00	.00	.00	2
7.94	12.67	.00	12.67	10.21	2.46	2
7.78	25.34	.00	25.34	20.41	4.93	2
7.61	38.01	.00	38.01	30.62	7.39	2
7.45	50.68	.00	50.68	40.82	9.86	2
7.29	63.35	.00	63.35	51.03	12.32	2
7.13	76.02	.00	76.02	61.24	14.78	2
6.97	88.69	.00	88.69	71.44	17.25	2
6.80	101.36	.00	101.36	81.65	19.71	2
6.64	114.03	.00	114.03	91.85	22.18	2
6.48	126.70	.00	126.70	102.06	24.64	2
6.32	139.37	.00	139.37	112.27	27.10	2
6.16	152.04	.00	152.04	122.47	29.57	2
5.99	164.71	.00	164.71	132.68	32.03	2
5.83	177.38	.00	177.38	142.88	34.50	2
5.67	190.05	.00	190.05	153.09	36.96	2
5.51	202.72	.00	202.72	163.30	39.42	2
5.35	215.39	.00	215.39	173.50	41.89	2
5.18	228.06	.00	228.06	183.71	44.35	2
5.02	240.73	.00	240.73	193.91	46.82	2
4.86	253.40	.00	253.40	204.12	49.28	2
4.70	266.07	.00	266.07	214.33	51.74	2
4.54	278.74	.00	278.74	224.53	54.21	2
4.37	291.41	.00	291.41	234.74	56.67	2
4.21	304.08	.00	304.08	244.94	59.14	2
4.05	316.75	.00	316.75	255.15	61.60	2
3.89	329.42	.00	329.42	265.36	64.06	2
3.73	342.09	.00	342.09	275.56	66.53	2
3.56	354.76	.00	354.76	285.77	68.99	2
3.40	367.43	.00	367.43	295.97	71.46	2
3.24	380.10	.00	380.10	306.18	73.92	2
3.08	392.77	.00	392.77	316.39	76.38	2
2.92	405.44	.00	405.44	326.59	78.85	2
2.75	418.11	.00	418.11	336.80	81.31	2
2.59	430.78	.00	430.78	347.00	83.78	2
2.43	443.45	.00	443.45	357.21	86.24	2
2.27	456.12	.00	456.12	367.42	88.70	2
2.11	468.79	.00	468.79	377.62	91.17	2
1.94	481.46	.00	481.46	387.83	93.63	2
1.78	494.13	.00	494.13	398.03	96.10	2
1.62	506.80	.00	506.80	408.24	98.56	2
1.46	519.47	.00	519.47	418.45	101.02	2
1.30	532.14	.00	532.14	428.65	103.49	2
1.13	544.81	.00	544.81	438.86	105.95	2
.97	557.48	.00	557.48	449.06	108.42	2
.81	570.15	.00	570.15	459.27	110.88	2
.65	582.82	.00	582.82	469.48	113.34	2
.49	595.49	.00	595.49	479.68	115.81	2
.32	608.16	.00	608.16	489.89	118.27	2

			BW8FINM.PSO			
.16	620.83	.00	620.83	500.09	120.74	2
.00	633.50	.00	633.50	510.30	123.20	2

Time = 0. Degree of Consolidation = 0.0%

Total Settlement = .000

Settlement at End of Primary Consolidation = 2.207

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
25.00	25.00	17.11	.47	.47	.47	1
18.73	18.73	12.83	.46	.46	.46	1
12.48	12.47	8.56	.46	.46	.46	1
6.23	6.23	4.28	.46	.46	.46	1
.00	.00	.00	.46	.46	.46	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	
Material						
25.00	558.37	26.72	531.65	435.17	96.48	1
18.73	1411.42	464.79	946.63	830.09	116.55	1
12.47	2263.63	916.27	1347.36	1224.16	123.20	1
6.23	3115.04	1388.16	1726.87	1617.44	109.44	1
.00	3965.74	1955.74	2010.00	2010.00	.00	1

Time = 120. Degree of Consolidation = 13.0%

Total Settlement = .002

Settlement at End of Primary Consolidation = .012

Settlement caused by Primary Consolidation at time 120. = .002

Settlement caused by Secondary Compression at time 120. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
8.10	6.91	1.16	6.00	6.00	10.00	2
7.94	6.75	1.13	6.00	5.87	5.61	2
7.78	6.59	1.11	6.00	5.80	4.96	2
7.61	6.43	1.09	6.00	5.75	4.87	2
7.45	6.28	1.06	6.00	5.70	4.77	2
7.29	6.12	1.04	6.00	5.66	4.68	2
7.13	5.97	1.02	6.00	5.62	4.59	2
6.97	5.82	1.00	6.00	5.58	4.49	2
6.80	5.66	.97	6.00	5.54	4.40	2
6.64	5.51	.95	6.00	5.51	4.30	2
6.48	5.36	.93	6.00	5.47	4.21	2
6.32	5.21	.90	6.00	5.43	4.11	2
6.16	5.06	.88	6.00	5.39	4.02	2
5.99	4.92	.86	6.00	5.35	3.99	2
5.83	4.77	.83	6.00	5.32	3.99	2
5.67	4.62	.81	6.00	5.28	3.98	2
5.51	4.48	.79	6.00	5.25	3.97	2
5.35	4.34	.76	6.00	5.21	3.97	2
5.18	4.19	.74	6.00	5.18	3.96	2
5.02	4.05	.72	6.00	5.14	3.95	2
4.86	3.91	.69	6.00	5.11	3.95	2
4.70	3.77	.67	6.00	5.08	3.94	2
4.54	3.63	.65	6.00	5.04	3.93	2
4.37	3.49	.62	6.00	5.01	3.93	2
4.21	3.35	.60	6.00	4.98	3.92	2
4.05	3.21	.58	6.00	4.95	3.91	2
3.89	3.07	.56	6.00	4.92	3.91	2
3.73	2.94	.53	6.00	4.89	3.90	2
3.56	2.80	.51	6.00	4.86	3.89	2
3.40	2.67	.49	6.00	4.83	3.89	2
3.24	2.53	.46	6.00	4.79	3.88	2
3.08	2.40	.44	6.00	4.76	3.87	2
2.92	2.26	.42	6.00	4.73	3.87	2
2.75	2.13	.39	6.00	4.70	3.86	2
2.59	2.00	.37	6.00	4.67	3.85	2
2.43	1.87	.35	6.00	4.64	3.85	2
2.27	1.74	.32	6.00	4.60	3.84	2
2.11	1.61	.30	6.00	4.57	3.83	2
1.94	1.48	.28	6.00	4.54	3.83	2
1.78	1.35	.25	6.00	4.51	3.82	2

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1.62	1.23	.23	6.00	4.47	3.81	2
1.46	1.10	.21	6.00	4.44	3.81	2
1.30	.98	.19	6.00	4.41	3.80	2
1.13	.85	.16	6.00	4.37	3.79	2
.97	.73	.14	6.00	4.34	3.79	2
.81	.60	.12	6.00	4.30	3.78	2
.65	.48	.09	6.00	4.27	3.77	2
.49	.36	.07	6.00	4.23	3.77	2
.32	.24	.05	6.00	4.20	3.76	2
.16	.12	.02	6.00	4.16	3.75	2
.00	.00	.00	6.00	4.13	3.75	2

***** Stresses *****

***** Pore Pressures *****

XI Material	Total	Effective	Total	Static	Excess	
6.91	.00	.00	.00	.00	.00	2
6.75	12.57	1.82	10.75	10.10	.64	2
6.59	24.99	2.00	23.00	20.07	2.93	2
6.43	37.34	2.13	35.21	29.94	5.26	2
6.28	49.61	2.24	47.37	39.75	7.62	2
6.12	61.81	2.34	59.47	49.49	9.98	2
5.97	73.96	2.44	71.52	59.18	12.34	2
5.82	86.05	2.54	83.51	68.81	14.71	2
5.66	98.09	2.64	95.45	78.38	17.07	2
5.51	110.06	2.74	107.33	87.89	19.44	2
5.36	121.99	2.83	119.15	97.35	21.81	2
5.21	133.85	2.93	130.92	106.75	24.18	2
5.06	145.66	3.02	142.64	116.09	26.55	2
4.92	157.42	3.11	154.30	125.39	28.92	2
4.77	169.12	3.21	165.91	134.62	31.29	2
4.62	180.77	3.30	177.47	143.81	33.66	2
4.48	192.37	3.39	188.98	152.94	36.04	2
4.34	203.91	3.47	200.44	162.02	38.41	2
4.19	215.40	3.56	211.84	171.05	40.79	2
4.05	226.85	3.65	223.20	180.03	43.17	2
3.91	238.24	3.73	234.51	188.96	45.55	2
3.77	249.59	3.81	245.78	197.84	47.93	2
3.63	260.89	3.89	257.00	206.68	50.32	2
3.49	272.14	3.97	268.17	215.47	52.70	2
3.35	283.35	4.49	278.86	224.21	54.65	2
3.21	294.51	5.29	289.22	232.91	56.31	2
3.07	305.63	6.10	299.53	241.56	57.97	2
2.94	316.70	6.91	309.79	250.17	59.62	2
2.80	327.72	7.72	320.01	258.73	61.28	2
2.67	338.70	8.53	330.17	267.25	62.93	2
2.53	349.64	9.35	340.29	275.72	64.57	2
2.40	360.53	10.17	350.36	284.14	66.22	2
2.26	371.37	10.99	360.38	292.52	67.86	2
2.13	382.17	11.82	370.35	300.86	69.50	2

BW8FINM.PSO						
2.00	392.92	12.65	380.27	309.14	71.13	2
1.87	403.62	13.48	390.14	317.38	72.76	2
1.74	414.28	14.32	399.96	325.57	74.38	2
1.61	424.89	15.17	409.72	333.72	76.00	2
1.48	435.45	16.01	419.44	341.82	77.62	2
1.35	445.97	16.87	429.10	349.87	79.23	2
1.23	456.43	17.73	438.70	357.87	80.83	2
1.10	466.85	18.59	448.25	365.82	82.43	2
.98	477.22	19.47	457.75	373.73	84.02	2
.85	487.54	20.35	467.19	381.59	85.61	2
.73	497.81	21.23	476.58	389.39	87.19	2
.60	508.03	22.12	485.91	397.15	88.76	2
.48	518.20	23.03	495.18	404.86	90.32	2
.36	528.32	23.93	504.39	412.51	91.87	2
.24	538.39	24.85	513.54	420.12	93.42	2
.12	548.41	25.78	522.63	427.67	94.96	2
.00	558.37	26.72	531.65	435.17	96.49	2

Time = 120. Degree of Consolidation = 54.%

Total Settlement = 1.193

Settlement at End of Primary Consolidation = 2.207

Settlement caused by Primary Consolidation at time 120. = 1.193

Settlement caused by Secondary Compression at time 120. = .000

Surface Elevation = 28.91

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
25.00	25.00	17.11	.47	.47	.47	1
18.73	18.73	12.83	.46	.46	.46	1
12.48	12.47	8.56	.46	.46	.46	1
6.23	6.23	4.28	.46	.46	.46	1
.00	.00	.00	.46	.46	.46	1

***** Stresses *****			***** Pore Pressures *****		
XI	Total	Effective	Total	Static	Excess

BW8FINM.PSO

Material

25.00	468.25	76.78	391.47	298.08	93.40	1
18.73	1321.27	478.37	842.89	692.96	149.94	1
12.47	2173.47	916.27	1257.20	1087.03	170.18	1
6.23	3024.87	1409.90	1614.97	1480.29	134.68	1
.00	3875.53	1983.00	1892.53	1872.82	19.71	1

Time = 365. Degree of Consolidation = 20.0%

Total Settlement = .003

Settlement at End of Primary Consolidation = .015

Settlement caused by Primary Consolidation at time 365. = .003

Settlement caused by Secondary Compression at time 365. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

Material	A	XI	Z	Einitial	E	Eeop	
	8.10	5.38	1.16	6.00	2.50	2.50	2
	7.94	5.30	1.13	6.00	2.50	2.50	2
	7.78	5.22	1.11	6.00	2.50	2.50	2
	7.61	5.14	1.09	6.00	2.50	2.50	2
	7.45	5.06	1.06	6.00	2.50	2.50	2
	7.29	4.98	1.04	6.00	2.50	2.50	2
	7.13	4.90	1.02	6.00	2.50	2.50	2
	6.97	4.82	1.00	6.00	2.50	2.50	2
	6.80	4.73	.97	6.00	3.17	3.95	2
	6.64	4.63	.95	6.00	3.40	3.95	2
	6.48	4.53	.93	6.00	3.40	3.94	2
	6.32	4.43	.90	6.00	3.40	3.93	2
	6.16	4.33	.88	6.00	3.40	3.93	2
	5.99	4.22	.86	6.00	3.40	3.92	2
	5.83	4.12	.83	6.00	3.40	3.91	2
	5.67	4.01	.81	6.00	3.93	3.91	2
	5.51	3.90	.79	6.00	3.94	3.90	2
	5.35	3.78	.76	6.00	3.95	3.89	2
	5.18	3.67	.74	6.00	3.96	3.89	2
	5.02	3.55	.72	6.00	3.97	3.88	2
	4.86	3.44	.69	6.00	3.98	3.87	2
	4.70	3.32	.67	6.00	3.98	3.87	2
	4.54	3.21	.65	6.00	3.99	3.86	2

BW8FINM.PSO

4.37	3.09	.62	6.00	3.99	3.85	2
4.21	2.98	.60	6.00	3.99	3.85	2
4.05	2.86	.58	6.00	3.99	3.84	2
3.89	2.75	.56	6.00	3.99	3.83	2
3.73	2.63	.53	6.00	3.99	3.83	2
3.56	2.51	.51	6.00	3.99	3.82	2
3.40	2.40	.49	6.00	3.99	3.81	2
3.24	2.28	.46	6.00	3.99	3.81	2
3.08	2.17	.44	6.00	3.98	3.80	2
2.92	2.05	.42	6.00	3.98	3.79	2
2.75	1.94	.39	6.00	3.97	3.79	2
2.59	1.82	.37	6.00	3.97	3.78	2
2.43	1.71	.35	6.00	3.96	3.77	2
2.27	1.59	.32	6.00	3.96	3.77	2
2.11	1.48	.30	6.00	3.95	3.76	2
1.94	1.36	.28	6.00	3.95	3.75	2
1.78	1.25	.25	6.00	3.94	3.75	2
1.62	1.14	.23	6.00	3.94	3.74	2
1.46	1.02	.21	6.00	3.93	3.73	2
1.30	.91	.19	6.00	3.92	3.73	2
1.13	.79	.16	6.00	3.92	3.72	2
.97	.68	.14	6.00	3.91	3.71	2
.81	.57	.12	6.00	3.91	3.71	2
.65	.45	.09	6.00	3.90	3.70	2
.49	.34	.07	6.00	3.89	3.69	2
.32	.23	.05	6.00	3.89	3.69	2
.16	.11	.02	6.00	3.88	3.68	2
.00	.00	.00	6.00	3.87	3.67	2

***** Stresses *****

***** Pore Pressures *****

XI Material	Total	Effective	Total	Static	Excess	
5.38	.00	.00	.00	.00	.00	2
5.30	5.74	5.74	.00	.00	.00	2
5.22	11.49	11.49	.00	.00	.00	2
5.14	17.23	17.23	.00	.00	.00	2
5.06	22.98	22.98	.00	.00	.00	2
4.98	28.72	28.72	.00	.00	.00	2
4.90	34.47	34.47	.00	.00	.00	2
4.82	40.21	40.21	.00	.00	.00	2
4.73	46.98	46.98	.00	.00	.00	2
4.63	55.75	49.44	6.31	6.31	.00	2
4.53	64.62	51.90	12.72	12.72	.00	2
4.43	73.50	54.37	19.14	19.14	.00	2
4.33	82.38	56.83	25.55	25.55	.00	2
4.22	91.39	59.30	32.09	32.09	.00	2
4.12	100.14	61.76	38.38	38.38	.00	2
4.01	109.53	56.53	53.00	45.31	7.69	2
3.90	119.19	51.73	67.46	52.50	14.96	2

BW8FINM.PSO

3.78	128.87	47.43	81.43	59.71	21.72	2
3.67	138.56	43.69	94.87	66.94	27.92	2
3.55	148.27	40.53	107.73	74.19	33.55	2
3.44	157.98	37.95	120.04	81.44	38.60	2
3.32	167.71	35.91	131.80	88.70	43.10	2
3.21	177.45	34.39	143.06	95.97	47.08	2
3.09	187.18	33.33	153.85	103.25	50.61	2
2.98	196.93	32.69	164.23	110.53	53.71	2
2.86	206.67	32.43	174.24	117.81	56.44	2
2.75	216.41	32.49	183.92	125.09	58.84	2
2.63	226.16	32.85	193.30	132.37	60.94	2
2.51	235.90	33.48	202.42	139.64	62.78	2
2.40	245.64	34.34	211.30	146.92	64.38	2
2.28	255.37	35.41	219.96	154.19	65.77	2
2.17	265.10	36.67	228.43	161.46	66.97	2
2.05	274.83	38.10	236.73	168.72	68.01	2
1.94	284.55	39.68	244.87	175.97	68.90	2
1.82	294.26	41.38	252.88	183.22	69.66	2
1.71	303.97	43.19	260.77	190.46	70.31	2
1.59	313.66	45.11	268.56	197.70	70.86	2
1.48	323.35	47.10	276.25	204.92	71.33	2
1.36	333.04	49.17	283.87	212.14	71.72	2
1.25	342.71	51.30	291.41	219.35	72.06	2
1.14	352.38	53.48	298.90	226.55	72.35	2
1.02	362.03	55.70	306.33	233.75	72.59	2
.91	371.68	57.96	313.73	240.93	72.80	2
.79	381.32	60.24	321.08	248.11	72.97	2
.68	390.95	62.55	328.40	255.27	73.13	2
.57	400.57	64.88	335.69	262.43	73.26	2
.45	410.19	67.23	342.95	269.58	73.37	2
.34	419.79	69.60	350.19	276.72	73.47	2
.23	429.38	71.98	357.40	283.84	73.56	2
.11	438.97	74.37	364.59	290.96	73.63	2
.00	448.54	76.78	371.76	298.08	73.69	2

Time = 365. Degree of Consolidation = 76.%

Total Settlement = 2.715

Settlement at End of Primary Consolidation = 2.761

Settlement caused by Primary Consolidation at time 365. = 2.105

Settlement caused by Secondary Compression at time 365. = .000

Settlement Due to Desiccation = .610

Surface Elevation = 27.38

BW8FINM.PSO

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
25.00	24.99	17.11	.47	.47	.47	1
18.73	18.73	12.83	.46	.46	.46	1
12.48	12.47	8.56	.46	.46	.46	1
6.23	6.23	4.28	.46	.46	.46	1
.00	.00	.00	.46	.45	.45	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	
Material						
24.99	447.01	183.84	263.18	218.82	44.35	1
18.73	1299.96	498.60	801.36	613.64	187.72	1
12.47	2152.17	916.27	1235.90	1007.71	228.19	1
6.23	3003.54	1447.12	1556.41	1400.95	155.47	1
.00	3854.15	2016.37	1837.78	1793.42	44.36	1

Time = 730. Degree of Consolidation = 29.%

Total Settlement = .005

Settlement at End of Primary Consolidation = .018

Settlement caused by Primary Consolidation at time 730. = .005

Settlement caused by Secondary Compression at time 730. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
8.10	4.94	1.16	6.00	2.50	2.50	2
7.94	4.86	1.13	6.00	2.50	2.50	2
7.78	4.78	1.11	6.00	2.50	2.50	2
7.61	4.70	1.09	6.00	2.50	2.50	2

BW8FINM.PSO

7.45	4.62	1.06	6.00	2.50	2.50	2
7.29	4.54	1.04	6.00	2.50	2.50	2
7.13	4.45	1.02	6.00	2.50	2.50	2
6.97	4.37	1.00	6.00	2.50	2.50	2
6.80	4.29	.97	6.00	2.50	2.50	2
6.64	4.21	.95	6.00	2.50	2.50	2
6.48	4.13	.93	6.00	2.50	2.50	2
6.32	4.05	.90	6.00	2.50	2.50	2
6.16	3.97	.88	6.00	2.50	2.50	2
5.99	3.89	.86	6.00	2.50	2.50	2
5.83	3.81	.83	6.00	2.50	2.50	2
5.67	3.73	.81	6.00	2.50	2.50	2
5.51	3.64	.79	6.00	2.50	2.50	2
5.35	3.57	.76	6.00	2.50	2.50	2
5.18	3.47	.74	6.00	3.74	3.80	2
5.02	3.36	.72	6.00	3.79	3.79	2
4.86	3.25	.69	6.00	3.78	3.78	2
4.70	3.14	.67	6.00	3.78	3.78	2
4.54	3.03	.65	6.00	3.77	3.77	2
4.37	2.92	.62	6.00	3.76	3.76	2
4.21	2.81	.60	6.00	3.76	3.76	2
4.05	2.70	.58	6.00	3.75	3.75	2
3.89	2.59	.56	6.00	3.74	3.74	2
3.73	2.48	.53	6.00	3.74	3.74	2
3.56	2.37	.51	6.00	3.73	3.73	2
3.40	2.26	.49	6.00	3.72	3.72	2
3.24	2.15	.46	6.00	3.72	3.72	2
3.08	2.04	.44	6.00	3.71	3.71	2
2.92	1.93	.42	6.00	3.70	3.70	2
2.75	1.83	.39	6.00	3.70	3.70	2
2.59	1.72	.37	6.00	3.69	3.69	2
2.43	1.61	.35	6.00	3.68	3.68	2
2.27	1.50	.32	6.00	3.68	3.68	2
2.11	1.39	.30	6.00	3.67	3.67	2
1.94	1.28	.28	6.00	3.66	3.66	2
1.78	1.18	.25	6.00	3.66	3.66	2
1.62	1.07	.23	6.00	3.65	3.65	2
1.46	.96	.21	6.00	3.64	3.64	2
1.30	.85	.19	6.00	3.64	3.64	2
1.13	.75	.16	6.00	3.63	3.63	2
.97	.64	.14	6.00	3.62	3.62	2
.81	.53	.12	6.00	3.62	3.62	2
.65	.43	.09	6.00	3.61	3.61	2
.49	.32	.07	6.00	3.60	3.60	2
.32	.21	.05	6.00	3.60	3.60	2
.16	.11	.02	6.00	3.59	3.59	2
.00	.00	.00	6.00	3.58	3.58	2

***** Stresses *****

***** Pore Pressures *****

		BW8FINM.PSO				
XI	Total	Effective	Total	Static	Excess	
Material						
4.94	.00	.00	.00	.00	.00	2
4.86	5.74	5.74	.00	.00	.00	2
4.78	11.49	11.49	.00	.00	.00	2
4.70	17.23	17.23	.00	.00	.00	2
4.62	22.98	22.98	.00	.00	.00	2
4.54	28.72	28.72	.00	.00	.00	2
4.45	34.47	34.47	.00	.00	.00	2
4.37	40.21	40.21	.00	.00	.00	2
4.29	45.96	45.96	.00	.00	.00	2
4.21	51.70	51.70	.00	.00	.00	2
4.13	57.45	57.45	.00	.00	.00	2
4.05	63.19	63.19	.00	.00	.00	2
3.97	68.93	68.93	.00	.00	.00	2
3.89	74.68	74.68	.00	.00	.00	2
3.81	80.42	80.42	.00	.00	.00	2
3.73	86.17	86.17	.00	.00	.00	2
3.64	91.91	91.91	.00	.00	.00	2
3.57	97.66	97.66	.00	.00	.00	2
3.47	104.99	104.99	.00	.00	.00	2
3.36	114.41	107.45	6.96	6.96	.00	2
3.25	123.86	109.92	13.94	13.94	.00	2
3.14	133.29	112.38	20.91	20.91	.00	2
3.03	142.72	114.85	27.87	27.87	.00	2
2.92	152.13	117.31	34.82	34.82	.00	2
2.81	161.54	119.77	41.76	41.76	.00	2
2.70	170.93	122.24	48.69	48.69	.00	2
2.59	180.32	124.70	55.62	55.62	.00	2
2.48	189.69	127.17	62.53	62.53	.00	2
2.37	199.06	129.63	69.43	69.43	.00	2
2.26	208.42	132.09	76.32	76.32	.00	2
2.15	217.76	134.56	83.21	83.21	.00	2
2.04	227.10	137.02	90.08	90.08	.00	2
1.93	236.43	139.49	96.94	96.94	.00	2
1.83	245.75	141.95	103.80	103.80	.00	2
1.72	255.05	144.41	110.64	110.64	.00	2
1.61	264.35	146.88	117.47	117.47	.00	2
1.50	273.64	149.34	124.30	124.30	.00	2
1.39	282.92	151.81	131.11	131.11	.00	2
1.28	292.19	154.27	137.92	137.92	.00	2
1.18	301.45	156.73	144.71	144.71	.00	2
1.07	310.70	159.20	151.50	151.50	.00	2
.96	319.94	161.66	158.28	158.28	.00	2
.85	329.17	164.13	165.04	165.04	.00	2
.75	338.39	166.59	171.80	171.80	.00	2
.64	347.60	169.05	178.55	178.55	.00	2
.53	356.80	171.52	185.28	185.28	.00	2
.43	365.99	173.98	192.01	192.01	.00	2
.32	375.17	176.45	198.73	198.73	.00	2
.21	384.35	178.91	205.44	205.44	.00	2

			BW8FINM.PSO			
.11	393.51	181.37	212.14	212.13	.00	2
.00	402.66	183.84	218.82	218.82	.00	2

Time = 730. Degree of Consolidation = 73.0%

Total Settlement = 3.159

Settlement at End of Primary Consolidation = 3.158

Settlement caused by Primary Consolidation at time 730. = 2.310

Settlement caused by Secondary Compression at time 730. = .000

Settlement Due to Desiccation = .849

Surface Elevation = 26.94

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****		
A	XI	Z	Einitial	E	Eeop
Material					
25.00	24.99	17.11	.47	.47	.47
18.73	18.73	12.83	.46	.46	.46
12.48	12.47	8.56	.46	.46	.46
6.23	6.23	4.28	.46	.46	.46
.00	.00	.00	.46	.45	.45

***** Stresses *****			***** Pore Pressures *****		
XI	Total	Effective	Total	Static	Excess
Material					
24.99	445.42	187.14	258.28	211.46	46.82
18.73	1298.34	509.42	788.93	606.25	182.68
12.47	2150.54	922.32	1228.22	1000.31	227.91
6.23	3001.88	1479.50	1522.38	1393.52	128.86
.00	3852.46	2019.68	1832.77	1785.96	46.81

Time = 1095. Degree of Consolidation = 37.0%

Total Settlement = .007

Settlement at End of Primary Consolidation = .019

BW8FINM.PSO

Settlement caused by Primary Consolidation at time 1095. = .007

Settlement caused by Secondary Compression at time 1095. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
8.10	4.92	1.16	6.00	2.50	2.50	2
7.94	4.83	1.13	6.00	2.50	2.50	2
7.78	4.75	1.11	6.00	2.50	2.50	2
7.61	4.67	1.09	6.00	2.50	2.50	2
7.45	4.59	1.06	6.00	2.50	2.50	2
7.29	4.51	1.04	6.00	2.50	2.50	2
7.13	4.43	1.02	6.00	2.50	2.50	2
6.97	4.35	1.00	6.00	2.50	2.50	2
6.80	4.27	.97	6.00	2.50	2.50	2
6.64	4.19	.95	6.00	2.50	2.50	2
6.48	4.11	.93	6.00	2.50	2.50	2
6.32	4.02	.90	6.00	2.50	2.50	2
6.16	3.94	.88	6.00	2.50	2.50	2
5.99	3.86	.86	6.00	2.50	2.50	2
5.83	3.78	.83	6.00	2.50	2.50	2
5.67	3.70	.81	6.00	2.50	2.50	2
5.51	3.62	.79	6.00	2.50	2.50	2
5.35	3.53	.76	6.00	2.50	2.50	2
5.18	3.46	.74	6.00	2.50	2.50	2
5.02	3.36	.72	6.00	3.78	3.78	2
4.86	3.25	.69	6.00	3.78	3.78	2
4.70	3.14	.67	6.00	3.77	3.77	2
4.54	3.03	.65	6.00	3.76	3.76	2
4.37	2.92	.62	6.00	3.76	3.76	2
4.21	2.81	.60	6.00	3.75	3.75	2
4.05	2.70	.58	6.00	3.74	3.74	2
3.89	2.59	.56	6.00	3.74	3.74	2
3.73	2.48	.53	6.00	3.73	3.73	2
3.56	2.37	.51	6.00	3.72	3.72	2
3.40	2.26	.49	6.00	3.72	3.72	2
3.24	2.15	.46	6.00	3.71	3.71	2
3.08	2.04	.44	6.00	3.70	3.70	2
2.92	1.93	.42	6.00	3.70	3.70	2
2.75	1.82	.39	6.00	3.69	3.69	2
2.59	1.71	.37	6.00	3.68	3.68	2
2.43	1.61	.35	6.00	3.68	3.68	2

BW8FINM.PSO

2.27	1.50	.32	6.00	3.67	3.67	2
2.11	1.39	.30	6.00	3.66	3.66	2
1.94	1.28	.28	6.00	3.66	3.66	2
1.78	1.17	.25	6.00	3.65	3.65	2
1.62	1.07	.23	6.00	3.64	3.64	2
1.46	.96	.21	6.00	3.64	3.64	2
1.30	.85	.19	6.00	3.63	3.63	2
1.13	.74	.16	6.00	3.62	3.62	2
.97	.64	.14	6.00	3.62	3.62	2
.81	.53	.12	6.00	3.61	3.61	2
.65	.42	.09	6.00	3.60	3.60	2
.49	.32	.07	6.00	3.60	3.60	2
.32	.21	.05	6.00	3.59	3.59	2
.16	.11	.02	6.00	3.58	3.58	2
.00	.00	.00	6.00	3.58	3.58	2

***** Stresses *****

***** Pore Pressures *****

XI Material	Total	Effective	Total	Static	Excess	
4.92	.00	.00	.00	.00	.00	2
4.83	5.74	5.74	.00	.00	.00	2
4.75	11.49	11.49	.00	.00	.00	2
4.67	17.23	17.23	.00	.00	.00	2
4.59	22.98	22.98	.00	.00	.00	2
4.51	28.72	28.72	.00	.00	.00	2
4.43	34.47	34.47	.00	.00	.00	2
4.35	40.21	40.21	.00	.00	.00	2
4.27	45.96	45.96	.00	.00	.00	2
4.19	51.70	51.70	.00	.00	.00	2
4.11	57.45	57.45	.00	.00	.00	2
4.02	63.19	63.19	.00	.00	.00	2
3.94	68.93	68.93	.00	.00	.00	2
3.86	74.68	74.68	.00	.00	.00	2
3.78	80.42	80.42	.00	.00	.00	2
3.70	86.17	86.17	.00	.00	.00	2
3.62	91.91	91.91	.00	.00	.00	2
3.53	97.66	97.66	.00	.00	.00	2
3.46	103.40	103.40	.00	.00	.00	2
3.36	110.76	110.76	.00	.00	.00	2
3.25	120.19	113.23	6.97	6.97	.00	2
3.14	129.61	115.69	13.92	13.92	.00	2
3.03	139.03	118.15	20.87	20.87	.00	2
2.92	148.43	120.62	27.81	27.81	.00	2
2.81	157.82	123.08	34.74	34.74	.00	2
2.70	167.20	125.55	41.66	41.66	.00	2
2.59	176.58	128.01	48.56	48.56	.00	2
2.48	185.94	130.47	55.46	55.46	.00	2
2.37	195.29	132.94	62.35	62.35	.00	2
2.26	204.64	135.40	69.23	69.23	.00	2

BW8FINM.PSO

2.15	213.97	137.87	76.10	76.10	.00	2
2.04	223.29	140.33	82.96	82.96	.00	2
1.93	232.61	142.80	89.81	89.81	.00	2
1.82	241.91	145.26	96.65	96.65	.00	2
1.71	251.21	147.72	103.48	103.48	.00	2
1.61	260.49	150.19	110.31	110.31	.00	2
1.50	269.77	152.65	117.12	117.12	.00	2
1.39	279.03	155.12	123.92	123.92	.00	2
1.28	288.29	157.58	130.71	130.71	.00	2
1.17	297.54	160.04	137.49	137.49	.00	2
1.07	306.77	162.51	144.27	144.27	.00	2
.96	316.00	164.97	151.03	151.03	.00	2
.85	325.22	167.44	157.78	157.78	.00	2
.74	334.42	169.90	164.53	164.53	.00	2
.64	343.62	172.36	171.26	171.26	.00	2
.53	352.81	174.83	177.98	177.98	.00	2
.42	361.99	177.29	184.70	184.70	.00	2
.32	371.16	179.76	191.40	191.40	.00	2
.21	380.32	182.22	198.10	198.10	.00	2
.11	389.47	184.68	204.78	204.78	.00	2
.00	398.61	187.15	211.46	211.46	.00	2

Time = 1095. Degree of Consolidation = 72.%

Total Settlement = 3.185

Settlement at End of Primary Consolidation = 3.185

Settlement caused by Primary Consolidation at time 1095. = 2.307

Settlement caused by Secondary Compression at time 1095. = .000

Settlement Due to Desiccation = .877

Surface Elevation = 26.91

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
25.00	24.99	17.11	.47	.47	.47	1
18.73	18.72	12.83	.46	.46	.46	1
12.48	12.47	8.56	.46	.46	.46	1
6.23	6.23	4.28	.46	.46	.46	1

BW8FINM.PSO

.00 .00 .00 .46 .45 .45 1

***** Stresses *****

***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	
Material						
24.99	445.42	187.14	258.28	211.46	46.82	1
18.72	1298.33	519.54	778.79	606.23	172.56	1
12.47	2150.50	932.44	1218.07	1000.27	217.79	1
6.23	3001.82	1496.75	1505.07	1393.46	111.61	1
.00	3852.38	2019.68	1832.70	1785.88	46.81	1

Time = 1460. Degree of Consolidation = 43.0%

Total Settlement = .008

Settlement at End of Primary Consolidation = .019

Settlement caused by Primary Consolidation at time 1460. = .008

Settlement caused by Secondary Compression at time 1460. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	
Material						
8.10	4.92	1.16	6.00	2.50	2.50	2
7.94	4.83	1.13	6.00	2.50	2.50	2
7.78	4.75	1.11	6.00	2.50	2.50	2
7.61	4.67	1.09	6.00	2.50	2.50	2
7.45	4.59	1.06	6.00	2.50	2.50	2
7.29	4.51	1.04	6.00	2.50	2.50	2
7.13	4.43	1.02	6.00	2.50	2.50	2
6.97	4.35	1.00	6.00	2.50	2.50	2
6.80	4.27	.97	6.00	2.50	2.50	2
6.64	4.19	.95	6.00	2.50	2.50	2
6.48	4.11	.93	6.00	2.50	2.50	2
6.32	4.02	.90	6.00	2.50	2.50	2
6.16	3.94	.88	6.00	2.50	2.50	2
5.99	3.86	.86	6.00	2.50	2.50	2
5.83	3.78	.83	6.00	2.50	2.50	2
5.67	3.70	.81	6.00	2.50	2.50	2
5.51	3.62	.79	6.00	2.50	2.50	2

BW8FINM.PSO

5.35	3.53	.76	6.00	2.50	2.50	2
5.18	3.46	.74	6.00	2.50	2.50	2
5.02	3.36	.72	6.00	3.78	3.78	2
4.86	3.25	.69	6.00	3.78	3.78	2
4.70	3.14	.67	6.00	3.77	3.77	2
4.54	3.03	.65	6.00	3.76	3.76	2
4.37	2.92	.62	6.00	3.76	3.76	2
4.21	2.81	.60	6.00	3.75	3.75	2
4.05	2.70	.58	6.00	3.74	3.74	2
3.89	2.59	.56	6.00	3.74	3.74	2
3.73	2.48	.53	6.00	3.73	3.73	2
3.56	2.37	.51	6.00	3.72	3.72	2
3.40	2.26	.49	6.00	3.72	3.72	2
3.24	2.15	.46	6.00	3.71	3.71	2
3.08	2.04	.44	6.00	3.70	3.70	2
2.92	1.93	.42	6.00	3.70	3.70	2
2.75	1.82	.39	6.00	3.69	3.69	2
2.59	1.71	.37	6.00	3.68	3.68	2
2.43	1.61	.35	6.00	3.68	3.68	2
2.27	1.50	.32	6.00	3.67	3.67	2
2.11	1.39	.30	6.00	3.66	3.66	2
1.94	1.28	.28	6.00	3.66	3.66	2
1.78	1.17	.25	6.00	3.65	3.65	2
1.62	1.07	.23	6.00	3.64	3.64	2
1.46	.96	.21	6.00	3.64	3.64	2
1.30	.85	.19	6.00	3.63	3.63	2
1.13	.74	.16	6.00	3.62	3.62	2
.97	.64	.14	6.00	3.62	3.62	2
.81	.53	.12	6.00	3.61	3.61	2
.65	.42	.09	6.00	3.60	3.60	2
.49	.32	.07	6.00	3.60	3.60	2
.32	.21	.05	6.00	3.59	3.59	2
.16	.11	.02	6.00	3.58	3.58	2
.00	.00	.00	6.00	3.58	3.58	2

***** Stresses *****

***** Pore Pressures *****

XI Material	Total	Effective	Total	Static	Excess	
4.92	.00	.00	.00	.00	.00	2
4.83	5.74	5.74	.00	.00	.00	2
4.75	11.49	11.49	.00	.00	.00	2
4.67	17.23	17.23	.00	.00	.00	2
4.59	22.98	22.98	.00	.00	.00	2
4.51	28.72	28.72	.00	.00	.00	2
4.43	34.47	34.47	.00	.00	.00	2
4.35	40.21	40.21	.00	.00	.00	2
4.27	45.96	45.96	.00	.00	.00	2
4.19	51.70	51.70	.00	.00	.00	2
4.11	57.45	57.45	.00	.00	.00	2

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4.02	63.19	63.19	.00	.00	.00	2
3.94	68.93	68.93	.00	.00	.00	2
3.86	74.68	74.68	.00	.00	.00	2
3.78	80.42	80.42	.00	.00	.00	2
3.70	86.17	86.17	.00	.00	.00	2
3.62	91.91	91.91	.00	.00	.00	2
3.53	97.66	97.66	.00	.00	.00	2
3.46	103.40	103.40	.00	.00	.00	2
3.36	110.76	110.76	.00	.00	.00	2
3.25	120.19	113.23	6.97	6.97	.00	2
3.14	129.61	115.69	13.92	13.92	.00	2
3.03	139.03	118.15	20.87	20.87	.00	2
2.92	148.43	120.62	27.81	27.81	.00	2
2.81	157.82	123.08	34.74	34.74	.00	2
2.70	167.20	125.55	41.66	41.66	.00	2
2.59	176.58	128.01	48.56	48.56	.00	2
2.48	185.94	130.47	55.46	55.46	.00	2
2.37	195.29	132.94	62.35	62.35	.00	2
2.26	204.64	135.40	69.23	69.23	.00	2
2.15	213.97	137.87	76.10	76.10	.00	2
2.04	223.29	140.33	82.96	82.96	.00	2
1.93	232.61	142.80	89.81	89.81	.00	2
1.82	241.91	145.26	96.65	96.65	.00	2
1.71	251.21	147.72	103.48	103.48	.00	2
1.61	260.49	150.19	110.31	110.31	.00	2
1.50	269.77	152.65	117.12	117.12	.00	2
1.39	279.03	155.12	123.92	123.92	.00	2
1.28	288.29	157.58	130.71	130.71	.00	2
1.17	297.54	160.04	137.49	137.49	.00	2
1.07	306.77	162.51	144.27	144.27	.00	2
.96	316.00	164.97	151.03	151.03	.00	2
.85	325.22	167.44	157.78	157.78	.00	2
.74	334.42	169.90	164.53	164.53	.00	2
.64	343.62	172.36	171.26	171.26	.00	2
.53	352.81	174.83	177.98	177.98	.00	2
.42	361.99	177.29	184.70	184.70	.00	2
.32	371.16	179.76	191.40	191.40	.00	2
.21	380.32	182.22	198.10	198.10	.00	2
.11	389.47	184.68	204.78	204.78	.00	2
.00	398.61	187.15	211.46	211.46	.00	2

Time = 1460. Degree of Consolidation = 72.0%

Total Settlement = 3.185

Settlement at End of Primary Consolidation = 3.185

Settlement caused by Primary Consolidation at time 1460. = 2.307

Settlement caused by Secondary Compression at time 1460. = .000

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Settlement Due to Desiccation = .877

Surface Elevation = 26.91

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****				
Material	A	XI	Z	Einitial	E	Eeop	
	25.00	24.99	17.11	.47	.47	.47	1
	18.73	18.72	12.83	.46	.46	.46	1
	12.48	12.47	8.56	.46	.46	.46	1
	6.23	6.23	4.28	.46	.46	.46	1
	.00	.00	.00	.46	.45	.45	1
	Time = 2190.		Degree of Consolidation = 56.%				
	Total Settlement =		.010				
	Settlement at End of Primary Consolidation =		.019				
	Settlement caused by Primary Consolidation at time 2190. =		.010				
	Settlement caused by Secondary Compression at time 2190. =		.000				

*****Current Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****				
Material	A	XI	Z	Einitial	E	Eeop	
	8.10	4.92	1.16	6.00	2.50	2.50	2
	7.94	4.83	1.13	6.00	2.50	2.50	2
	7.78	4.75	1.11	6.00	2.50	2.50	2
	7.61	4.67	1.09	6.00	2.50	2.50	2
	7.45	4.59	1.06	6.00	2.50	2.50	2
	7.29	4.51	1.04	6.00	2.50	2.50	2
	7.13	4.43	1.02	6.00	2.50	2.50	2
	6.97	4.35	1.00	6.00	2.50	2.50	2
	6.80	4.27	.97	6.00	2.50	2.50	2

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6.64	4.19	.95	6.00	2.50	2.50	2
6.48	4.11	.93	6.00	2.50	2.50	2
6.32	4.02	.90	6.00	2.50	2.50	2
6.16	3.94	.88	6.00	2.50	2.50	2
5.99	3.86	.86	6.00	2.50	2.50	2
5.83	3.78	.83	6.00	2.50	2.50	2
5.67	3.70	.81	6.00	2.50	2.50	2
5.51	3.62	.79	6.00	2.50	2.50	2
5.35	3.53	.76	6.00	2.50	2.50	2
5.18	3.46	.74	6.00	2.50	2.50	2
5.02	3.36	.72	6.00	3.78	3.78	2
4.86	3.25	.69	6.00	3.78	3.78	2
4.70	3.14	.67	6.00	3.77	3.77	2
4.54	3.03	.65	6.00	3.76	3.76	2
4.37	2.92	.62	6.00	3.76	3.76	2
4.21	2.81	.60	6.00	3.75	3.75	2
4.05	2.70	.58	6.00	3.74	3.74	2
3.89	2.59	.56	6.00	3.74	3.74	2
3.73	2.48	.53	6.00	3.73	3.73	2
3.56	2.37	.51	6.00	3.72	3.72	2
3.40	2.26	.49	6.00	3.72	3.72	2
3.24	2.15	.46	6.00	3.71	3.71	2
3.08	2.04	.44	6.00	3.70	3.70	2
2.92	1.93	.42	6.00	3.70	3.70	2
2.75	1.82	.39	6.00	3.69	3.69	2
2.59	1.71	.37	6.00	3.68	3.68	2
2.43	1.61	.35	6.00	3.68	3.68	2
2.27	1.50	.32	6.00	3.67	3.67	2
2.11	1.39	.30	6.00	3.66	3.66	2
1.94	1.28	.28	6.00	3.66	3.66	2
1.78	1.17	.25	6.00	3.65	3.65	2
1.62	1.07	.23	6.00	3.64	3.64	2
1.46	.96	.21	6.00	3.64	3.64	2
1.30	.85	.19	6.00	3.63	3.63	2
1.13	.74	.16	6.00	3.62	3.62	2
.97	.64	.14	6.00	3.62	3.62	2
.81	.53	.12	6.00	3.61	3.61	2
.65	.42	.09	6.00	3.60	3.60	2
.49	.32	.07	6.00	3.60	3.60	2
.32	.21	.05	6.00	3.59	3.59	2
.16	.11	.02	6.00	3.58	3.58	2
.00	.00	.00	6.00	3.58	3.58	2

Time = 2190. Degree of Consolidation = 72.%

Total Settlement = 3.185

Settlement at End of Primary Consolidation = 3.185

Settlement caused by Primary Consolidation at time 2190. = 2.307

BW8FINM.PSO

Settlement caused by Secondary Compression at time 2190. = .000

Settlement Due to Desiccation = .877

Surface Elevation = 26.90

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
25.00	24.99	17.11	.47	.47	.47	1
18.73	18.72	12.83	.46	.46	.46	1
12.48	12.47	8.56	.46	.46	.46	1
6.23	6.23	4.28	.46	.46	.46	1
.00	.00	.00	.46	.45	.45	1

Time = 2920. Degree of Consolidation = 67.%

Total Settlement = .012

Settlement at End of Primary Consolidation = .019

Settlement caused by Primary Consolidation at time 2920. = .012

Settlement caused by Secondary Compression at time 2920. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
8.10	4.92	1.16	6.00	2.50	2.50	2
7.94	4.83	1.13	6.00	2.50	2.50	2
7.78	4.75	1.11	6.00	2.50	2.50	2
7.61	4.67	1.09	6.00	2.50	2.50	2
7.45	4.59	1.06	6.00	2.50	2.50	2
7.29	4.51	1.04	6.00	2.50	2.50	2
7.13	4.43	1.02	6.00	2.50	2.50	2

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6.97	4.35	1.00	6.00	2.50	2.50	2
6.80	4.27	.97	6.00	2.50	2.50	2
6.64	4.19	.95	6.00	2.50	2.50	2
6.48	4.11	.93	6.00	2.50	2.50	2
6.32	4.02	.90	6.00	2.50	2.50	2
6.16	3.94	.88	6.00	2.50	2.50	2
5.99	3.86	.86	6.00	2.50	2.50	2
5.83	3.78	.83	6.00	2.50	2.50	2
5.67	3.70	.81	6.00	2.50	2.50	2
5.51	3.62	.79	6.00	2.50	2.50	2
5.35	3.53	.76	6.00	2.50	2.50	2
5.18	3.46	.74	6.00	2.50	2.50	2
5.02	3.36	.72	6.00	3.78	3.78	2
4.86	3.25	.69	6.00	3.78	3.78	2
4.70	3.14	.67	6.00	3.77	3.77	2
4.54	3.03	.65	6.00	3.76	3.76	2
4.37	2.92	.62	6.00	3.76	3.76	2
4.21	2.81	.60	6.00	3.75	3.75	2
4.05	2.70	.58	6.00	3.74	3.74	2
3.89	2.59	.56	6.00	3.74	3.74	2
3.73	2.48	.53	6.00	3.73	3.73	2
3.56	2.37	.51	6.00	3.72	3.72	2
3.40	2.26	.49	6.00	3.72	3.72	2
3.24	2.15	.46	6.00	3.71	3.71	2
3.08	2.04	.44	6.00	3.70	3.70	2
2.92	1.93	.42	6.00	3.70	3.70	2
2.75	1.82	.39	6.00	3.69	3.69	2
2.59	1.71	.37	6.00	3.68	3.68	2
2.43	1.61	.35	6.00	3.68	3.68	2
2.27	1.50	.32	6.00	3.67	3.67	2
2.11	1.39	.30	6.00	3.66	3.66	2
1.94	1.28	.28	6.00	3.66	3.66	2
1.78	1.17	.25	6.00	3.65	3.65	2
1.62	1.07	.23	6.00	3.64	3.64	2
1.46	.96	.21	6.00	3.64	3.64	2
1.30	.85	.19	6.00	3.63	3.63	2
1.13	.74	.16	6.00	3.62	3.62	2
.97	.64	.14	6.00	3.62	3.62	2
.81	.53	.12	6.00	3.61	3.61	2
.65	.42	.09	6.00	3.60	3.60	2
.49	.32	.07	6.00	3.60	3.60	2
.32	.21	.05	6.00	3.59	3.59	2
.16	.11	.02	6.00	3.58	3.58	2
.00	.00	.00	6.00	3.58	3.58	2

Time = 2920. Degree of Consolidation = 72.0%

Total Settlement = 3.185

Settlement at End of Primary Consolidation = 3.185

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Settlement caused by Primary Consolidation at time 2920. = 2.307

Settlement caused by Secondary Compression at time 2920. = .000

Settlement Due to Desiccation = .877

Surface Elevation = 26.90

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
25.00	24.98	17.11	.47	.47	.47	1
18.73	18.72	12.83	.46	.46	.46	1
12.48	12.47	8.56	.46	.46	.46	1
6.23	6.23	4.28	.46	.46	.46	1
.00	.00	.00	.46	.45	.45	1
Time = 3650. Degree of Consolidation = 75.%						
Total Settlement = .014						
Settlement at End of Primary Consolidation = .019						
Settlement caused by Primary Consolidation at time 3650. = .014						
Settlement caused by Secondary Compression at time 3650. = .000						

*****Current Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
8.10	4.92	1.16	6.00	2.50	2.50	2
7.94	4.83	1.13	6.00	2.50	2.50	2
7.78	4.75	1.11	6.00	2.50	2.50	2
7.61	4.67	1.09	6.00	2.50	2.50	2
7.45	4.59	1.06	6.00	2.50	2.50	2

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7.29	4.51	1.04	6.00	2.50	2.50	2
7.13	4.43	1.02	6.00	2.50	2.50	2
6.97	4.35	1.00	6.00	2.50	2.50	2
6.80	4.27	.97	6.00	2.50	2.50	2
6.64	4.19	.95	6.00	2.50	2.50	2
6.48	4.11	.93	6.00	2.50	2.50	2
6.32	4.02	.90	6.00	2.50	2.50	2
6.16	3.94	.88	6.00	2.50	2.50	2
5.99	3.86	.86	6.00	2.50	2.50	2
5.83	3.78	.83	6.00	2.50	2.50	2
5.67	3.70	.81	6.00	2.50	2.50	2
5.51	3.62	.79	6.00	2.50	2.50	2
5.35	3.53	.76	6.00	2.50	2.50	2
5.18	3.46	.74	6.00	2.50	2.50	2
5.02	3.36	.72	6.00	3.78	3.78	2
4.86	3.25	.69	6.00	3.78	3.78	2
4.70	3.14	.67	6.00	3.77	3.77	2
4.54	3.03	.65	6.00	3.76	3.76	2
4.37	2.92	.62	6.00	3.76	3.76	2
4.21	2.81	.60	6.00	3.75	3.75	2
4.05	2.70	.58	6.00	3.74	3.74	2
3.89	2.59	.56	6.00	3.74	3.74	2
3.73	2.48	.53	6.00	3.73	3.73	2
3.56	2.37	.51	6.00	3.72	3.72	2
3.40	2.26	.49	6.00	3.72	3.72	2
3.24	2.15	.46	6.00	3.71	3.71	2
3.08	2.04	.44	6.00	3.70	3.70	2
2.92	1.93	.42	6.00	3.70	3.70	2
2.75	1.82	.39	6.00	3.69	3.69	2
2.59	1.71	.37	6.00	3.68	3.68	2
2.43	1.61	.35	6.00	3.68	3.68	2
2.27	1.50	.32	6.00	3.67	3.67	2
2.11	1.39	.30	6.00	3.66	3.66	2
1.94	1.28	.28	6.00	3.66	3.66	2
1.78	1.17	.25	6.00	3.65	3.65	2
1.62	1.07	.23	6.00	3.64	3.64	2
1.46	.96	.21	6.00	3.64	3.64	2
1.30	.85	.19	6.00	3.63	3.63	2
1.13	.74	.16	6.00	3.62	3.62	2
.97	.64	.14	6.00	3.62	3.62	2
.81	.53	.12	6.00	3.61	3.61	2
.65	.42	.09	6.00	3.60	3.60	2
.49	.32	.07	6.00	3.60	3.60	2
.32	.21	.05	6.00	3.59	3.59	2
.16	.11	.02	6.00	3.58	3.58	2
.00	.00	.00	6.00	3.58	3.58	2

Time = 3650. Degree of Consolidation = 72.%

Total Settlement = 3.185

BW8FINM.PSO

Settlement at End of Primary Consolidation = 3.185

Settlement caused by Primary Consolidation at time 3650. = 2.307

Settlement caused by Secondary Compression at time 3650. = .000

Settlement Due to Desiccation = .877

Surface Elevation = 26.90

*****Current Conditions in Compressible Foundation*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
25.00	24.98	17.11	.47	.47	.47	1
18.73	18.72	12.83	.46	.46	.46	1
12.48	12.47	8.56	.46	.46	.46	1
6.23	6.23	4.28	.46	.46	.46	1
.00	.00	.00	.46	.45	.45	1

Time = 8760. Degree of Consolidation = 77.%

Total Settlement = .014

Settlement at End of Primary Consolidation = .019

Settlement caused by Primary Consolidation at time 8760. = .014

Settlement caused by Secondary Compression at time 8760. = .000

*****Current Conditions in Dredged Fill*****

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	
Material						
8.10	4.92	1.16	6.00	2.50	2.50	2
7.94	4.83	1.13	6.00	2.50	2.50	2
7.78	4.75	1.11	6.00	2.50	2.50	2

BW8FINM.PSO

7.61	4.67	1.09	6.00	2.50	2.50	2
7.45	4.59	1.06	6.00	2.50	2.50	2
7.29	4.51	1.04	6.00	2.50	2.50	2
7.13	4.43	1.02	6.00	2.50	2.50	2
6.97	4.35	1.00	6.00	2.50	2.50	2
6.80	4.27	.97	6.00	2.50	2.50	2
6.64	4.19	.95	6.00	2.50	2.50	2
6.48	4.11	.93	6.00	2.50	2.50	2
6.32	4.02	.90	6.00	2.50	2.50	2
6.16	3.94	.88	6.00	2.50	2.50	2
5.99	3.86	.86	6.00	2.50	2.50	2
5.83	3.78	.83	6.00	2.50	2.50	2
5.67	3.70	.81	6.00	2.50	2.50	2
5.51	3.62	.79	6.00	2.50	2.50	2
5.35	3.53	.76	6.00	2.50	2.50	2
5.18	3.46	.74	6.00	2.50	2.50	2
5.02	3.36	.72	6.00	3.78	3.78	2
4.86	3.25	.69	6.00	3.78	3.78	2
4.70	3.14	.67	6.00	3.77	3.77	2
4.54	3.03	.65	6.00	3.76	3.76	2
4.37	2.92	.62	6.00	3.76	3.76	2
4.21	2.81	.60	6.00	3.75	3.75	2
4.05	2.70	.58	6.00	3.74	3.74	2
3.89	2.59	.56	6.00	3.74	3.74	2
3.73	2.48	.53	6.00	3.73	3.73	2
3.56	2.37	.51	6.00	3.72	3.72	2
3.40	2.26	.49	6.00	3.72	3.72	2
3.24	2.15	.46	6.00	3.71	3.71	2
3.08	2.04	.44	6.00	3.70	3.70	2
2.92	1.93	.42	6.00	3.70	3.70	2
2.75	1.82	.39	6.00	3.69	3.69	2
2.59	1.71	.37	6.00	3.68	3.68	2
2.43	1.61	.35	6.00	3.68	3.68	2
2.27	1.50	.32	6.00	3.67	3.67	2
2.11	1.39	.30	6.00	3.66	3.66	2
1.94	1.28	.28	6.00	3.66	3.66	2
1.78	1.17	.25	6.00	3.65	3.65	2
1.62	1.07	.23	6.00	3.64	3.64	2
1.46	.96	.21	6.00	3.64	3.64	2
1.30	.85	.19	6.00	3.63	3.63	2
1.13	.74	.16	6.00	3.62	3.62	2
.97	.64	.14	6.00	3.62	3.62	2
.81	.53	.12	6.00	3.61	3.61	2
.65	.42	.09	6.00	3.60	3.60	2
.49	.32	.07	6.00	3.60	3.60	2
.32	.21	.05	6.00	3.59	3.59	2
.16	.11	.02	6.00	3.58	3.58	2
.00	.00	.00	6.00	3.58	3.58	2

Time = 8760. Degree of Consolidation = 72.0%

BW8FINM.PSO

Total Settlement = 3.185

Settlement at End of Primary Consolidation = 3.185

Settlement caused by Primary Consolidation at time 8760. = 2.307

Settlement caused by Secondary Compression at time 8760. = .000

Settlement Due to Desiccation = .877

Surface Elevation = 26.90